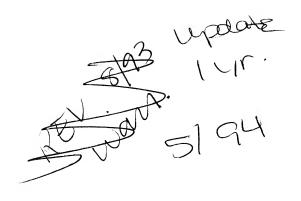
720A Kelvin-Varley Voltage Divider

Instruction Manual

P/N 294058 March 1969 Rev. 2 9/74





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*For European customers, Air Freight prepaid.

Jöhn Fluke Mfg. Co., Inc., P.O. Box C9090, Everett, Washington 98206

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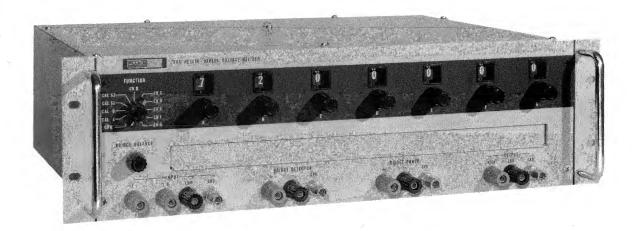
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MODEL 720A KELVIN-VARLEY VOLTAGE DIVIDER

Section 1

Introduction & Specifications

1-1. INTRODUCTION

- The Model 720A Kelvin-Varley Voltage Divider is a seven-dial primary ratio standard which meets the most exacting requirements of the standards laboratory. Absolute linearity of 0.1 ppm, temperature coefficient of linearity of 0.1 ppm/°C, and self-calibration make the 720A the most accurate instrument available for the comparison of primary and secondary voltage and resistance standards. The linearity has a small power derating coefficient of 0.2 ppm per watt which is achieved by matching the resistors' temperature coefficients close to zero. This permits operation at up to 1100 volts and 11 watts.
- The Model 720A has two high input terminals. The terminal labeled INPUT 1.0 is for general use in all Kelvin-Varley applications for which direct reading, in ratio, is desired. The terminal labeled INPUT 1.1 is used for voltage measurement applications when both direct reading in voltage and over-ranging are desired. An example of this application is the measurement of standard cell voltages. Use of the 1.1 INPUT at a level of 1.1 volts in this application results in divider resolution of 0.1 microvolt and allows comparison of standard cells to within 1 microvolt.
- Only thoroughly aged resistors of the highest quality are used in the Model 720A Kelvin-Varley Divider. As a result, linearity change per year will not exceed one part per million unless the instrument is subjected to abuse. To assure that the divider remains within its specifications throughout its useful life, adjustments are provided for the resistors of the first three decades. The third decade adjustments normally will be used only during annual calibration. Performing the self calibration procedure sets the adjustments of the first two decades. With reasonable care these adjustments will provide instrument accuracy of 0.1 part per million at the time of adjustment.

1-5. **ELECTRICAL SPECIFICATIONS**

RATIO RANGE

0 to 1.0 (1.0 INPUT TAP) and 0 to 1.1 (1.1 INPUT TAP).

RESOLUTION

0.1 ppm of input with 7 decades.

ABSOLUTE LINEARITY

(at calibration temperature and without the use of a correction chart)*

 ± 0.1 ppm of input at dial settings of 1.1 to 0.1. ± 0.1 (10S)^{1/3} of input at dial settings (S) of 0.1 to 0. (See Figure 1-1.)

ABSOLUTE LINEARITY STABILITY (without self-calibration)

 ± 1.0 ppm of input/year at dial settings of 1.1 to 0.1. ± 1.0 (10S) $^{2/3}$ ppm of input/year at dial settings (S) of 0.1 to 0.

(See Figure 1-2.)

NOTE!

The self-calibration procedure may be used at any time to reset absolute linearity to ± 0.1 ppm of input.

TEMPERATURE COEFFICIENT OF LINEARITY ±0.1 ppm of input/°C maximum at dial settings of 1.1 to 0.1.

(See Figure 1-3.)

SHORT-TERM LINEARITY STABILITY

Under typical conditions in a standards laboratory environment (temperature maintained within $\pm 1^{\circ}$ C) and with an applied voltage of up to 100 volts, stability of linearity is 0.1 ppm/30 days.

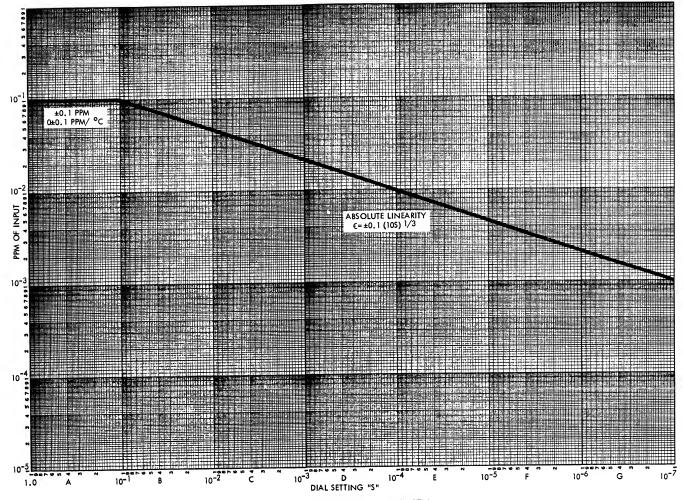


Figure 1-1. ABSOLUTE LINEARITY

POWER COEFFICIENT OF LINEARITY

 ± 0.2 ppm of input/watt maximum at dial settings of 1.1 to 0.1.

 $\pm 0.2 (10S)^2$ ppm of input/watt maximum at dial settings (S) of 0.1 to 0. (See Figure 1-4.)

MAXIMUM END ERRORS

Zero error, at output low
Zero error, at input low
0.004 ppm of input
0.05 ppm of input
Full-scale error
0.05 ppm of input

THERMAL VOLTAGES ±0.5 uv maximum.

MAXIMUM INPUT POWER

10 watts on 1.0 INPUT terminal. 11 watts on 1.1 INPUT terminal.

*Absolute linearity is defined as the linearity between maximum and minimum output voltages.

MAXIMUM INPUT VOLTAGE 1000 volts on 1.0 INPUT terminal. 1100 volts on 1.1 INPUT terminal.

BREAKDOWN VOLTAGE 2000 volts to case at 10,000 feet.

2500 volts to case at sea level.

INPUT RESISTANCE

100 kilohms $\pm 0.005\%$ at 1.0 INPUT terminal at 25°C. 110 kilohms $\pm 0.005\%$ at 1.1 INPUT terminal at 25°C.

TEMPERATURE COEFFICIENT OF INPUT RESISTANCE ±1 ppm/°C maximum.

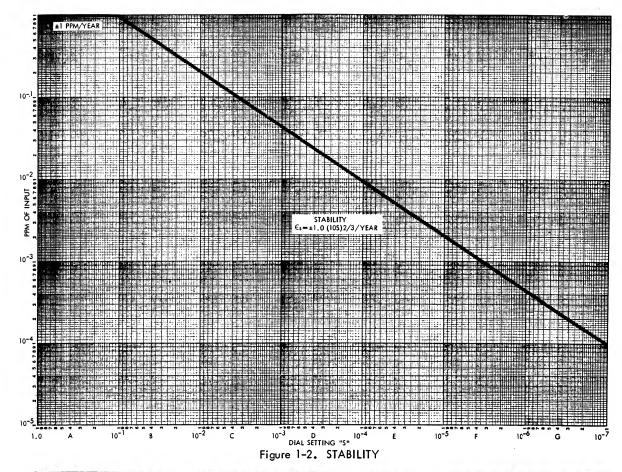
MAXIMUM OUTPUT RESISTANCE 66 kilohms.

1-6. MECHANICAL AND ENVIRONMENTAL SPECIFICATIONS

OPERATING TEMPERATURE RANGE 0°C to 50°C (32°F to 122°F).

NOTE!

When the Model 720A is used at temperatures below 15°C (59°F) or above 35°C (95°F), the range of the calibration adjustments may be



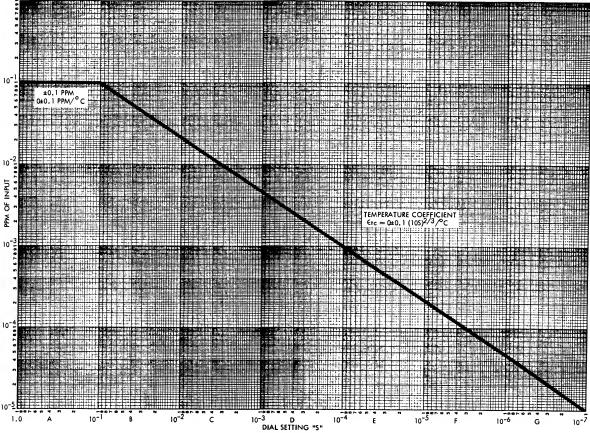


Figure 1-3. TEMPERATURE COEFFICIENT

exceeded and linearity must be derated 0.1 ppm/°C from the calibration temperature,

OPERATING HUMIDITY RANGE

Up to 70% relative humidity at 35° C (95° F): No derating is required.

Up to 80% relative humidity at 35°C (95°F): Linearity derating is 0.1 ppm of input for any relative humidity between 70% and 80%.

STORAGE TEMPERATURE RANGE -34°C to 70°C (-29°F to 158°F).

SHOCK

Meets requirements of MIL-T-945A and MIL-S-901B, rigidly mounted with slides.

VIBRATION

Meets requirements of MIL-T-945A, rigidly mounted or rack mounted with slides.

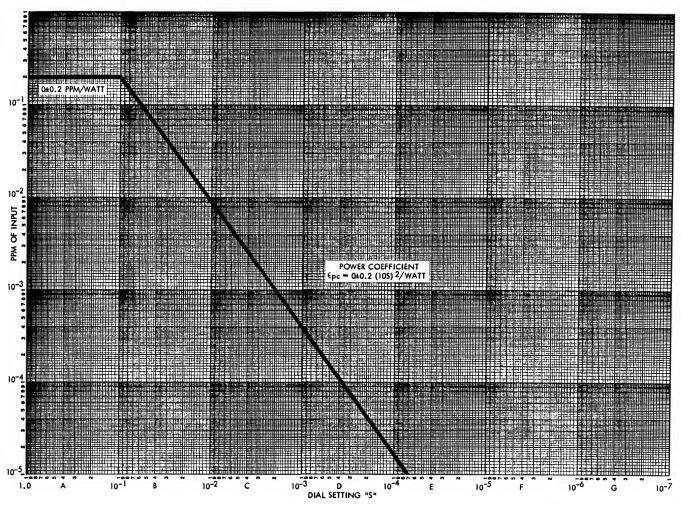


Figure 1-4. POWER COEFFICIENT

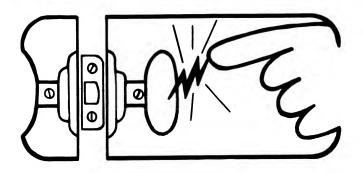


static awareness



A Message From

John Fluke Mfg. Co., Inc.

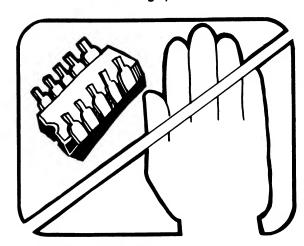


Some semiconductors and custom IC's can be damaged by electrostatic discharge during handling. This notice explains how you can minimize the chances of destroying such devices by:

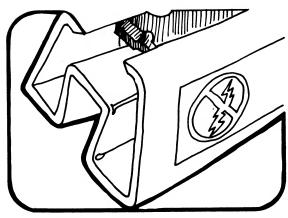
- 1. Knowing that there is a problem.
- 2. Learning the guidelines for handling them.
- 3. Using the procedures, and packaging and bench techniques that are recommended.

The Static Sensitive (S.S.) devices are identified in the Fluke technical manual parts list with the symbol " ()"

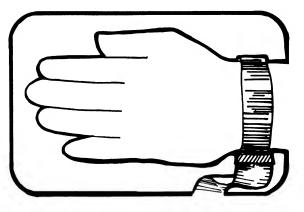
The following practices should be followed to minimize damage to S.S. devices.



1. MINIMIZE HANDLING



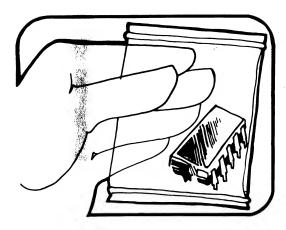
2. KEEP PARTS IN ORIGINAL CONTAINERS UNTIL READY FOR USE.



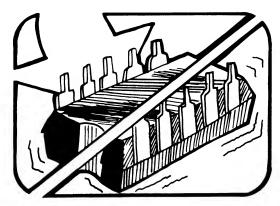
3. DISCHARGE PERSONAL STATIC BEFORE HANDLING DEVICES. USE A HIGH RESISTANCE GROUNDING WRIST STRAP.



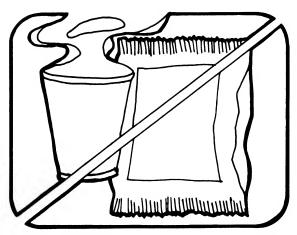
4. HANDLE S.S. DEVICES BY THE BODY



5. USE STATIC SHIELDING CONTAINERS FOR HANDLING AND TRANSPORT

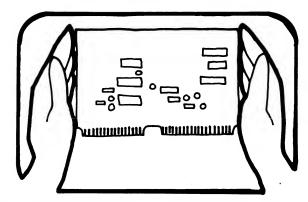


6. DO NOT SLIDE S.S. DEVICES OVER ANY SURFACE

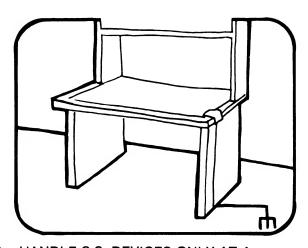


7. AVOID PLASTIC, VINYL AND STYROFOAM® IN WORK AREA

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AND GENERAL DYNAMICS, POMONA DIV.



8. WHEN REMOVING PLUG-IN ASSEMBLIES, HANDLE ONLY BY NON-CONDUCTIVE EDGES AND NEVER TOUCH OPEN EDGE CONNECTOR EXCEPT AT STATIC-FREE WORK STATION. PLACING SHORTING STRIPS ON EDGE CONNECTOR HELPS TO PROTECT INSTALLED SS DEVICES.



- 9. HANDLE S.S. DEVICES ONLY AT A STATIC-FREE WORK STATION
- 10. ONLY ANTI-STATIC TYPE SOLDER-SUCKERS SHOULD BE USED.
- 11. ONLY GROUNDED TIP SOLDERING IRONS SHOULD BE USED.

A complete line of static shielding bags and accessories is available from Fluke Parts Department, Telephone 800-526-4731 or write to:

JOHN FLUKE MFG. CO., INC. PARTS DEPT. M/S 86 9028 EVERGREEN WAY EVERETT, WA 98204

Section 2

Operating Instructions

2-1. INTRODUCTION

2-2. Although the Model 720A is a primary ratio standard it has the versatility necessary for use in a wide variety of measurement and control applications. In most applications the divider is used as an element of a system for measuring ratios, voltages, or resistances.

2-3. POWER LIMITATIONS

2-4. It is possible to damage the Model 720A by applying voltages incorrectly to the input terminals or by drawing more than 11 milliamperes from the output tap. The instrument will be damaged if a potential greater than 200 volts is applied between the 1.0 INPUT terminal and the 1.1 INPUT terminal. To prevent damage caused by drawing excessive current from the output tap, either the input or the output can be fused for 11 milliamperes. Another method of protecting the instrument is through the use of a power supply with current limiting capability. The current limit should be set for 11 milliamperes or less.

2-5. FUNCTIONS OF CONTROLS AND TERMINALS

2-6. Figure 2-1 shows the controls and terminals of the Model 720A and describes their functions.

2-7. RATIO ERRORS CAUSED BY LOADING OR LEAKAGE

- 2-8. Measurements of any kind require a knowledge of the errors associated with the equipment used to perform the measurement. Measurement made with the Model 720A are not different.
- 2-9. One very important source of error in measurements employing the Model 720A is the effect that external load and leakage resistances have on overall accuracy. If excessive current is drawn from the divider output tap because of loading or leakage, linearity errors which far exceed the linearity specifications can result. For this reason, Kelvin-Varley dividers customarily are used in null-balance systems in which minimum current is drawn from the divider output tap.

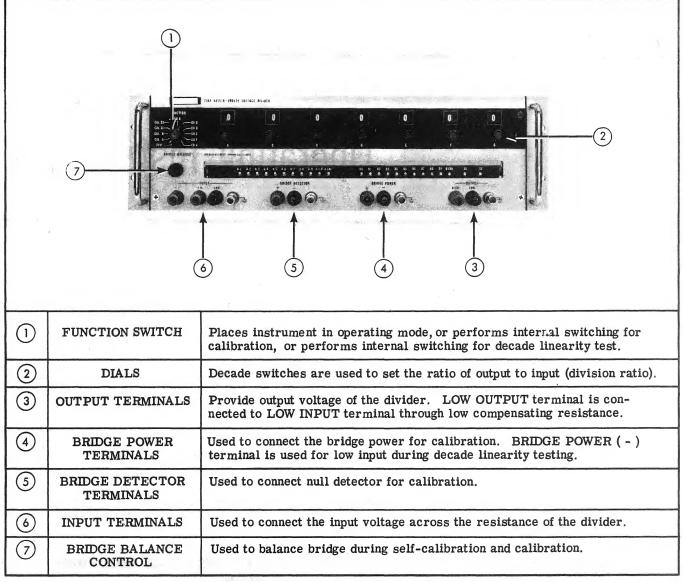


Figure 2-1. FUNCTIONS OF CONTROLS AND TERMINALS

2-10. Loading Errors

2-11. Figure 2-2 illustrates the Thevinin equivalent for the Model 720A Kelvin-Varley Divider.

To calculate the error in output voltage, as a fraction of the input voltage, the following expressions are given.

$$E_0 (1 + \epsilon_0) = \frac{S(1 + \epsilon) E_{IN} R_L}{R_L + R_0}$$

but
$$E_0 = SE_{IN}$$

therefore
$$(1 + \epsilon_0) = \frac{(1 + \epsilon) R_L}{R_L + R_0}$$

If
$$R_L \gg R_0$$
 and $\left(1 + \frac{R_0}{R_L}\right)$ is expanded in series then
$$(1 + \epsilon_0) = (1 + \epsilon) \left[1 - \frac{R_0}{R_L} + \left(\frac{R_0}{R_L}\right)^2 - \left(\frac{R_0}{R_2}\right)^3 + \dots \right]$$

$$\cong (1 + \epsilon) \left(1 - \frac{R_0}{R_L}\right)$$

$$\epsilon_0 \cong \epsilon - \frac{R_0}{R_L}$$

and
$$\in_{L}^{\underline{\omega}} \frac{R_0}{R_L}$$

Converting to errors expressed as a fraction of the input voltage the expression becomes:

$$\in^{\dagger}_{0} = \in^{\dagger} - \frac{S R_{0}}{R_{L}}$$

If the 1.1 INPUT terminal is used then:

$$E_0 = \frac{S}{1 - 1} E_{IN}$$

and:

$$\in$$
'o \cong \in ' - $\frac{SR_0}{1.1 R_T}$

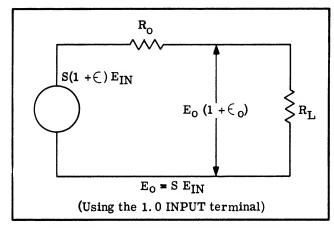


Figure 2-2. THEVININ EQUIVALENT CIRCUIT

- 2-12. The following list of definitions are given for the terms used in the preceding paragraphs.
- a. E₀ Nominal output voltage.
- b. E_{IN} Input voltage.
- c. ϵ_0 Error in output voltage as a fraction of output.
- d. \in Divider linearity error as a fraction of output.
- e. ξ_{τ} Loading error as a fraction of output.
- f. \in o Error in output voltage as a fraction of input.
- g. \in ' Divider linearity error as a fraction of input.
- h. $\in \frac{1}{L}$ Loading error as a fraction of input.
- i. S Divider dial setting.
- j. R_O Divider output resistance.
- k. R_L Load resistance (including leakage resistance from the tap terminal to the divider input terminal).

2-13. Output Resistance Versus Loading

- 2-14. The graph in Figure 2-3 illustrates the approximate variation of output resistance with the dial setting for both the 1.0 and 1.1 INPUT terminals. This resistance is measured by shorting the input high and input low terminals and measuring the resistance between the output high and low terminals. When computing correction factors for loading of a particular instrument do not use the approximate resistance values given by Figure 2-3. Instead, measure the output resistance at the desired dial setting. The maximum amount of loading which will still be negligible for any dial setting may be calculated as follows:
- a. Divider specification = 0.1 ppm of input.
- b. Maximum loading error limit = 0.03 ppm of input.

c.
$$\frac{S R_0}{R_L} = \{$$
 = 0.3 x 10⁻⁸

d. Maximum $R_0 = 66$ kilohms when S = .454.

e. Minimum
$$R_L = \frac{S R_0}{\xi_L} = \frac{(.454) (6.6 \times 10^4)}{3 \times 10^{-8}}$$

$$= 1 \times 10^{12} \text{ ohms.}$$

- 2-15. Similar calculations have been made for other dial settings and the results have been plotted in Figure 2-4. The choice of a loading error limit of 0.03 ppm was, of course, arbitrary and should vary over a wide range for different measurement applications. In general, the error should be calculated and allowances made unless the errors are small compared to either the desired measurement accuracies or the divider specifications.
- 2-16. It should be noted that resistances calculated are the parallel combinations of the load resistor and any leakage resistances which may exist from the tap point (OUTPUT HIGH terminal) to the input terminals of the divider.
- 2-17. In applications where the load resistance must be supplied with a current, this current may be supplied by either a stable power supply or a second voltage divider in parallel with the measurement divider.

2-18. TEMPERATURE CONTROL

2-19. Because of slight differences in temperature coefficients of the resistors used in the Model 720A, the linearity of the divider will vary with ambient temperature. This change in linearity will never exceed ±0.1 ppm of input per degree centigrade for dial settings above 0.1, and typically will be 0.05 ppm/°C. For measurement applications which require the best possible accuracy, temperature and temperature variations must be considered. The operating temperature should be within 1°C of the self-calibration temperature if at all possible. If the desired operating temperature is

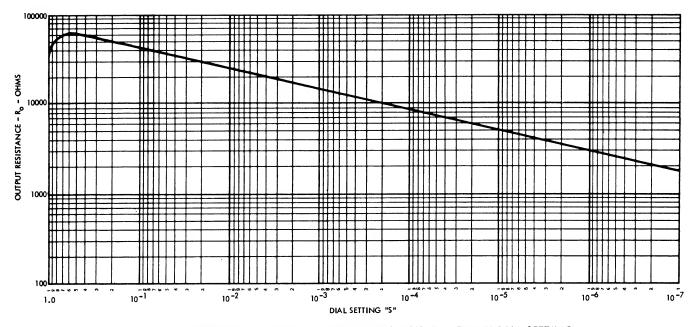


Figure 2-3. APPROXIMATE VARIATION OF OUTPUT RESISTANCE WITH DIAL SETTING

appreciably different from the last calibration temperature, the instrument should be allowed to stabilize at the operating temperature and then the self-calibration procedure should be performed to adjust linearity to 0.1 ppm of input. The Model 720A is factory tested at a temperature of $23 \pm 1^{\circ}$ C.

2-20. POWER COEFFICIENT

2-21. The power coefficient will not exceed 0.2 ppm per watt of input power and typically will be 0.1 ppm per watt or less. With high-voltage applied, self-heating will cause the linearity of the instrument to drift. This drift may continue for as long as four hours after application of the high voltage. Low-voltage, highaccuracy measurements (0.1 ppm) should not be attempted immediately after high-voltage use. Each time the setting of the "A" decade is changed, the power distribution in it is changed because the current through the instrument is divided between the two shunted resistors of the "A" decade and the resistance of the other decades which shunts them. Because of this current division, the two shunted resistors do not become as hot as the other resistors in the "A" decade. The change in current distribution brought about by changing the setting of the "A" decade causes linearity to drift for a few minutes if high voltage is applied.

2-22. END ERRORS

2-23. When the Model 720A is compared to another divider, and a lead compensator such as the Fluke Model 721A is used, absolute linearity may be used directly without correction for end errors. In other applications, the use of a lead compensator is not practical and end error corrections must be applied. Use the following procedure to determine the end error corrections for the Model 720A:

- a. Connect the equipment as shown in Figure 2-5 (A).
- b. Adjust the input voltage to 1000 volts.
- c. With all dials set to zero, measure the voltage between the OUTPUT HIGH terminal and the INPUT LOW terminal. This is the zero error at input low. One microvolt equals 0.001 ppm.
- d. Connect the equipment shown in Figure 2-5 (B).
- e. Adjust the input voltage to 1000 volts.
- f. With all dials set to zero, measure the voltage between the OUTPUT HIGH and OUTPUT LOW terminals. This is the zero error at output low. One microvolt equals 0.001 ppm.
- g. Connect the equipment as shown in Figure 2-5 (C).
- h. Adjust the input voltage to 1000 volts.
- With dials set to 999999X, measure the voltage between the OUTPUT HIGH and 1.0 terminals. This is the full-scale error. One microvolt equals 0.001 ppm.
- j. Maintain the test set up of Figure 2-5 (C) except move the two leads connected to the 1.0 INPUT terminal to the 1.1 INPUT terminal.
- k. Adjust the input voltage to 1000 volts.
- With all dials set to 1.0 09999X, measure the voltage between the OUTPUT HIGH and 1.1 INPUT terminals. One microvolt equals 0.001 ppm.

2-24. SELF-CALIBRATION PROCEDURE

2-25. Performing this self-calibration procedure adjusts the step resistance and overall resistance of the

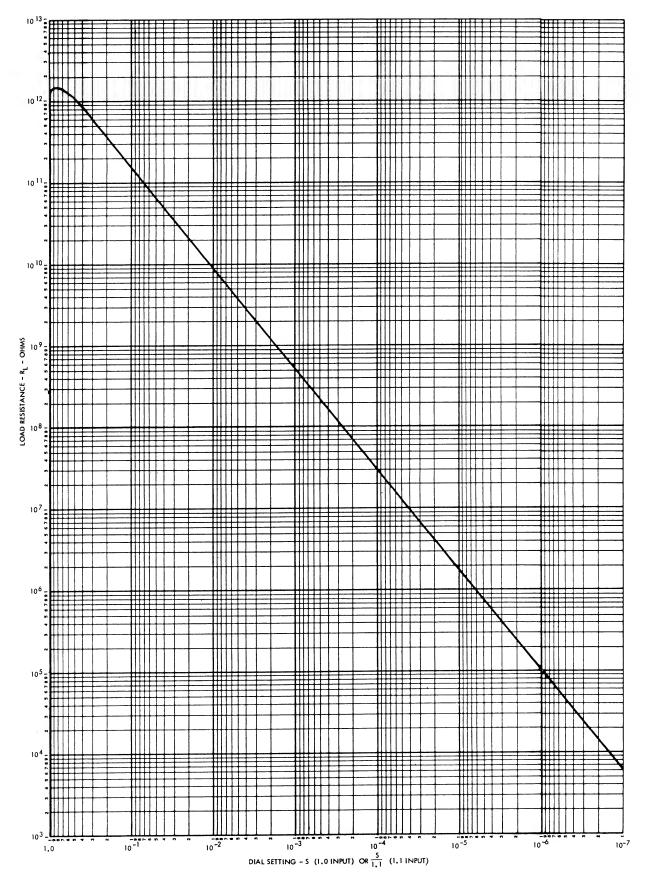


Figure 2-4. APPROXIMATE VARIATION OF MINIMUM LOAD RESISTANCE FOR 0.03 PPM OF INPUT LOADING ERROR

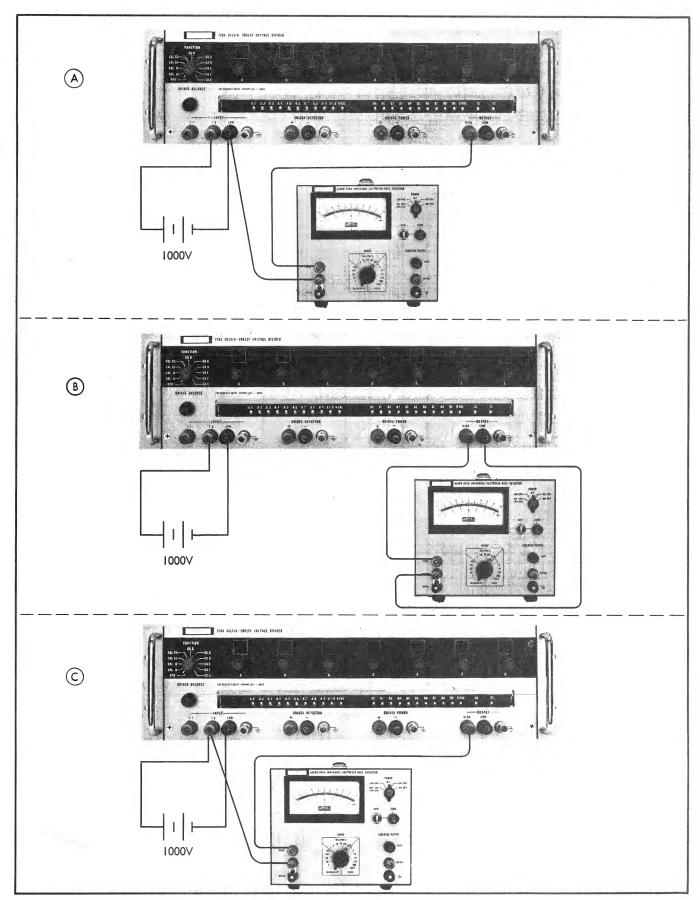


Figure 2-5. CONNECTIONS FOR DETERMINING END ERRORS

first two decades to compensate for any resistance changes caused by temperature changes or aging. Thus, the absolute linearity of the instrument is adjusted to 0.1 ppm of input. The only external test units required are a stable source of 10 volts and 20 volts such as the Fluke Model 412B and a sensitive null detector such as the Fluke Model 845AB. The procedure may be adapted easily to use batteries as the voltage source if a suitable dc power supply is not available. The procedure is as follows:

- a. Connect the null detector (845AB) to the BRIDGE DETECTOR binding posts using low thermal leads.
- b. On the Model 720A, set the FUNCTION switch to CAL A and the decade readout to .0000000.
- c. On the Model 845AB, set the range switch to 10 microvolts; set the OPR ZERO switch to ZERO and adjust for zero meter deflection. Return the OPR-ZERO switch to OPR position.
- d. Set the power supply (412B) for 20 volts output and connect it to the BRIDGE POWER binding posts.
- e. Adjust the BRIDGE BALANCE control for a null indication on the Model 845AB.
- f. Advance the "A" decade to 0.1, and adjust the associated variable resistor (A.1) to produce null, ±0.5 microvolts.

 NOTE!

As the procedure is continued, occasionally return the "A" decade switch to zero and recheck bridge balance.

- g. In turn, advance the "A" decade one position (A. 2 through A CAL) and adjust the associated variable resistor.
- h. Return the "A" decade to zero upon completion of the CAL position adjustment.
- i. Set the power supply output to 10 volts.
- j. Adjust the BRIDGE BALANCE to obtain a null.

k. Set the FUNCTION switch to CAL B, and adjust the associated variable resistor (BO) to produce a null ±1 microvolt.

NOTE!

As the procedure is continued, occasionally return the FUNCTION switch to CAL A and recheck bridge balance.

- In turn, advance the "B" decade one position (B1 through B CAL) and adjust the associated variable resistor.
- m. Return the "B" decade to zero upon completion of the CAL position adjustment.
- n. Set the FUNCTION switch to CAL S1 and adjust variable resistor S1 for a null, ±1 microvolt.
- o. Set the power supply to 20 volts.
- p. Set the "A" decade to . 0 and set the FUNCTION switch to CAL A.
- q. Adjust the BRIDGE BALANCE control for a null.
- r. Set the FUNCTION switch to CAL S2 and adjust variable resistor S2 for a null, ±0.5 microvolt.
- s. Set the FUNCTION switch to OPR and disconnect the test units. The self-calibration is complete.

2-26. CHECK POSITIONS OF THE FUNCTION SWITCH

2-27. Check positions (CK B etc.) are provided on the FUNCTION switch to permit checking the linearity of each decade from the front panel. This linearity check is a maintenance procedure. It should not be undertaken as a part of operation.

2-28. APPLICATIONS OF THE MODEL 720A

2-29. The following paragraphs give general instructions and equipment connections for calibrating a voltage divider, measuring unknown voltages, and measuring unknown resistances. Although these are by no means

TYPICAL EQUIPMENT	REQUIRED SPECIFICATIONS
DC Voltage source; John Fluke Mfg. Co. Model 332B or equivalent.	Output voltage from 0 to 1100 volts. Stability of 0.0015% per hour. Output ripple less than 40 uv rms.
DC Null Detector; John Fluke Mfg. Co. Model 845AB or equivalent.	1 uv full-scale sensitivity. 10 megohms input resistance.
Lead compensator; John Fluke Mfg. Co. Model 721A	Resolution of 0.1 milliohm.

Figure 2-6. TYPICAL ASSOCIATED EQUIPMENT FOR VOLTAGE DIVIDER CALIBRATION

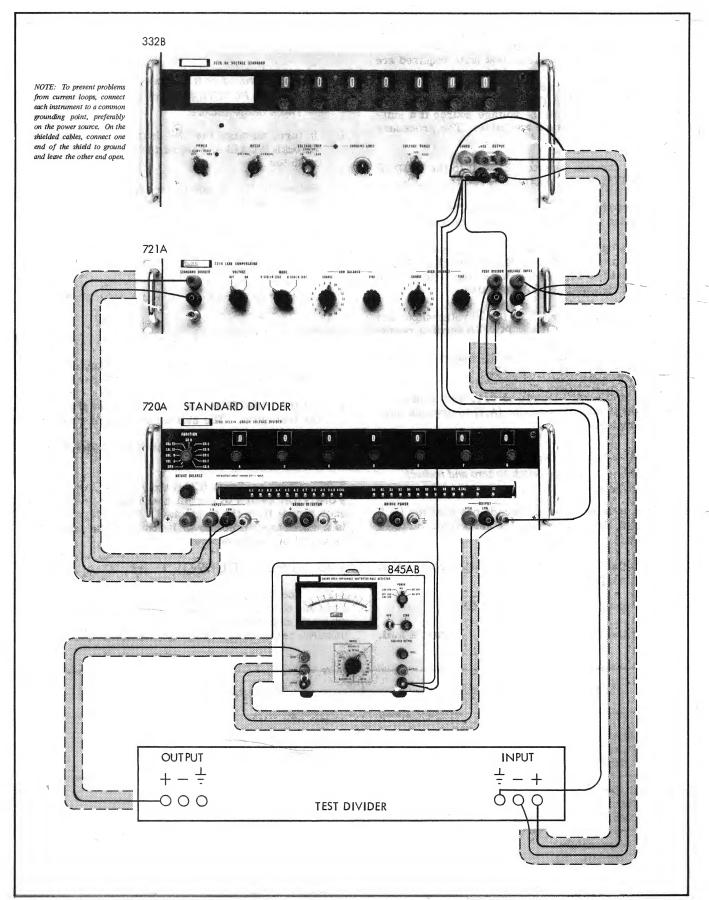


Figure 2-7. EQUIPMENT CONNECTIONS FOR CALIBRATING A VOLTAGE DIVIDER

the only applications of the instrument, they are the most common applications of a high-accuracy Kelvin-Varley divider such as the Model 720A.

2-30. Calibrating a Voltage Divider

2-31. The Model 720A in company with a dc voltage source, a null detector, and a lead compensator can be used to calibrate voltage dividers to an accuracy of 0.1 parts per million of input. Typical associated equipment for this application is listed in Figure 2-6. With this equipment, the full electrical capabilities of the Model 720A Kelvin-Varley Voltage Divider may be realized.

2-32. To calibrate a voltage divider, connect the equipment as shown in Figure 2-7 and proceed as follows:

NOTE!

Figure 2-8 is a schematic diagram of the test setup obtained by interconnecting the equipment as shown in Figure 2-7.

- a. Set both dividers to zero.
- b. Turn all equipment on and allow it to warm up until it reaches temperature equilibrium.
- Place the null detector in zero mode, adjust it for zero deflection, and return it to operating mode.
- Adjust the LOW BALANCE controls of the lead compensator to obtain a zero indication on the null detector.
- Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.

NOTE!

If the dividers are set from one calibration point to the next while the test setup is energized, the null detector meter will require several seconds to recover between readings. Measurement may be performed more rapidly if the VOLTAGE switch of the lead compensator is turned to OFF before switching. Measurement may be speeded further by turning the ZERO-OPR switch of the null detector to ZERO during switching. This prevents the transient caused by turning the voltage on, from saturating the null detector amplifier.

- f. Set both dividers to full scale and adjust the HIGH BALANCE FINE control to obtain a zero indication on the null detector.
- g. Set both dividers to zero and re-adjust the LOW BALANCE FINE control if necessary to obtain a zero indication on the null detector.
- h. Set both dividers to the first calibration point.
- Observe the null detector and adjust the Model 720A to obtain a zero indication on the null detector. The difference between the setting of the Model 720A and the nominal value of the calibration point is the error of the divider being calibrated expressed as a decimal fraction of the input.
- Find the error at each calibration point until the calibration is complete.

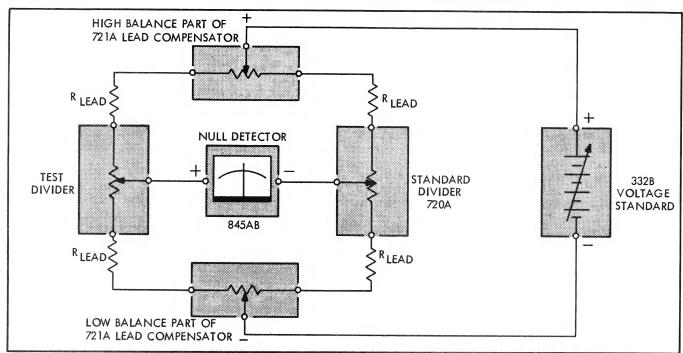


Figure 2-8. SIMPLIFIED SCHEMATIC DIAGRAM OF VOLTAGE DIVIDER CALIBRATION

TYPICAL EQUIPMENT	REQUIRED SPECIFICATIONS
DC Voltage Source; John Fluke Mfg. Co. Model 332B or equivalent.	Output voltage from 0 to 1100 volts. Stability of 0.0015% per hour. Output ripple less than 40 uv rms.
DC Null Detector (2 required); John Fluke Mfg. Co. Model 845AB or equivalent.	1 uv full-scale sensitivity. 10 megohms input resistance.
Standard Cell; Guildline Instruments Model 9152 or equivalent.	At least three saturated cells. Accuracy of 0.0005%.
DC Reference Voltage Divider; John Fluke Mfg. Co. Model 750A or equivalent.	Output accuracy of ±10 ppm. Input and output voltage. Rating of 1100V dc.

Figure 2-9. TYPICAL ASSOCIATED EQUIPMENT FOR MEASURING UNKNOWN VOLTAGES

2-33. Measuring Unknown Voltages

2-34. The Model 720A in company with a stable dc voltage source, two null detectors, a standard cell, and a reference voltage divider may be used to measure an unknown voltage with high accuracy. Typical equipment for this application is listed in Figure 2-9. With this equipment the full electrical capabilities of the Model 720A may be realized.

2-35. To measure an unknown voltage, first connect the equipment as shown in Figure 2-10. The size of wire for leads A and B should be no smaller than No. 24 and the total length should be less than 3 feet. Then measure the approximate voltage by dialing the Model 720A to .0000000 and reading the null detector on the appropriate voltage range. Proceed as follows:

- a. Open the standard cell voltage switch on the reference divider and set the standard cell voltage dials to the correct standard cell voltage.
- b. Set the reference divider input switch to the first position higher than the voltage to be measured. Set the output switch to the same position.
- c. Turn on all equipment and allow it to warm up until it reaches temperature equilibrium.
- d. Set the standard cell switch of the reference divider to momentary position and adjust the output of the dc source to obtain a null indication on null detector number 1.
- e. Adjust the readout dials of the Model 720A to obtain a null indication on null detector number 2.
- f. Calculate the unknown voltage by multiplying the input voltage of the Model 720A by the numerical setting of the readout dials. For example, if the input voltage is 100 volts and the dial setting is . 8903174, the unknown voltage is 89.03174 volts.

2-36. Simplified Method of Voltage Measurement

2-37. Voltages under 11 volts may be measured with comparable accuracy by the simpler equipment setup shown in Figure 2-12. This method standardizes the output voltage of the Model 720A by comparing it directly to a known standard cell. When used with an input of 1.1 volts, it is ideally suited to the accurate certification of standard cells. Typical associated equipment for this application is listed in Figure 2-11.

2-38. To measure the unknown voltages, connect the equipment as shown in Figure 2-12 and proceed as follows:

- a. Set the dc voltage source for an output of eleven or 1.1 volts depending on the desired range and allow to warm up.
- Set the readout dials of the Model 720A to the standard cell voltage.
- c. Connect the standard cell in place of the unknown voltage and adjust the dc source to obtain a null indication on the null detector.
- d. Disconnect the standard cell.
- e. Set the readout dials of the Model 720A to the approximate value of the unknown voltage.
- f. Connect the unknown voltage.
- g. Adjust the readout dials of the Model 720A to obtain a null indication on the null detector.
- h. Calculate the unknown voltage by multiplying by 10 or 1 depending on the range. For example, if the readout dials are set at .7500055 and the input is 11 volts, the unknown voltage is 7.500055 volts.

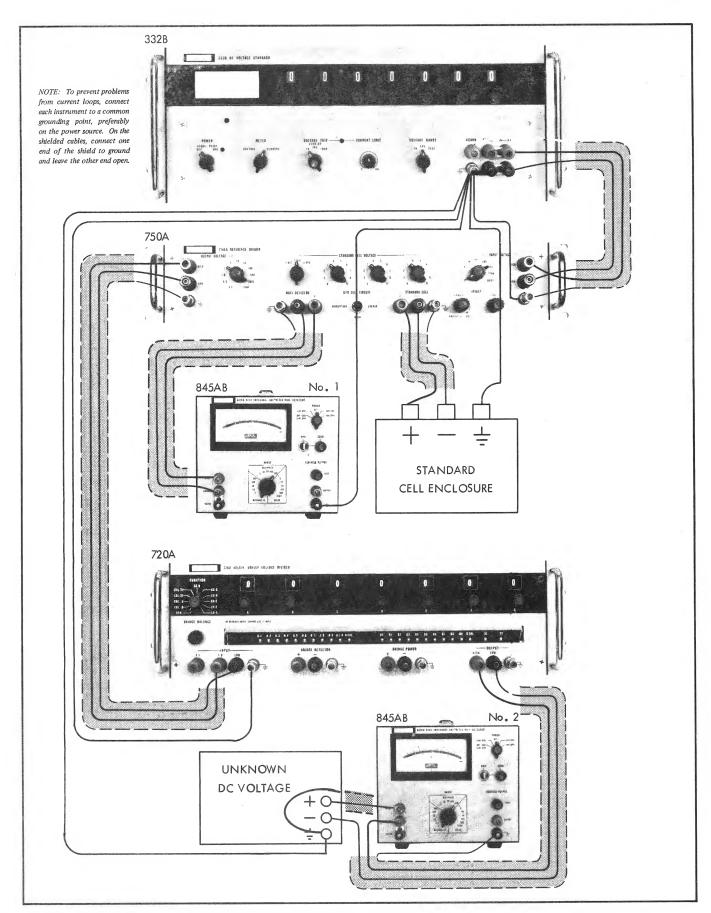


Figure 2-10. EQUIPMENT CONNECTIONS FOR VOLTAGE MEASUREMENTS (Sheet 1 of 2)

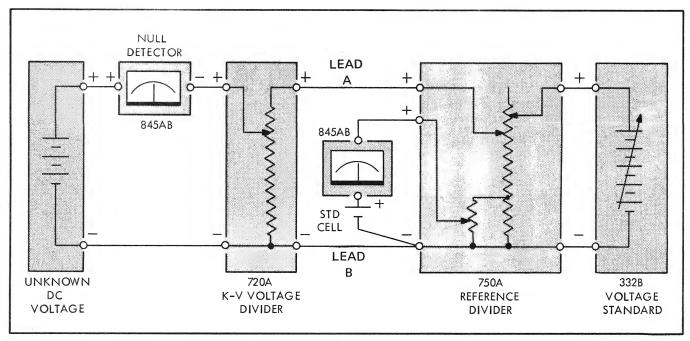


Figure 2-10. EQUIPMENT CONNECTIONS FOR VOLTAGE MEASUREMENTS (Sheet 2 of 2)

2-39. Measuring Unknown Resistance

2-40. The Model 720A may be used in a setup including a null detector, a power supply, and a standard resistor, to measure an unknown resistance with a high degree of accuracy. Typical associated equipment for this application is listed in Figure 2-13. The unknown resistance and the standard resistance should be in the same order of magnitude for the best accuracy.

2-41. To measure an unknown resistance, connect the equipment as shown in Figure 2-14 using shielded leads. Apply the positive lead from the dc voltage source to the 1.0 INPUT terminal of the Model 720A. Proceed as follows:

 P_1 , P_2 , P_3 , and P_4 = decimal ratio set on the readout dials of the Model 720A at points P_1 , P_2 , P_3 , and P_4 respectively.

If Rx + R std is greater than 100 ohms, the use of a lead compensator is desirable. If a lead compensator is used, P_1 can be made equal to 1.0000000 and P_4 can be made equal to .0000000.

$$\frac{Rx}{R \text{ std}} = \frac{1 - P_2}{P_2}$$

If lead resistance between the resistors is made insignificant in addition to using a lead compensator, then $P_2=P_3$ and the equation may be further simplified to:

$$\frac{Rx}{R \text{ std}} = \frac{1}{P} - 1$$

a. Set the dc voltage source to the desired test voltage.

CAUTION!

Do not exceed the current rating of the standard resistor.

- b. Set the readout dials of the Model 720A to zero.
- c. Connect the null detector lead to point P_1 and adjust the readout dials of the Model 720A to obtain a null indication. Record the dial reading.

TYPICAL EQUIPMENT	REQUIRED SPECIFICATIONS
DC Voltage Source; John Fluke Mfg. Co. Model 332B or equivalent.	Output voltage from 0 to 1100 volts. Stability of 0.0015% per hour. Output ripple less than 40 uv rms.
DC Null Detector John Fluke Mfg. Co. Model 845AB or equivalent.	1 uv full-scale sensitivity. 10 megohms input resistance.

Figure 2-11. TYPICAL ASSOCIATED EQUIPMENT FOR MEASURING UNKNOWN VOLTAGES

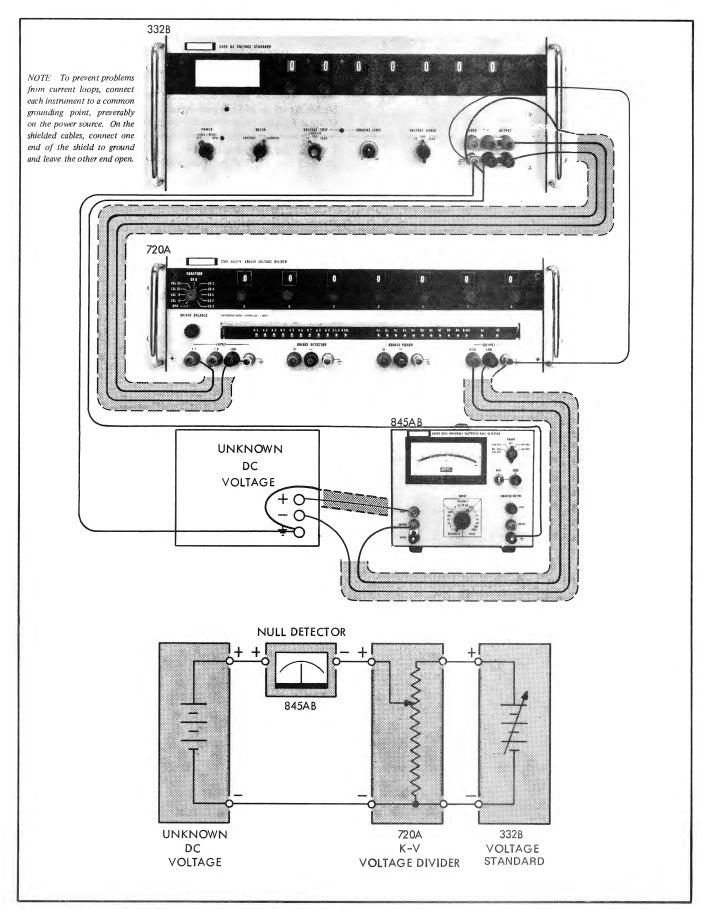


Figure 2-12. EQUIPMENT CONNECTIONS FOR SIMPLIFIED METHOD OF VOLTAGE MEASUREMENT

TYPICAL EQUIPMENT	REQUIRED SPECIFICATIONS
DC Voltage Source; John Fluke Mfg. Co. Model 332B or equivalent.	Output voltage from 0 to 1100 volts. Stability of 0.0015% per hour. Output ripple less than 40 uv rms.
DC Null Detector John Fluke Mfg. Co. Model 845AB or equivalent.	1 uv full-scale sensitivity. 10 megohms input resistance.
Standard resistor.	

Figure 2-13. TYPICAL ASSOCIATED EQUIPMENT FOR MEASURING UNKNOWN RESISTANCE RATIOS

- d. Move the null detector lead to point P_2 , adjust the readout dials to obtain a null, and record the dial reading.
- e. Move the null detector lead to point P_3 , adjust the readout dials to obtain a null, and record the reading.
- f. Move the null detector lead to point P_4 , adjust the dials to obtain a null, and record the dial reading.
- g. Calculate the unknown resistance from the following equation.

$$\frac{Rx}{R \text{ std}} = \frac{P_1 - P_2}{P_3 - P_4}$$

where:

Rx = unknown resistance R std = standard resistance

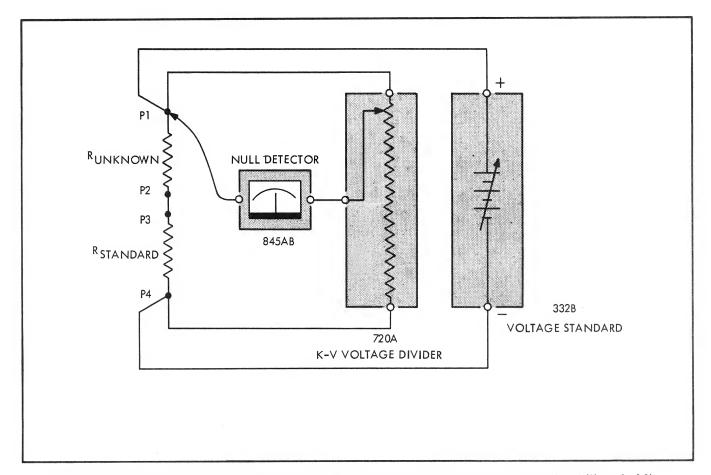


Figure 2-14. EQUIPMENT CONNECTIONS FOR DETERMINING AN UNKNOWN RESISTANCE VALUE (Sheet 1 of 2)

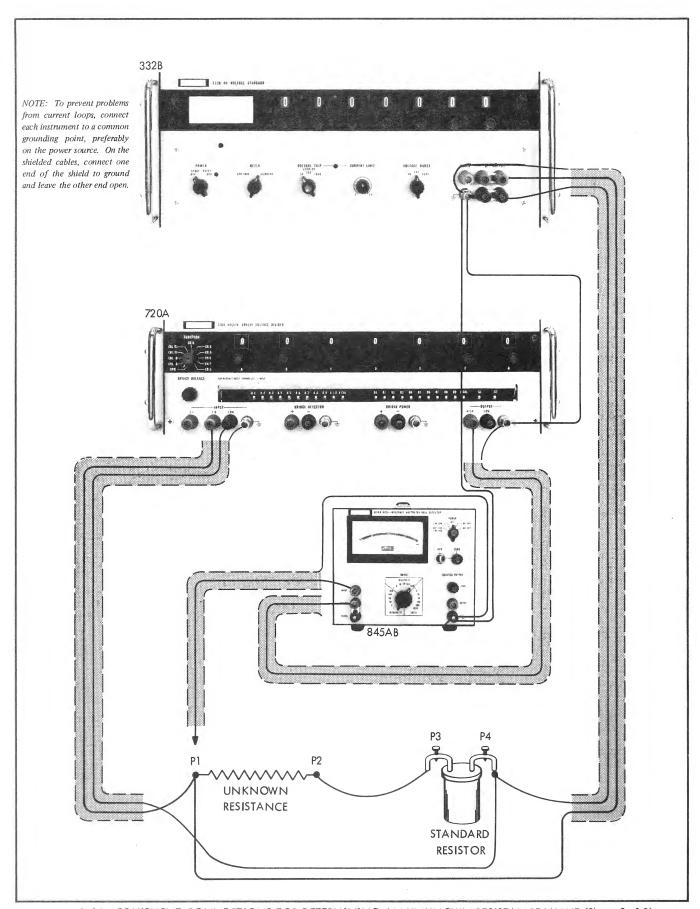


Figure 2-14. EQUIPMENT CONNECTIONS FOR DETERMINING AN UNKNOWN RESISTANCE VALUE (Sheet 2 of 2)

Section 3

Theory of Operation

3-1. INTRODUCTION

3-2. The Kelvin-Varley divider is a resistive circuit used primarily as a ratio standard. It is capable of dividing the input voltage with high resolution, usually to six or seven decimal places, and with high accuracy, usually a few parts per million.

3-3. THE BASIC CIRCUIT

- 3-4. Figure 3-1 is a simplified schematic diagram of a basic Kelvin-Varley divider. This simplified divider is capable of dividing the input voltage into 10,000 parts. It consists of four decades or resistive dividers each of which divides its input voltage into 10 equal parts $(10^4 = 10,000)$.
- For a decade to divide the voltage across it into 10 equal parts it must consist of 10 equal resistances. Placing the resistance of succeeding decade in parallel with a portion of the resistance of a decade, reduces the effective resistance of that portion. Referring to Figure 3-1, notice that the shunted resistance in the first decade is 20 kilohms and that each of the other steps is 10 kilohms. The 20 kilohms in the first decade is shunted by the 20 kilohms total effective resistance of the second decade resulting in a total effective resistance of 10 kilohms for that step. Thus all steps are kept equal. Each step of the second decade is two kilohms. The four kilohms spanned by the switch contacts is shunted by the four kilohms effective resistance of the third decade. Similarly 800 ohms of the third decade is shunted by the 800 ohms total resistance of the fourth decade.

3-6. CIRCUIT REFINEMENTS

3-7. Although the simplified Kelvin-Varley divider shown in Figure 3-1 shows all of the essential details of the basic circuit, a number of common design refinements should be mentioned. The latter decades may employ step resistors which are all of the same value and a shunt across the entire decade to reduce the effective decade resistance to the proper value. In Figure 3-1, this could be accomplished by using 400 ohm resistors in the fourth decade with a 1000 ohm shunt across the decade to reduce the effective resistance of

the decade to 800 ohms. This avoids the necessity of using resistors of very small value in the latter decades. Usually each step of at least the first decade will consist of two equal resistors matched for equal but opposite temperature coefficients. This matching tends to produce a zero temperature coefficient for each step and for the entire decade, which reduces the nonlinearity caused by uneven temperature when power is applied. Some Kelvin-Varley dividers have adjustable trimmer resistors in the first, or even the second and third decades to permit compensation for drift and changes of ambient temperature. Overranging capability is provided in some circuits by adding an additional step of resistance and a 1.1 input terminal at the upper end of the first decade. In some dividers a small series resistance is added between the lower end of the divider string and the low input terminal to compensate for contact and wiring resistance bringing the low output voltage at zero setting to the same value as the low input voltage. Although these refinements improve the capability of the circuit, it operates in the same manner with them as without them.

3-8. THE MODEL 720A

- 3-9. The Model 720A is a seven-dial Kelvin-Varley divider with overranging and adjustable trimmers in the first three decades. The low output is compensated by a small resistance in series with the low input terminal. The input resistance (total effective resistance of the first decade is 110 kilohms at the 1.1 input terminal or 100 kilohms at the 1.0 input terminal. Resistors of equal value and fixed decade shunts are used in the last four decades to avoid using very small resistance values.
- 3-10. Design characteristics of the Model 720A which are not commonly found in Kelvin-Varley dividers include adjustable shunts in the first three decades, a built-in Wheatstone bridge, and switching to permit linearity adjustment (self-calibration) from the front panel. In addition, internal switching provides access to the second through the seventh decades so the linearity of any decade may be checked against a 10-step divider from the front panel.

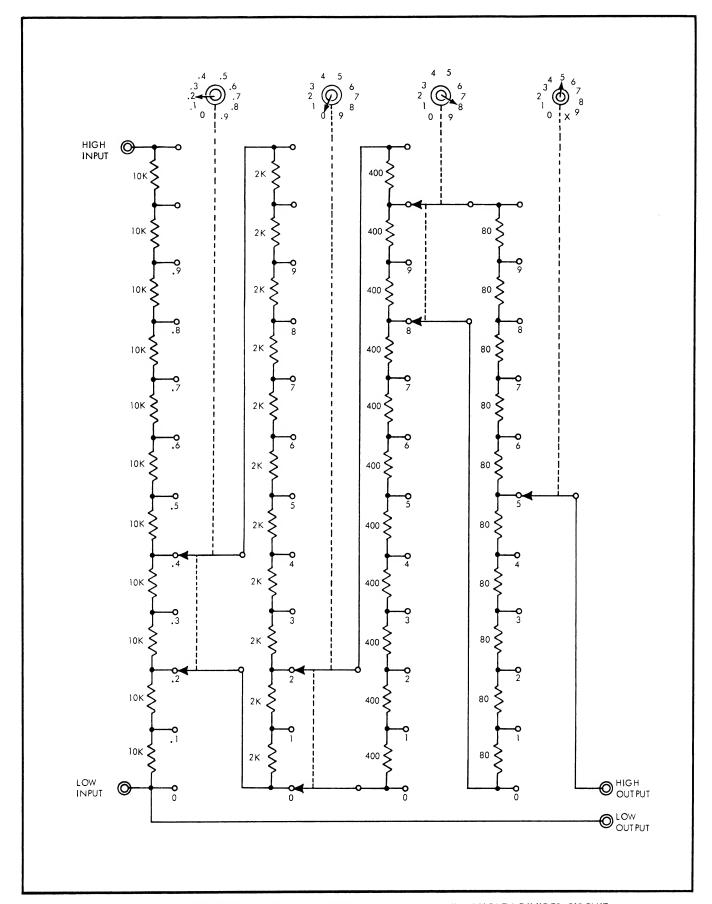


Figure 3-1. SIMPLIFIED SCHEMATIC DIAGRAM OF BASIC KELVIN-VARLEY DIVIDER CIRCUIT

Section 4 Maintenance

4-1. INTRODUCTION

- 4-2. This section contains the instructions and information required for maintenance of the Model 720A Kelvin—Varley Divider. Instructions are included for preventive maintenance, testing and repair of the instrument. If repair is beyond the capability of the user, it is recommended that the instrument be returned to the manufacturer. All maintenance procedures except the replacement of factory selected resistors and resistors housed in the oil tank are within the capability of a skilled technician if the listed test equipment is available.
- The ratio accuracy of 0.1 ppm of the Model 720A 4-3. is guaranteed for one year after shipment from the factory provided the instrument is regularly self-calibrated in accordance with paragraph 2-24 and is operated in the same environment in which it is self-calibrated. The instrument also must meet the requirements of the Leakage Resistance Test, paragraph 4-8. In the self-calibration procedure, all resistors on the A and B decades are adjusted to be equal to each other by substituting each in turn into the self-contained resistance bridge. The Linearity Test given in paragraph 4-14 should be performed once each year to verify instrument performance. If testing and calibration are beyond the capability of the user, these services may be obtained from a commercial calibration laboratory or from the manufacturer.

4-4. TEST EQUIPMENT REQUIRED FOR MAINTENANCE

4-5. The test equipment required for maintenance is listed in Figure 4-1. Equivalent or similar units may be substituted for those listed providing they have the required specifications listed in the figure.

4-6. PREVENTIVE MAINTENANCE

4-7. Preventive maintenance of the Model 720A consists of leakage resistance testing, cleaning, switch contact lubrication, and linearity testing. The frequency with which preventive maintenance procedures should be scheduled depends upon the user's requirements and the environment of the instrument. In an air conditioned standards laboratory, there will be little contamination of surfaces within this instrument and therefore testing and cleaning will seldom be required. In a contaminated atmosphere, frequent testing and cleaning may be required to maintain the accuracy of the instrument.

4-8. Leakage Resistance Tests

4-9. The need for cleaning can be determined without removing the cover from the Model 720A by performing

RECOMMENDED EQUIPMENT	SPECIFICATIONS REQUIRED
DC Voltage Source John Fluke Mfg. Co. Model 332B or Model 412B	Source of 0 to 1100 vdc. Accuracy at least 0.25% Stability at least 0.005% per hour.
DC Null Detector John Fluke Mfg. Co. Model 845AB	Sensitivity at least 10 microvolts full scale. 10 Megohm input Resistance.
Lead Compensator John Fluke Mfg. Co. Model 721A	Resolution of 0.1 milliohm. Ratio capability of 110:1
Standard Divider John Fluke Mfg. Co. Model 720A	Ratio accuracy of 0.1 ppm of input.
Standard Divider (11 Steps)	Ratio accuracy of 0.05 ppm of input
Decade Resistance Standard Electro Scientific Industries Model RS925A	4007.6 ohms, 10,000 ohms Accuracy of ±20 ppm

Figure 4-1. TEST EQUIPMENT REQUIRED FOR MAINTENANCE

the simple leakage resistance test described in this paragraph. This test should also be performed after cleaning to assure that all contamination has been removed. To measure leakage resistance, proceed as follows:

- a. Place the Model 720A on a sheet of dielectric.
- b. Use teflon insulated wire to connect the Model 720A, a 1000-volt source (Model 332B), and a null detector (Model 845AB) as shown in Figure 4-2.
- c. Connect a shunt resistor across the input of the null-detector to bring its input resistance to one megohm on the one millivolt range. The value required for the Model 845AB is 1.1 megohms.
- d. Turn on the 1000-volt supply and read the null detector. An indication of 1 millivolt corresponds to leakage resistance of 10¹² ohms. If the indication is more than 1 millivolt, the leakage resistance is too low and corrective measures must be taken. If repeated cleaning fails to correct the problem, troubleshooting must be undertaken.

4-10. CLEANING

4-11. When the Model 720A is properly cared for and

kept in a controlled atmosphere, cleaning will seldom be required. However, any contamination, particularly oil, in the instrument can contribute to reduced leakage resistance which will impair accuracy. Special care has been taken in the design and manufacture of the instrument to prevent leakage. The voltage dial switches are supported by Lexan spacers, and the circuit board is coated with a moisture sealant and isolated from the chassis by polyethelene grommets. These insulators and the switches can be contaminated easily by handling or by airborne contaminants. Dust may be removed with dry oil-free air at a pressure of 15 pounds per square inch or less. To remove oil, place the instrument on its side, place paper towels under it and spray with denatured anhydrous ethyl alcohol, Crown SPRA-TOOL No. 8011 or equivalent. When dry, perform switch contact lubrication, paragraph 4-12. After cleaning and drying, the leakage resistance test should be performed to assure that the excessive leakage has been corrected.

4-12. Switch Contact Lubrication

4-13. Corrosion of switch contacts can cause high contact resistance in one or more positions resulting in an impairment of linearity. If evidence of this condition is present and exercising the switch fails to correct it, the switch contact should be lubricated with a special purpose switch lubricant. The product recommended for this purpose is Rykon lubricant No. 2 EP (American Oil Co.) mixed with Tuluol. It should be carefully applied in a very thin film with a camel's hair brush.

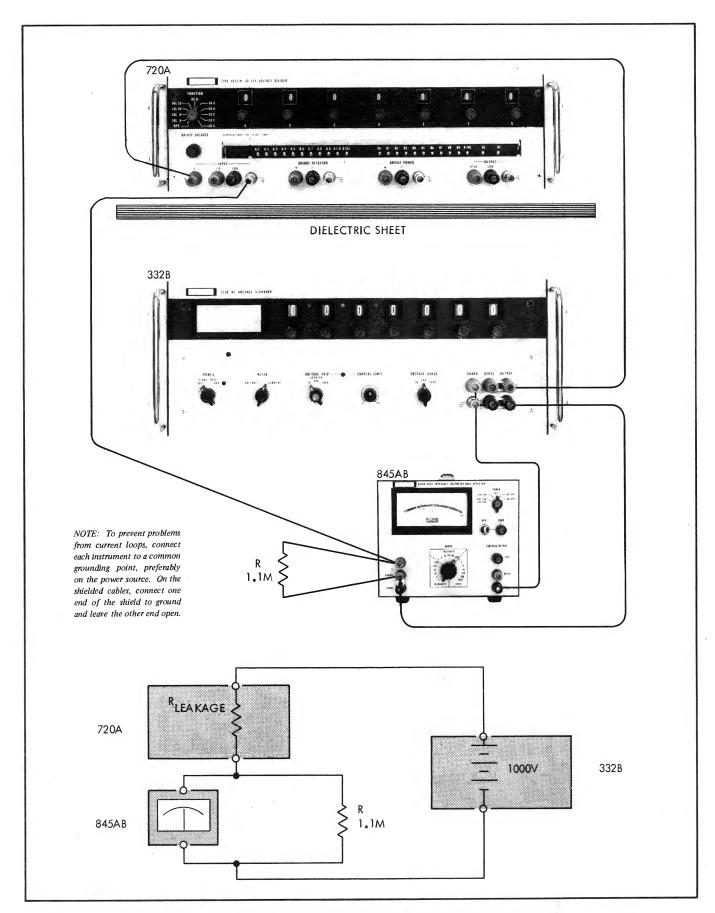


Figure 4-2. EQUIPMENT CONNECTIONS FOR LEAKAGE RESISTANCE TEST

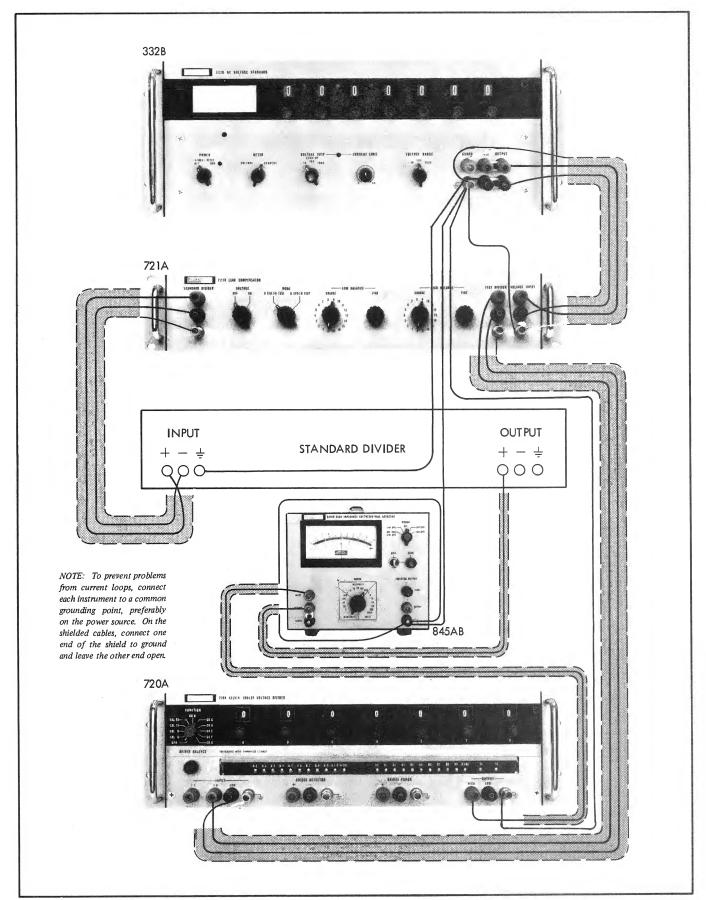


Figure 4-3. EQUIPMENT CONNECTIONS FOR LINEARITY COMPARISON TEST

CAUTION!

Great care should be used to avoid excessive use of contact lubricant on the switches of the Model 720A. The contacts should not be lubricated unless there is evidence of irregular operation.

Before applying the lubricant, clean the switch following the instructions in paragraph 4-10. Only a minute amount of lubricating fluid should be applied. After application, exercise the switch by rotating it through all positions several times.

4-14. Linearity Testing

4-15. The design of the 720A Voltage Divider is such that if the instrument is self-calibrated, if the leakage resistance is low, and if the switch contacts display repeatable contact resistance, the divider will meet its linearity specifications. Because of the extremely tight over-all specification (0.1 PPM of input) very few laboratories will have both the necessary equipment and the required technical skills to prove this. The following linearity test using a second Model 720A as a standard is therefore intended only to indicate gross errors (0.2 PPM of input) in the first decade and to prove specification on the lower decades. The customer who hopes to prove more than this is referred to the following articles and papers:

- Andrew F. Dunn, "Calibration of a Kelvin-Varley Voltage Divider," National Research Council Report No. 7863.
- M. L. Morgan and J. C. Riley, "Calibration of a Kelvin-Varley Standard Divider," IRE

Trans. on Instrumentation, vol. 1-9, pp 237-243; Sept. 1960.

4-16. To compare divider linearity, connect the equipment as shown in Figure 4-3 and proceed as follows:

NOTE!

Figure 4-4 is a schematic diagram of the test setup obtained by interconnecting the equipment as shown in Figure 4-3.

- a. Self-calibrate the Model 720A. (See paragraph 2-24 in Section II).
- b. Set both dividers to zero.
- c. Set the voltage source to the desired test voltage, turn on all equipment and allow it to warm up until it reaches temperature equilibrium.
- d. Place the null detector in the zero mode, adjust it for zero deflection, and return it to operating mode.
- e. Adjust the LOW BALANCE controls of the lead compensator to obtain a zero indication on the null detector.
- f. Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.

NOTE!

If the dividers are set from one calibration point to the next while the test setup is energized, the null detector meter will require several seconds to recover between readings. Measurement may

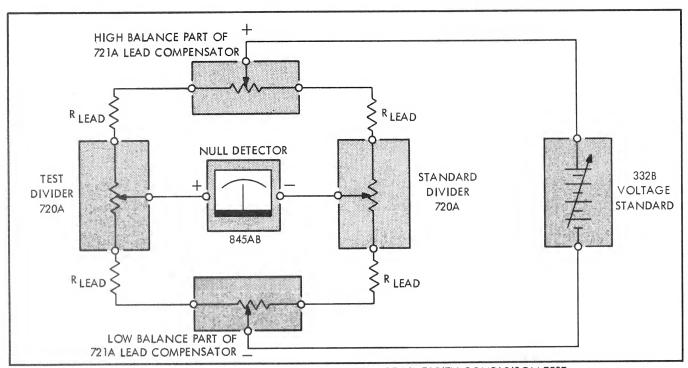


Figure 4-4. SIMPLIFIED SCHEMATIC DIAGRAM OF LINEARITY COMPARISON TEST

be performed more rapidly if the VOLTAGE switch of the lead compensator is turned to OFF before switching. Measurement may be speeded further by turning the ZERO-OPR switch of the null detector to ZERO during switching. This prevents the transient caused by turning the voltage on from saturating the null detector amplifier.

- g. Set both dividers to full scale and adjust the HIGH BALANCE FINE control to obtain a zero indication on the null detector.
- h. Set both dividers to zero and re-adjust the LOW BALANCE FINE control if necessary to obtain a zero indication on the null detector.
- i. Set the null detector to the desired sensitivity.
- j. Set both dividers to the first comparison point and adjust the standard divider for a near zero indication on the null detector. The dial settings of the two dividers plus the null detector reading shall agree within a tolerance of 0.2 PPM. This criterion is applicable for input voltages of 100 volts or less.
- k. Continue to compare each setting of each decade until the comparison is complete. The following dial setting combinations should be checked on each decade.

0 all zeros	
1 all zeros	1 (dial 09 and all 9 ^S except X
2 all zeros	in last) 2 (dial 19 and all $9^{\underline{S}}$ except X
3 all zeros	in last) 3 (dial 29 and all $9^{\underline{S}}$ except X
4 all zeros	in last) 4 (dial 39 and all 9 ^S except X
5 all zeros	in last) 5 (dial 49 and all 9 ^{<u>S</u> except X}
6 all zeros	in last) 6 (dial 59 and all 9 ^{<u>S</u> except X}
7 all zeros	in last) 7 (dial 69 and all $9^{\underline{S}}$ except X
8 all zeros	in last) 8 (dial 79 and all 9 [§] except X
9 all zeros	in last) 9 (dial 89 and all 9 ^S except X
1.0 all zeros	in last) 10 (dial 99 and all 9 ^S except X
	in last) 1.1 (dial 1.09 and all $9^{\underline{S}}$ except X
	in last)

4-17. Decade Linearity Testing

4-18. The CK B through CK G positions of the FUNCTION switch are provided to permit access to the individual decades of the Model 720A under test so that each may be checked against the first decade of the standard divider. To test the linearity of each decade individually, proceed as follows:

a. Change the test setup to that shown in Figure 4-5.

NOTE!

Figure 4-6 is a schematic diagram of the test setup obtained by interconnecting the equipment as shown in Figure 4-5.

- b. Turn the FUNCTION switch to CK B.
- c. Set the standard divider to zero.
- d. Set the divider under test to 1.0 000000.
- e. Set the voltage source to the desired test voltage.

CAUTION!

Do not exceed the maximum test voltages listed in Figures 4-7 through 4-12.

- Place the null detector in the zero mode, adjust it for zero deflection, and return it to operating mode.
- g. Adjust the LOW BALANCE controls of the lead compensator to obtain a zero indication on the null detector.
- h. Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.

NOTE!

If the dividers are set from one calibration point to the next while the test setup is energized, the null detector meter will require several seconds to recover between readings. Measurement may be performed more rapidly if the VOLTAGE switch of the lead compensator is turned to OFF before switching. Measurement may be speeded further by turning the ZERO-OPR switch of the null detector to ZERO during switching. This prevents the transient caused by turning the voltage on, from saturating the null detector amplifier.

- Set the standard divider to full scale.
- j. Set the divider under test to 1.0 99999X.
- k. Adjust the HIGH BALANCE FINE control to obtain a zero indication on the null detector.
- Set the divider under test back to <u>1.0</u> 000000 and set the standard divider back to zero.
- m. Re-adjust the LOW BALANCE FINE control if necessary to obtain a zero indication on the null detector.
- Set the null detector for the desired sensitivity and make the linearity measurements given in Figure 4-7. The null detector indications must be

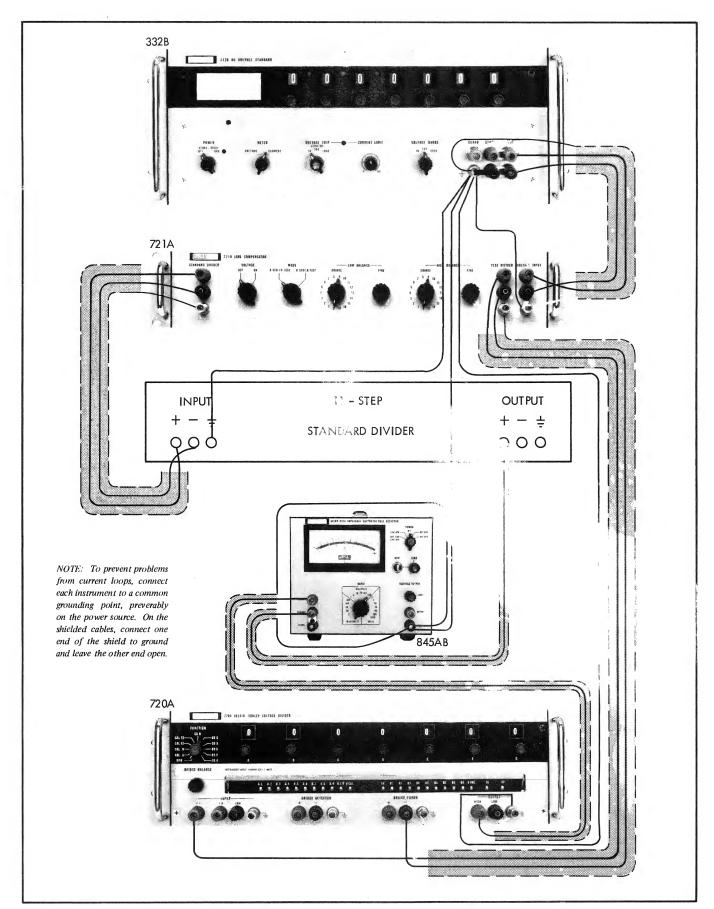


Figure 4-5. EQUIPMENT CONNECTIONS FOR DECADE LINEARITY TEST

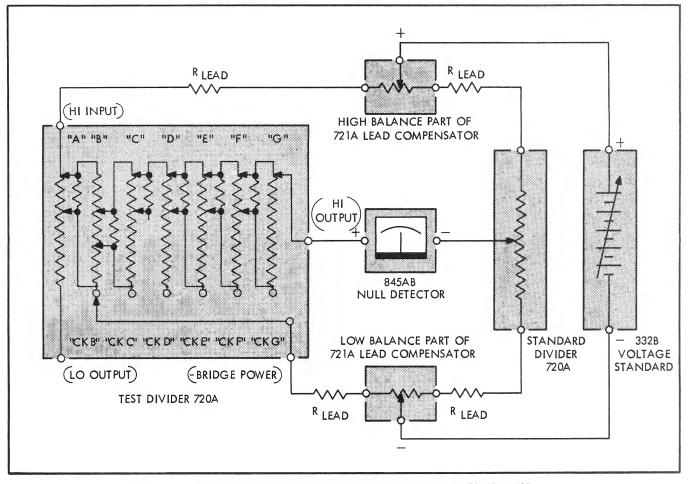


Figure 4-6. SIMPLIFIED SCHEMATIC DIAGRAM OF DECADE LINEARITY TEST

within the limits listed in the Permissible Deviation column.

NOTE!

An indication beyond these limits is a symptom of trouble within the instrument. Refer to the troubleshooting instructions to determine the nature of the fault.

- Set the voltage source to the desired voltage for testing the "C" decade.
- p. Turn the FUNCTION switch to CK C.
- q. Set the standard divider to zero.
- r. Set the divider under test to 1.0 900000.
- s. Place the null detector in the zero mode, adjust it for zero deflection, and return it to operating mode.
- Adjust the LOW BALANCE CONTROLS of the lead compensator to obtain a zero indication on the null detector.

- u. Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.
- v. Set the standard divider to full scale.
- w. Set the divider under test to 1.0 99999X.
- x. Adjust the HIGH BALANCE FINE control to obtain a zero indication on the null detector.
- y. Set the divider under test back to 1.0 900000 and set the standard divider back to zero.
- z. Re-adjust the LOW BALANCE FINE control if necessary to obtain a zero indication on the null detector.
- aa. Set the null detector for the desired sensitivity and make the linearity measurements listed in Figure 4-8
- ab. Set the voltage source to the desired test voltage for testing "D" Decade.
- ac. Turn the FUNCTION switch to CK D.

SETTINGS		PERMISSIBLE				
STANDARD DIVIDER	720A	DEVIATION PPM of INPUT to "B" DECADE	MAX. TEST VOLTAGE			
0	<u>1.0</u> 000000	0	100V			
.1	<u>1. 0</u> 100000	0.38				
. 2	<u>1. 0</u> 200000	0. 45				
. 3	<u>1. 0</u> 300000	0. 50				
. 4	<u>1. 0</u> 400000	0.54				
. 5	<u>1. 0</u> 500000	0. 57				
. 6	<u>1. 0</u> 600000	0. 60				
. 7	<u>1. 0</u> 700000	0. 63				
. 8	<u>1. 0</u> 800000	0.65				
. 9	<u>1.0</u> 900000	0.67				
. 999999 x	<u>1.0</u> 99999X	0				
. 9	<u>1.0</u> 89999X	0. 67				
. 8	<u>1. 0</u> 79999X	0.65				
. 7	<u>1.0</u> 69999X	0.63				
. 6	<u>1. 0</u> 59999X	0.60				
. 5	<u>1. 0</u> 49999X	0.57				
. 4	<u>1.0</u> 39999X	0.54				
. 3	<u>1.0</u> 29999X	0.50				
. 2	<u>1.0</u> 19999X	0.45				
.1	<u>1.0</u> 09999X	0.38	•			

Figure 4-7. "B" DECADE LINEARITY TEST

- ad. Set the standard divider to zero.
- ae. Set the divider under test to $\underline{1.0}$ 990000.
- af. Place the null detector in the zero mode, adjust it for zero deflection, and return it to operating mode.
- ag. Adjust the LOW BALANCE controls of the lead compensator to obtain a zero indication on the null detector.
- ah. Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.
- ai. Set the standard divider to full scale.

- aj. Set the divider under test to 1.0 99999X.
- ak. Adjust the HIGH BALANCE FINE control to obtain a zero indication on the null detector.
- al. Set the divider under test back to <u>1.0</u> 990000 and set the standard divider back to zero.
- am. Re-adjust the LOW BALANCE FINE control if necessary to obtain a zero indication on the null detector.
- an. Set the null detector for the desired sensitivity and make the linearity measurements given in Figure 4-9. The null detector indications must be within the limits listed in the "permissible deviation" column.

SETT	SETTINGS		
STANDARD DIVIDER	720A	PERMISSIBLE DEVIATION PPM of INPUT to "C" DECADE	MAX. TEST VOLTAGE
0	<u>1.0</u> 900000	0	100V
.1	<u>1.0</u> 910000	1.4	, ,
. 2	<u>1.0</u> 920000	1.7	
. 3	<u>1.0</u> 930000	1.9	
. 4	1.0 940000	2.1	
. 5	<u>1.0</u> 950000	2.3	
. 6	<u>1.0</u> 960000	2.4	4
.7	<u>1.0</u> 970000	2.5	
. 8	<u>1.0</u> 980000	2.7	
. 9	<u>1.0</u> 990000	2.8	!
. 999999 x	1.0 99999X	0	
. 9	1.0 98999X	2.8	
. 8	1.0 97999X	2.7	
.7	1.0 96999X	2.5	
. 6	1.0 95999X	2.4	
. 5	1.0 94999X	2.3	
. 4	1.0 93999X	2.1	
.3	<u>1.0</u> 92999X	1.9	
. 2	1.0 91999X	1.7	
.1	<u>1.0</u> 90999X	1.4	₩

Figure 4-8. "C" DECADE LINEARITY TEST

- ao. Turn the FUNCTION switch to CK E.
- ap. Set the standard divider to zero.
- aq. Set the divider under test to 1.0 999000.
- ar. Place the null detector in the zero mode, adjust it for zero deflection, and return it to operating mode.
- as. Adjust the LOW BALANCE controls of the lead compensator to obtain a zero indication on the null detector.
- at. Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.
- au. Set the standard divider to full scale.
- av. Set the divider under test to 1.0 99999X.
- aw. Adjust the HIGH BALANCE FINE control to obtain a zero indication on the null detector.
- ax. Set the divider under test back to 1.0 999000 and set the standard divider back to zero.

SETTINGS		PERMISSIBLE	
STANDARD DIVIDER	720A	DEVIATION PPM of INPUT to "D" DECADE	MAX. TEST VOLTAGE
0	<u>1.0</u> 990000	0	10V
. 1	<u>1.0</u> 991000	6.0	
. 2	1.0 992000	7.5	
. 3	<u>1.0</u> 993000	8. 6	
. 4	<u>1.0</u> 994000	9.5	
. 5	<u>1.0</u> 995000	10. 2	
. 6	<u>1.0</u> 996000	10. 8	
. 7	1.0 997000	11.4	
. 8	1.0 998000	12.0	
. 9	<u>1.0</u> 999000	12.5	
. 999999X	<u>1.0</u> 99999X	0	
. 9	<u>1.0</u> 99899X	12.5	
. 8	1.0 99799X	12.0	
.7	<u>1.0</u> 99699X	11.4	
. 6	1.0 99599X	10.8	
. 5	<u>1.0</u> 99499X	10. 2	
. 4	<u>1.0</u> 99399X	9. 5	
. 3	$\underline{1.0}$ 99299X	8.6	
. 2	1.0 99199X	7.5	
. 1	<u>1. 0</u> 99099X	6.0	. ↓

Figure 4-9. "D" DECADE LINEARITY TEST

- ay. Re-adjust the LOW BALANCE FINE control if necessary to obtain a zero indication on the null detector.
- az. Set the null detector for the desired sensitivity and make the linearity measurement given in Figure 4-10. The null detector indications must be within the limits listed in the "permissible deviation" column.
- ba. Turn the FUNCTION switch to CK F.
- bb. Set the standard divider to zero.
- bc. Set the divider under test 1.0 999900.

- bd. Place the null detector in the zero mode, adjust it for zero deflection, and return it to operating mode.
- be. Adjust the LOW BALANCE controls of the lead compensator to obtain a zero indication on the null detector.
- bf. Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.
- bg. Set the standard divider to full scale.
- bh. Set the divider under test to $\underline{1.0}$ 99999X.
- bi. Adjust the HIGH BALANCE FINE control to obtain a zero indication on the null detector.

SETTINGS		DEDMICCIDIE				
STANDARD DIVIDER	720A	PERMISSIBLE DEVIATION PPM of INPUT to "E" DECADE	MAX. TEST VOLTAGE			
0	<u>1.0</u> 999000	0	10V			
. 1	<u>1.0</u> 999100	28				
. 2	<u>1.0</u> 999200	35				
. 3	<u>1.0</u> 999300	40				
. 4	1.0 999400	44				
. 5	<u>1.0</u> 999500	47				
. 6	1.0 999600	50				
.7	1.0 999700	53				
. 8	<u>1.0</u> 999800	55				
. 9	<u>1.0</u> 999900	57				
. 999999X	1.0 999990	0				
. 9	<u>1.0</u> 99989X	57				
. 8	<u>1.0</u> 99979X	55				
. 7	1.0 99969X	53				
. 6	1.0 99959X	50				
. 5	1.0 99949X	47				
. 4	1.0 99939X	44				
. 3	1.0 99929X	40				
. 2	1.0 99919X	35	3			
. 1	<u>1.0</u> 99909X	28				

Figure 4-10. "E" DECADE LINEARITY TEST

- bj. Set the divider under test back to <u>1.0</u> 999900 and set the standard divider back to zero.
- bk. Re-adjust the LOW BALANCE FINE control if necessary to obtain zero indication on the null detector.
- bl. Set the null detector for the desired sensitivity and make the linearity measurements given in Figure 4-11. The null detector indications must be within the limits listed in the "permissible deviation" column.
- bm. Turn the FUNCTION switch to CK G.
- bn. Set the standard divider to zero.

- bo. Set the divider under test to 1.0 999990.
- bp. Place the null detector in the zero mode, adjust it for zero deflection, and return it to operating mode.
- bq. Adjust the LOW BALANCE controls of the lead compensator to obtain a zero indication on the null detector.
- br. Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.
- bs. Set the standard divider to full scale.
- bt. Set the divider under test to 1.0 99999X.

SETTINGS		PERMISSIBLE				
STANDARD DIVIDER	720A	DEVIATION PPM of INPUT to "F" DECADE	MAX. TEST VOLTAGE			
0	<u>1.0</u> 999900	0	10V			
.1	<u>1.0</u> 999910	130				
. 2	<u>1.0</u> 999920	160				
. 3	<u>1.0</u> 999930	180				
. 4	<u>1.0</u> 999940	200				
. 5	<u>1.0</u> 999950	220				
. 6	<u>1.0</u> 999960	230				
.7	<u>1.0</u> 999970	240				
.8	1.0 999980	260				
. 9	1.0 999990	270				
. 999999x	<u>1.0</u> 99999X	0				
. 9	<u>1.0</u> 99998X	270	,			
. 8	1.0 99997X	260				
.7	<u>1.0</u> 99996X	240				
. 6	<u>1.0</u> 99995X	230				
. 5	<u>1.0</u> 99994X	220				
.4	1.0 99993X	200				
.3	<u>1.0</u> 99992X	180				
. 2	<u>1.0</u> 99991X	160				
.1	<u>1.0</u> 99990X	130				

Figure 4-11. "F" DECADE LINEARITY TEST

- bu. Adjust the HIGH BALANCE FINE control to obtain a zero indication on the null detector.
- by. Set the divider under test back to $\underline{1.0}$ 999990 and set the standard divider back to zero.
- bw. Re-adjust the LOW BALANCE FINE control if necessary to obtain a zero indication on the null detector.
- bx. Set the null detector for the desired sensitivity and make the linearity measurements given in Figure 4-12. The null detector indications must be within the limits listed in the "permissible deviation" column.
- by. Disconnect the test equipment and return the FUNC-

TION switch to OPR position; the decade linearity tests are complete.

4-19. CALIBRATION

4-20. Calibration of the Model 720A consists of calibrating two standard resistance arms of the internal Wheatstone bridge and calibrating the first three decades. The bridge arms require calibration only if the BRIDGE BALANCE control has insufficient range to balance the bridge during divider calibration.

4-21. Divider Calibration

4-22. This procedure is used to adjust the linearity of the "A", "B" and "C" decades of the Model 720A so

SET	rings	PERMISSIBLE	
STANDARD DIVIDER	720A	DEVIATION PPM of INPUT to "G" DECADE	MAX. TEST VOLTAGE
0	<u>1.0</u> 999990	0	10V
.1	<u>1.0</u> 999991	600	
. 2	<u>1.0</u> 999992	750	
. 3	<u>1.0</u> 999993	860	
. 4	<u>1.0</u> 999994	950	
. 5	<u>1.0</u> 999995	1020	
. 6	<u>1.0</u> 999996	1080	
.7	<u>1.0</u> 999997	1140	
. 8	<u>1.0</u> 999998	1200	
. 9	<u>1.0</u> 999999	1250	
. 999999 x	<u>1.0</u> 99999X	0	+

Figure 4-12. "G" DECADE LINEARITY TEST

that any readout setting is accurate within 0.1 ppm of input. This procedure consists of two parts, calibration of the "C" decade and the "S3" shunt, and calibration of the "A" and "B" decades, and their shunts. The latter is the self calibration procedure which is performed from the front panel.

4-23. To calibrate the "C" decade and "S3" shunt proceed as follows:

NOTE!

Insure the system has the correct connections and ground as shown in Figure 4-14.

- a. Turn the FUNCTION switch to OPR, turn the internal FUNCTION switch to CAL C, exercise the "C" decade switch by turning it twice through all positions, and set the readout to .0000000.
- b. Connect the voltage source to the red and the black BRIDGE POWER binding posts.
- c. Connect the null detector to the BRIDGE DETECTOR binding posts. The guard terminal of the null detector must be connected to the common terminal.

- d. Turn the B decade switch to the blank position and apply 10 volts from the voltage source.
- e. Adjust the BRIDGE BALANCE control to obtain a null indication ±10 microvolts.

NOTE!

If the null meter cannot be nulled using the Bridge Balance Control, perform the Bridge Calibration Procedure (paragraph 4-25).

- f. Locate the C-0 trimmer (R1130) on the circuit board and sweep it slowly from stop to stop while observing the null detector. If the indication does not change smoothly, sweep it from stop to stop several times.
- g. Set the null detector to the 30 microvolt range and adjust the C-0 trimmer to obtain an indication of 0 ± 10 microvolts.
- h. Observe the null detector and tap the trimmer; the indication should remain within 10 microvolts of zero.

- i. Use the following procedure to calibrate the "C" deck switch positions 1 through CAL:
 - 1. Turn the "C" deck switch clockwise to the next position to be calibrated.
 - 2. Observe the null detector and slowly sweep the trimmer corresponding to the switch position (C-1 through C CAL) from stop to stop. If the indication does not change smoothly, sweep the trimmer from stop to stop several times.
 - Observe the null detector and adjust the trimmer to obtain an indication of 0 ±10 microvolts.
 - 4. Observe the null detector and tap the trimmer; the indication should stay within 10 microvolts of the zero.
 - 5. Turn the "C" deck switch away from the position being calibrated, return it and observe the meter. The indication should be within 10 microvolts of zero

NOTE!

If the indication is not within 10 microvolts of zero, exercise the switch and repeat the procedure. If this fails, lubricate the switch as instructed in paragraph 4-12.

- 6. Proceed to the next position to be calibrated.
- i. Return the "C" deck switch to the 0 position.
- k. Turn the internal FUNCTION switch to the CAL S3 position.
- 1. Observe the null detector and slowly sweep the CAL S3 trimmer from stop to stop. If the indication does not change smoothly, sweep it from stop to stop several times.
- m. Adjust the CAL S3 trimmer to obtain an indication of 0 +10 microvolts.
- Observe the null detector and tap the trimmer.
 The indication should stay within 10 microvolts of zero.

- o. Turn the "C" decade switch away from the 0 positions and return it to zero. The null detector indication should be within 10 microvolts of zero.
- p. Return the internal FUNCTION switch to OPR; Calibration of the "C" decade and S3 shunt is complete.
- 4-24. To calibrate the "A" and "B" decades, perform the self-calibration procedure using the instructions given in paragraphs 2-24 and 2-25.

4-25. Bridge Calibration

NOTE!

The Bridge Calibration procedure is required only if a null could not be obtained during Divider Calibration with the BRIDGE BAL-ANCE Control.

4-26. 10-KILOHM BRIDGE STANDARD. This procedure is used to adjust the total resistance of the bridge arm used for calibration of the "A" and "B" decades (self-calibration of the instrument) so the bridge can be balanced to measure a nominal 10,000 ohms. If the bridge can be balanced near the center of travel for the BRIDGE BALANCE during self-cal at CAL A - Zero positions the procedure following does not need to be performed. However, if during self-cal in the CAL A - Zero position (See paragraph 2-24) the bridge cannot be balanced using the BRIDGE BALANCE Control, perform the procedure below:

NOTE!

Insure the system has the correct connections and ground as shown in Figure 4-14.

- a. Turn the FUNCTION switch to CAL A; turn the internal FUNCTION switch to OPR (Fig. 4-13) and set the readout to .0000000.
- b. Connect a 20 volt DC source to the red and the black BRIDGE POWER binding posts.
- c. Connect the null detector to the BRIDGE DETECTOR binding posts. The guard terminal of the null detector must be connected to the Common terminal.

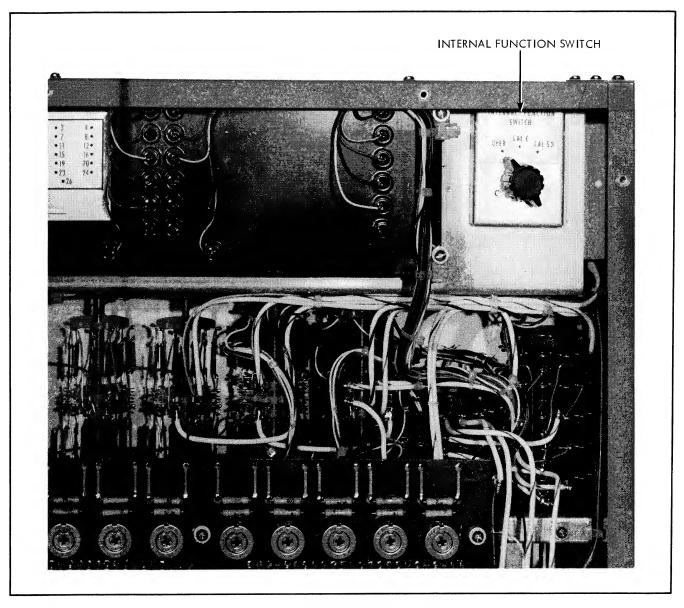


Figure 4-13. INTERNAL FUNCTION SWITCH

d. Adjust the Bridge Balance control to the center of its travel range.

NOTE!

BRIDGE BALANCE is a concentric control with both a Fine and Coarse range on the same control knob.

- e. Observe the null detector and sweep R203 on the bridge circuit board slowly from stop to stop. If the indication does not change smoothly, sweep R203 from stop to stop several times.
- f. Adjust R203 to obtain an indication of 0 ± 100

microvolts.

- g. Select the one millivolt range on the null detector. Vary the Bridge Balance control while observing the null detector. When the electrical center is obtained, leave the BRIDGE BALANCE control at that position.
- h. Re-adjust R203 to obtain an indication of 0 ± 100 microvolts
- i. Calibration of the 10-kilohm bridge standard is complete.

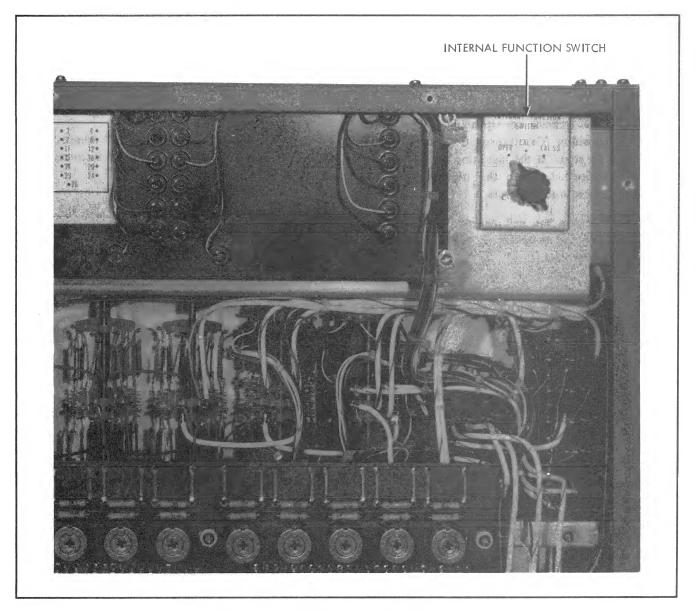


Figure 4-13. INTERNAL FUNCTION SWITCH

 Adjust the Bridge Balance control to the center of its travel range.

NOTE!

BRIDGE BALANCE is a concentric control with both a Fine and Coarse range on the same control knob.

- e. Observe the null detector and sweep R203 on the bridge circuit board slowly from stop to stop. If the indication does not change smoothly, sweep R203 from stop to stop several times.
- f. Adjust R203 to obtain an indication of $0.\pm100$

microvolts.

- g. Select the one millivolt range on the null detector. Vary the Bridge Balance control while observing the null detector. When the electrical center is obtained, leave the BRIDGE BALANCE control at that position.
- h. Re-adjust R203 to obtain an indication of 0 ± 100 microvolts
- i. Calibration of the 10-kilohm bridge standard is complete.

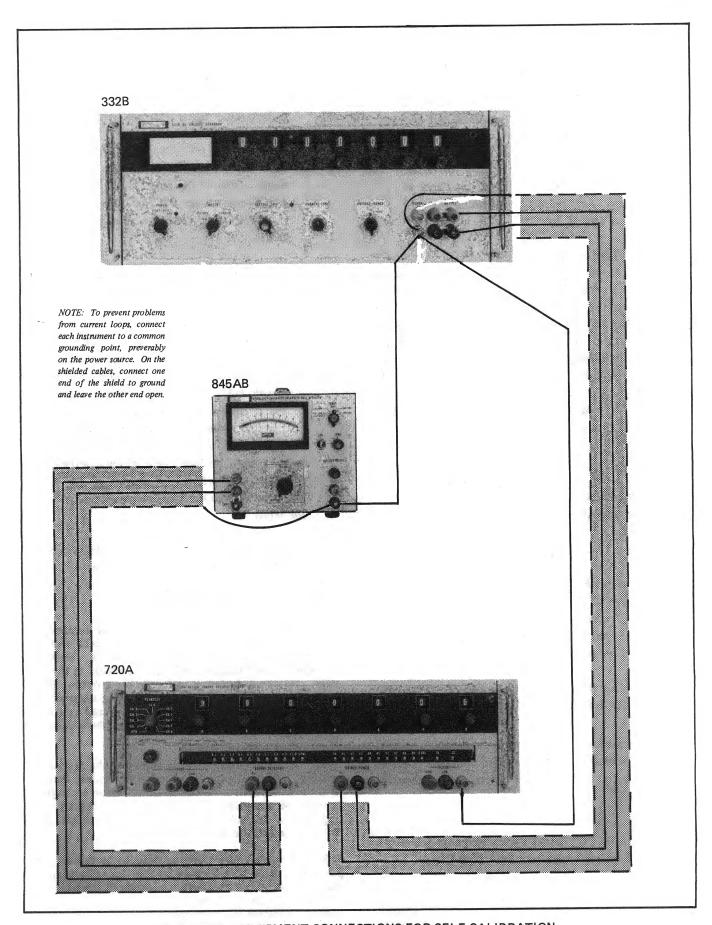


Figure 4-14. EQUIPMENT CONNECTIONS FOR SELF CALIBRATION.

NOTE!

The BRIDGE BALANCE control and R203 are now ready for the self-cal procedures for A and B decades in paragraph 2-24, assuming R312 and its associated trim resistors have not shifted excessively in value. If insufficient trim range remains at A.1, A.2, etc., the 720A should be returned to the factory for repair. Perform the C decade and S3 shunt check in paragraph 4-21 prior to performing the self-cal at A and B decades.

- 4-27. 4-KILOHM BRIDGE STANDARD. This procedure is used to adjust the total resistance of the bridge arm used for calibration of the third "C" decade so the bridge can be balanced to measure a nominal 4007.6 ohms. Calibration of the "C" decade consists of setting each step on the decade to a nominal 4007.6 ohms. If the bridge can be balanced with the BRIDGE BALANCE control on the front panel during self-cal in the CAL C-Zero position described in paragraph 4-21, this procedure does not need to be performed. To reset the range of the BRIDGE BALANCE, control for balance of the bridge, perform the following procedure:
- a. Turn the FUNCTION switch to OPR, and turn the internal FUNCTION switch to CAL C, and set the readout to .0000000.

NOTE!

The internal FUNCTION switch, which is shown in Figure 4-13, is used only for calibration of the "C" decade and the S-3 shunt. It should not be confused with the FUNCTION switch located on the front panel.

- b. Connect the voltage source to the red and the black BRIDGE POWER binding posts.
- c. Connect the null detector to the BRIDGE DETEC-TOR binding posts. The guard terminal of the null detector must be connected to the common terminal.
- d. Turn the "C" decade switch to the blank position and apply 10 volts from the voltage source.
- e. Adjust BRIDGE BALANCE to the mid-position and adjust R1130 (Decade C-9) to mid position

- f. Observing the Null Detector sweep R205 (Bridge Circuit Board) thru its range. If the null detector does not show a smooth change, sweep R205 through its range several times.
- g. Adjust R205 for 0 ± 50 microvolts on the Null Detector.
- h. Place the Null Detector on the 300 microvolt range. Observe the range of the BRIDGE BAL-ANCE control on the Null Detector and place the BRIDGE BALANCE control at the electrical center.
- i. Adjust R1130 (Decade C-0) for 0 ± 10 microvolts.

NOTE!

The BRIDGE BALANCE control, R205 and R1130 are now set to give a nominal 4007.6 ohm reference and the self-cal procedure in paragraph 4-21 will make the other positions of the C Decade the same value. If there is not enough range to trim the remaining positions of the C Decade to this nominal value repeat steps a through i with different settings for R205 and R1130. If calibration still is not possible, return the 720A to the factory for repair.

j. Disconnect the test equipment; calibration of the 4-kilohm bridge standard is complete.

4-28. TROUBLESHOOTING

- 4-29. Troubles in the Model 720A may be located most easily by performing the decade linearity test described in paragraph 4-15 and analyzing the results. Reference to the schematic diagram will greatly assist in the analysis. Before attempting to locate the trouble, the instrument should first be cleaned following the procedure described in paragraph 4-10 and the leakage resistance should be measured following the procedure described in paragraph 4-8.
- 4-30. Because of the passive nature of the instrument, troubles will be limited to defective resistors, defective switches, defective wiring, and excessive leakage will usually be corrected by cleaning. If repeated cleaning fails to correct the condition, the instrument should be returned to the factory for repair.
- 4-31. Not only may resistor defects be isolated to a particular step of a decade by the linearity test, but also the nature of the defect may be determined. A resistor may be shorted, open, over value, or under value. Because the switch contacts span two steps of resistance in all decades except the seventh ("G"), the

effect caused directly by a defective resistor will be seen at two adjacent switch positions. In the "D" through "G" decades the linearity test will isolate the defect to a particular resistor. In the "A", "B", and "C", decades each step is made up of several resistors and each resistor in the step will have to be measured to find the defect. In these decades, the variable trimmer resistor in the defective step should be checked by monitoring it and sweeping it from stop to stop several times. If the variation is not smooth, it should be replaced. If one of the resistors in the oil tank or one of the factory selected fixed resistors is found to be defective, the instrument should be returned to the factory for repair.

- 4-32. A shorted resistor will decrease the overall resistance of the decade thereby increasing the proportional value of all steps except the one containing the shorted resistor. The proportional value of this step will be very low.
- 4-33. An open resistor in any decade will prevent any output until the switch is advanced so the contacts span the open resistor. At this point the ratio will be high. As the switch is advanced so the contacts no longer span the open resistor, the measured output will be the source voltage. If a decade shunt is open all steps of the decade will be equal but resistance of the decade will be high. This will cause nonlinearity in the preceding decade which may be observed by dialing it upward from zero. Below the midpoint, the output will be high; above the midpoint, the output will be low.
- 4-34. An over value resistor in any decade will reduce the proportion of all other steps and increase the proportion of the step containing the over value resistor. In all decades except the seventh, this increase will be seen at two adjacent switch positions because the switch contacts span two resistance steps. In the seventh decade, there will be only one over value step. If a decade shunt is over value, all steps of the decade will be equal but the resistance of the decade will be high. This will cause nonlinearity in the preceding decade which may be observed by dialing it upward from zero. Below the midpoint, the output will be high; above the midpoint, the output will be low.
- 4-35. An under value resistor in any decade will increase the proportion of all other steps and decrease the proportion of the step containing the under value resistor. In all decades except the seventh, this decrease will be seen at two adjacent switch positions. In the seventh decade there will be only one under value step. If a decade shunt is under value, all steps of the decade will be equal but the resistance of the decade will be low. This will cause nonlinearity in the preceding decade which may be observed by dialing it upward from zero. Below the midpoint, the output will be low; above the midpoint, the output will be high.
- 4-36. A defective switch usually will cause erratic or irregular operation of the decade. A broken contact may cause one step to be missing although all others are of the correct value or it may completely open the divider circuit. When a switch defect is suspected, the switch should be checked for continuity at each position.

4-37. Defective wiring usually will cause one step of a decade to be missing or will completely open the divider circuit. Wiring continuity should be checked to isolate the fault.

4-38. REPAIR

- 4-39. Any parts of the Model 720A except factory selected resistors and resistors housed in the oil tank may be replaced without difficulty by an experienced electronic maintenance technician. When a switch is replaced all leads should be tagged as they are disconnected to assure that they are correctly connected to the new switch. Care should be exercised in any soldering operation to assure that good electrical contact is made. All parts except precision wirewound resistors may be ordered from the factory by giving only the information specified in paragraph 5-4.
- 4-40. The precision wirewound resistors used in the Model 720A are selected and matched during manufacture to form a completely matched set. Sufficient information is marked on each of these resistors to permit replacement with a resistor which will match the others in the set. The following information should be given when one of these resistors is ordered from the factory:
- a. Serial number of the instrument.
- b. Reference designation of the resistor.
- c. All markings on the resistor.

If all markings on the defective resistor can not be read, give the following information:

- a. Serial number of the instrument.
- b. Reference designation of the defective resistor.
- c. Reference designation and all part markings of the adjacent resistor on one side.
- d. Reference designation and all part markings of the adjacent resistor on the other side.

4-41. SERVICE INFORMATION

- 4-42. The John Fluke Manufacturing Co., Inc. warrants each instrument manufactured by them for the period of one year upon making delivery of the instrument to you, the original purchaser. Complete warranty page located at the rear of this manual.
- 4-43. If you should encounter any problem in the operation of your instrument, please feel free to contact your nearest John Fluke Sales Representative or write directly to the John Fluke Manufacturing Co., Inc. with a statement of your problem.

Section 5

List of Replaceable Parts

5-1. INTRODUCTION

This section contains complete descriptions of those parts one might normally expect to replace during the life of the instrument. The first listing is a breakdown of all of the major assemblies in the instrument. Subsequent listings itemize the components in each assembly. Every listing is accompanied by an illustration identifying each component in the listing. Assemblies and subassemblies are identified by name in the parts list and by a ten digit stock number in the illustrations. Components are identified by the schematic diagram reference designation (e.g. R1, C107 DS1). Parts not appearing on the schematic diagram are numbered consecutively throughout the parts list with a whole number. Flagnotes are used throughout the parts list and refer to ordering explanations. The flagnote explanations appear at the end of the parts list in which they are listed.

5-3. COLUMNAR INFORMATION

- a. The REF DESIG column indexes the item description to the associated illustration. In general the reference designations are listed under each assembly in alpha-numeric order. Subassemblies of minor proportions are sometimes listed with the assembly of which they are a part. In this case, the reference designations for the components of the subassembly may appear out of order.
- b. The DESCRIPTION column describes the salient characteristics of the component. Indention of the description indicates the relationship to other assemblies, components, etc. In many cases it is necessary to abbreviate in this column. For abbreviations and symbols used, see the following page.
- c. The ten-digit part number by which the item is identified at the John Fluke Mfg. Co. is listed in the STOCK NO. column. Use this number when ordering parts from the factory or authorized representatives.

- d. The Federal Supply Code for the item manufacturer is listed in the MFR column. An abbreviated list of Federal Supply Codes is included in the Appendix.
- e. The part number which uniquely identifies the item to the original manufacturer is listed in the MFR PART NO column. If a component must be ordered by description, the type number is listed.
- f. The TOT QTY column lists the total quantity of the item used in the instrument. Second and subsequent listing of the same item are referenced to the first listing with the abbreviation REF. In the case of optional subassemblies, plug ins, etc. that are not always pare of the instrument, the TOT QTY column lists the total quantity of the item in that particular assembly.
- g. Entries in the REC QTY column indicate the recommended number of spare parts necessary to support one to five instruments for a period of two years. This list presumes an availability of common electronic parts at the maintenance site. For maintenance for one year or more at an isolated site, it is recommended that at least one of every part in the instrument be stocked.
- which have been added, deleted or modified during the production of the instrument. Each part for which a Use Code has been assigned may be identified with a particular instrument serial number by consulting the Serial Number Effectivity List. As Use Codes are added to the list, the TOT QTY column listings are changed to reflect the most current information. Sometimes when a part is changed, the new part can and should be used as a replacement for the original part. In this event a parenthetical note is added in the DESCRIPTION column.

5-4. HOW TO OBTAIN PARTS

- 5-5. Standard components have been used wherever possible. Standard components may be ordered directly from the manufacturer by using the manufacturer's part number, or parts may be ordered from the John Fluke Mfg. Co. factory or authorized representative by using the Fluke part number. In the event the part you order has been replaced by a new or improved part, the replacement will be accompanied by an explanatory note and installation instructions, if necessary.
- 5-6. You can insure prompt and efficient handling of your order to the John Fluke Mfg. Co. if you include the following information:
- a. Quantity.
- b. FLUKE Stock Number.
- c. Description.
- d. Reference Designation.
- e. Instrument model and serial number.

Example; 2 each, 4805-177105, Transistors, 2N3565, Q107-108 for 845AR, s/n 168.

If you must order structural parts not listed in the parts list, describe the part as completely as possible. A sketch of the part showing its location to other parts of the instrument is usually most helpful.

5-8. SERIAL NUMBER EFFECTIVITY

5-9. A Use Code column is provided to identify certain parts that have been added, deleted, or modified during production of the Model 720A. Each part for which a use code has been assigned may be identified with a particular instrument serial number by consulting the Use Code Effectivity List below. All parts with no code are used on all instruments with serial numbers above 123. New codes will be added as required by instrument changes.

USE

CODE EFFECTIVITY

No

Code Model 720A, serial number 123 and on.

A Model 720A, serial number 536 and on.

REF DESIG	DESCRIPTION	STOCK NO	MFR	MFR PART NO	TOT QTY	REC QTY	USE CODE
	KELVIN-VARLEY VOLTAGE DIVIDER Figure 5-1	720A					
	Front Panel Assembly (See Figure 5-2)						
	Trimmer P/C Assembly (See Figure 5-3)	1702-210716 (720A-4001)	89536	1702-210716	1		
	Bridge P/C Assembly (See Figure 5-4)	1702-200295 (720A-4002)	89536	1702-200295	1		
	Resistor Can Assembly If a resistor in this assembly requires replacement, the entire instrument must be returned to the factory for repair and recalibration.	3158-217612 (720A-4018)	89536	3158-217612	1		
S1	Switch, "A" DECADE, rotary, 3p, 12 pos, 3 sect	5105-220012	89536	5105-220012	1		
	"B" Decade Switch Assembly (See Figure 5-5)	5110-217307 (720A-4004)	89536	5110-217307	1		
	"C" Decade Switch Assembly (See Figure 5-6)	5110-217315 (720A-4005)	89536	5110-217315	1		
	"D", "E", "F" and "G" Decades Switch Assy. (See Figure 5-7)	5110-217323 (720A-4006)	89536	5110-217323	1		
S 8	Switch, FUNCTION, 5p, 11 pos, 5 sect	5105-220020	89536	5105-220020	1		
S9	Switch, INTERNAL FUNCTION, 4p, 3 pos, 2 sect	5107-218560	89536	5107-218560	1		
1	Bushing, dial	2502-130435	89536	2502-130435	7		
1	Bushing, dial	3153-130252	89536	3153-130252	7		A
2	Coupler, switch (not illustrated)	2402-200592	89536	2402-200592	7		
3	Cover, bottom (not illustrated)	3156-217117	89536	3156-217117	1		
4	Cover, internal function switch	3156-217521	89536	3156-217521	1		
5	Cover, top (not illustrated)	3156-217125	89536	3156-217125	1		
6	Detent, switch	5108-218578	89536	5108-218578	6	į	
7	Detent, internal function switch (not illustrated)	5108-218552	89536	5108-218552	1		
8	Dial, 0.0 - 1.0 Cal	2403-208611	89536	2403-208611	1		
9	Dial, 0 - Cal	2403-208595	89536	2403-208595	2		
10	Dial, 0 - X	2403-208603	89536	2403-208603	1		
11	Dial, 0 - 9	2403-208587	89536	2403-208587	3		
12	Foot, rubber (not illustrated)	2819-103309	77969	9102-W	4		
13	Heat sink, resistor	3156-217463	89536	3156-217463	1		
14	Knob, INTERNAL FUNCTION	2405-170050	89536	2405-170050	1		
15	Panel, rear	3156-217075	89536	3156-217075	1		

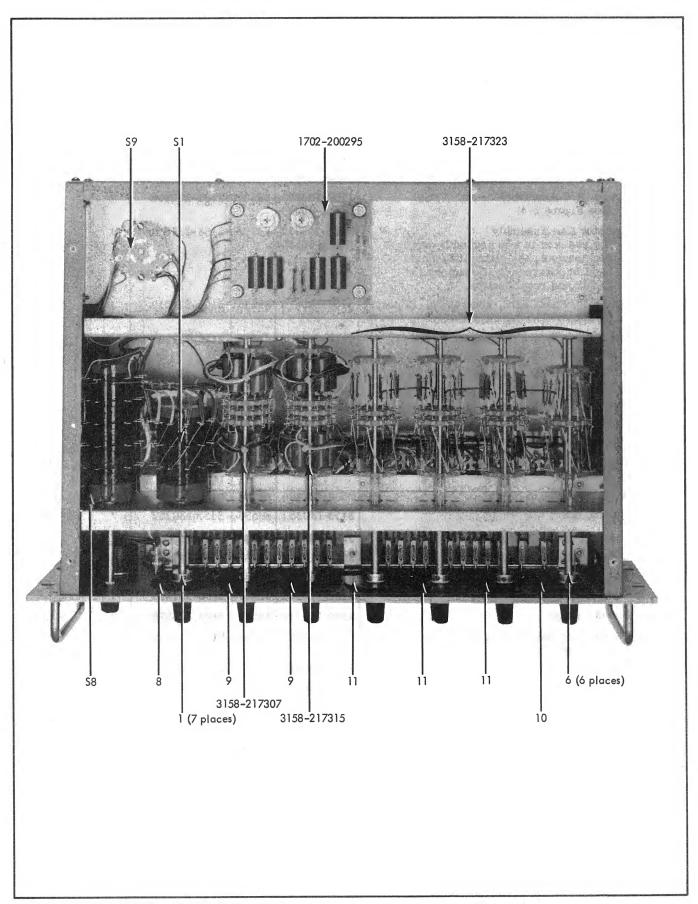


Figure 5-1. 720A KELVIN-VARLEY VOLTAGE DIVIDER (Sheet 1 of 2)

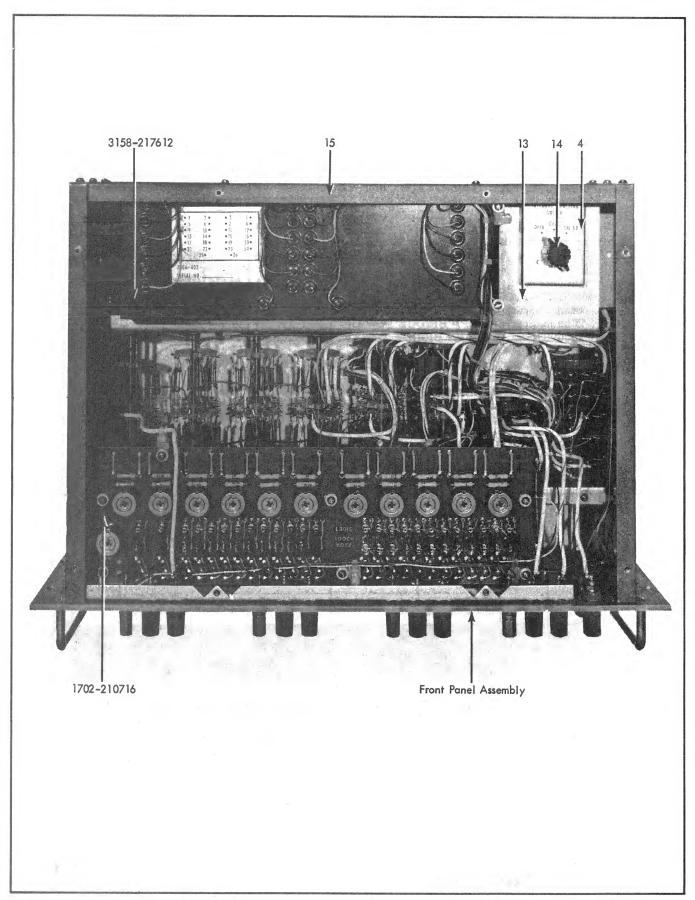


Figure 5-1. 720A KELVIN-VARLEY VOLTAGE DIVIDER (Sheet 2 of 2)

REF DESIG	DESCRIPTION	STOCK NO	MFR	MFR PART NO	TOT QTY	REC QTY	USE CODE
	FRONT PANEL ASSEMBLY - Figure 5-2						
J1	Binding post, red, 1.1 INPUT	2811-149856	58474	BHB-10208-G22	5		
J2	Binding post, red, 1.0 INPUT	2811-149856		BHB-10208-G22			
J3	Binding post, black, LOW INPUT	2811-149864		BHB-10208-G21			
J4	Binding post, GROUND INPUT	2811-155911			4		
J5	Binding post, red, HIGH OUTPUT	2811-149856		BHB-10208-G22	-		
J6	Binding post, black, LOW OUTPUT	2811-149864	58474	BHB-10208-G21	REF		
J7	Binding post, GROUND OUTPUT	2811-155911			REF		
J8	Binding post, black, - BRIDGE DETECTOR	2811-149864	1	BHB-10208-G21			
J9	Binding post, red, + BRIDGE DETECTOR	2811-149856	58474	BHB-10208-G22	REF		
J10	Binding post, GROUND BRIDGE DETECTOR	2811-155911	58474	GP30NC	REF		
J11	Binding post, red, + BRIDGE POWER	2811-149856	58474	BHB-10208-G22	REF		
J12	Binding post, black, - BRIDGE POWER	2811-149864		BHB-10208-G21			
J13	Binding post, GROUND BRIDGE POWER	2811-155911		GP30NC	REF		
R1	Res, var, ww, 5k ±3%, 3w, BRIDGE BALANCE (not illustrated)	4702-215319	89536	4702-215319	1		
16	Cover, calibration access	3156-217083	89536	3156-217083	1		
17	Handle, chrome-plated brass			1010-13	2		
18	Knob, A through G	2405-158949		2405-158949	7		
19	Knob, BRIDGE BALANCE	2405-158956	89536	2405-158956	1		
20	Knob, FUNCTION	2405-190249			1		
21	Panel, front	1406-217042		1406-217042	ī		

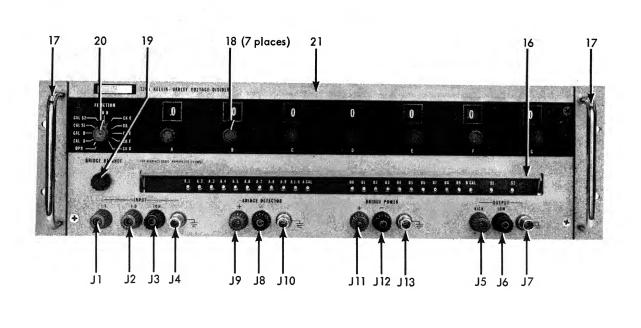


Figure 5-2. FRONT PANEL ASSEMBLY

REF	25525555	STOCK		MFR	тот	REC	USE
DESIG	DESCRIPTION	NO	MFR	PART NO	QTY	QTY	CODE
	TRIMMER P/C ASSEMBLY -Figure 5-3	1702-210716 (720A-4001)	89536	1702-210716	REF		
R1001	Res, var, ww, $5k \pm 10\%$, 1w	4702-215269	02660	3800P-502	24		
R1002	Res, met flm, $8.45k \pm 1\%$, $1/2w$	4705-159475	12400	Type CEC-TO	12		
R1003 R1004	Res, ww, $100\Omega \pm 0.5\%$, $1/2$ w Res, ww, factory selected	4707-155846	89536	4707-155846	23	1	
R1004	Res, var, ww, 5k ±10%, 1w	4702-215269	02660	3800P-502	REF		
R1006	Res, met flm, $8.45k \pm 1\%$, $1/2w$	4705-159475	12400	Type CEC-TO	REF		
R1007	Res, ww, $100\Omega \pm 0.5\%$, $1/2w$	4707-155846	89536	4707-155846	REF		
R1008	Res, ww, factory selected	1					
R1009 R1010	Res, var, ww, $5k \pm 10\%$, $1w$ Res, met flm, $8.45k \pm 1\%$, $1/2w$	4702-215269 4702-159475	02660 12400	3800P-502	REF		
				Type CEC-TO	REF		
R1011 R1012	Res, ww, $100\Omega \pm 0.5\%$, $1/2w$ Res, ww, factory selected	4707-155846	89536	4707-155846	REF		
R1013	Res, var, ww, 5k ±10%, 1w	4702-215269	02660	3800P-502	REF		
R1014	Res, met flm, $8.45k \pm 1\%$, $1/2w$	4705-159475	12400	Type CEC-TO	REF		
R1015	Res, ww, $100\Omega \pm 0.5\%$, $1/2w$	4707-155846	89536	4707-155846	REF		
R1016	Res, ww, factory selected	1>					
R1017	Res, var, ww, 5k ±10%, 1w	4702-215269	02660	3800P-502	REF		
R1018	Res, met flm, $8.45k \pm 1\%$, $1/2w$	4705-159475	12400	Type CEC-TO	REF		
R1019 R1020	Res, ww, $100\Omega \pm 0.5\%$, $1/2w$ Res, ww, factory selected	4707-155846	89536	4707-155846	REF		
	nes, ww, factory selected	1					
R1021	Res, var, ww, $5k \pm 10\%$, $1w$	4702-215269	02660	3800P-502	REF		
R1022	Res, met flm, $8.45k \pm 1\%$, $1/2w$	4705-159475	12400	Type CEC-TO	REF		
R1023 R1024	Res, ww, $100\Omega \pm 0.5\%$, $1/2w$ Res, ww, factory selected	4707-155846	89536	4707-155846	REF		
R1025	Res, var, ww, 5k ±10%, 1w	4702-215269	02660	3800P-502	REF		
R1026	Res, met flm, $8.45k \pm 1\%$, $1/2w$	4705-159475	12400	Type CEC-TO	REF		
R1027	Res, ww, $100\Omega \pm 0.5\%$, $1/2w$	4707-155846	89536	4707-155846	REF		
R1028	Res, ww, factory selected	1					
R1029 R1030	Res, var, ww, $5k \pm 10\%$, $1w$ Res, met flm, $8.45k \pm 1\%$, $1/2w$	4702-215269	02660	3800P-502	REF		
		4705-159475	12400	Type CEC-TO	REF		
R1031 R1032	Res, ww, $100\Omega \pm 0.5\%$, $1/2w$ Res, ww, factory selected	4707-155846	89536	4707-155846	REF		
R1033	Res, var, ww, 5k ±10%, 1w	4702-215269	02660	3800P-502	REF		
R1034	Res, met flm, $8.45k \pm 1\%$, $1/2w$	4705-159475	12400	Type CEC-TO	REF		
R1035	Res, ww, $100\Omega \pm 0.5\%$, $1/2w$	4707-155846	89536	4707-155846	REF		
R1036	Res, ww, factory selected						
R1037	Res, var, ww, $5k \pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		
R1038	Res, met flm, $8.45k \pm 1\%$, $1/2w$	4705-159475	12400	Type CEC-TO	REF		
R1039	Res, ww, $100\Omega \pm 0.5\%$, $1/2w$	4707-155846	89536	4707-155846	REF		
R1040	Res, ww, factory selected	1>					
R1041	Res, var, ww, 5k ±10%, 1w	4702-215269	02660	3800P-502	REF		
R1042	Res, met flm, $8.45k \pm 1\%$, $1/2w$	4705-159475	12400	Type CEC-TO	REF		
R1043 R1044	Res. www. footony.colorted	4707-155846	89536	4707-155846	REF		
R1044	Res, ww, factory selected Res, ww, $1000 \pm 0.5\%$, $1/2$ w	1 4707-155846	89536	4707-155846	REF		
		1					
R1046 R1047	Res, www, factory selected						
R1047	Res, ww, factory selected Res, var, ww, 5k ±10%, 1w	4702-215269	02660	3800P-502	REF		
		1.02 210200	02000	55551 552	1,111		4
					*		

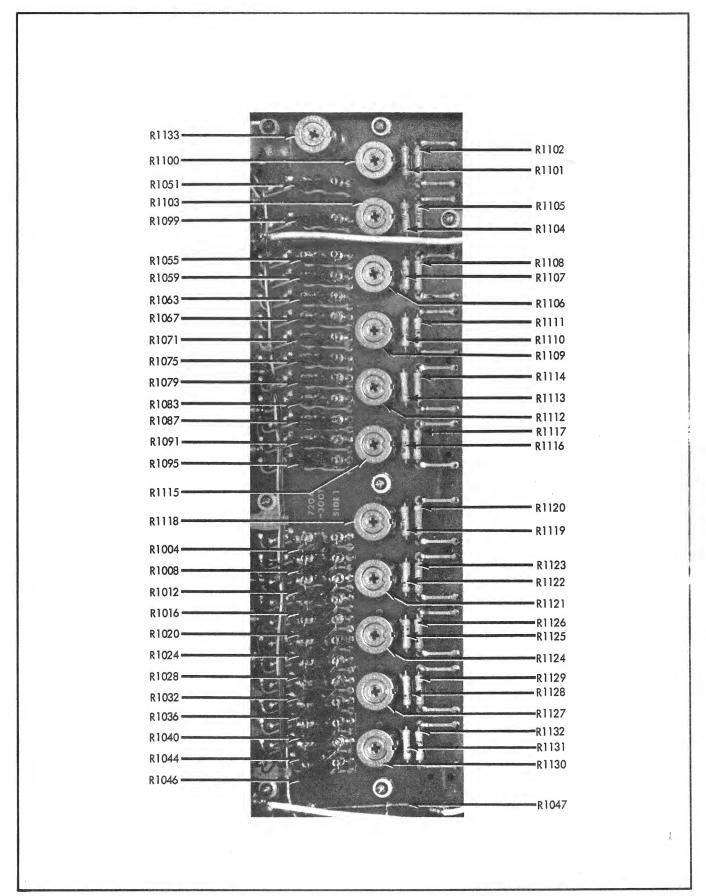


Figure 5-3. TRIMMER P/C ASSEMBLY (Sheet 1 of 2)

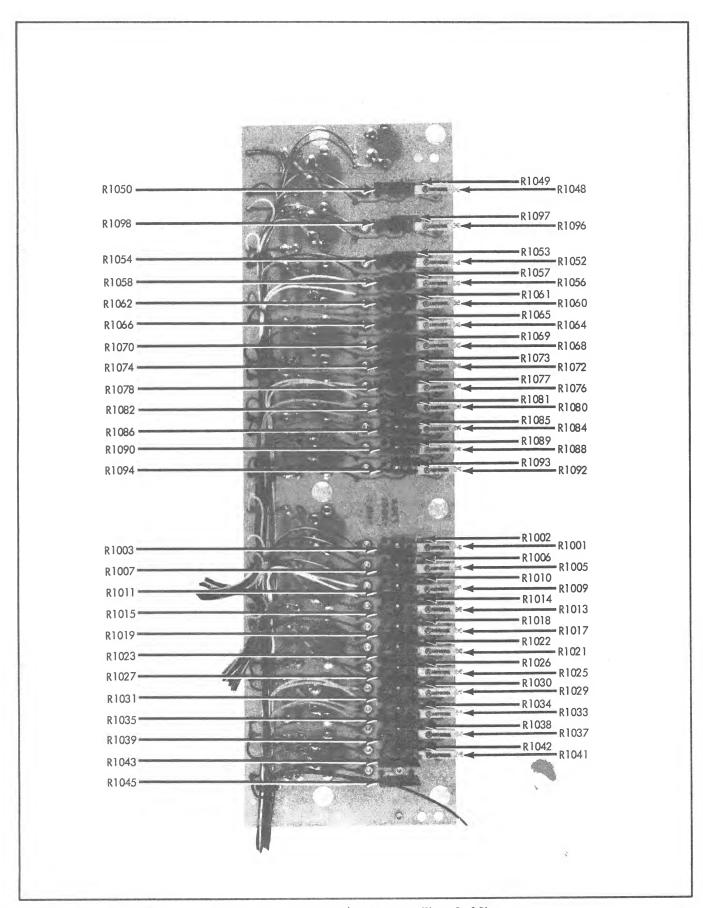


Figure 5-3. TRIMMER P/C ASSEMBLY (Sheet 2 of 2)

REF DESIG	DESCRIPTION	STOCK NO	MFR	MFR PART NO	TOT QTY	REC QTY	USE CODE
D1040	Dog mot flow 9 451; 10/ 1/9;;	4705-159475	12400	Type CEC-TO	REF		
R1049 R1050	Res, met flm, 8.45k $\pm 1\%$, 1/2w Res, ww, 250 Ω $\pm 0.5\%$, 1/2w	4707-199893	89536	4707-199893	REF 1	1	
R1050	Res, ww, factory selected	101-199093	09000	4101-199099	*	1	
R1051	Res, var, ww, 5k ±10%, 1w	4702-215269	02660	3800P-502	REF	1	
R1053	Res, met flm, $4.75k \pm 1\%$, $1/2w$	4705-192500	12400	Type CEC-TO	12		
111000	1000, 11100 12111, 11 1011 1270, 27 211	1.00					
R1054	Res, ww, $100\Omega \pm 0.5\%$, $1/2w$	4707-155846	89536	4707-155846	REF		
R1055	Res, ww, factory selected					ĺ	
R1056	Res, var, ww, $5k \pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		
R1057	Res, met flm, $4.75k \pm 1\%$, $1/2w$	4705-192500	12400	Type CEC-TO	REF		
R1058	Res, ww, $100\Omega \pm 0.5\%$, $1/2w$	4707-155846	89536	4707-155846	REF		
71050	December 6-states and set of	F					
R1059	Res, ww, factory selected	4702-215269	02660	3800P-502	DEE		
R1060 R1061	Res, var, ww, $5k \pm 10\%$, $1w$ Res, met flm, $4.75k \pm 1\%$, $1/2w$	4705-192500	12400	Type CEC-TO	REF REF		
R1062	Res, ww, $100\Omega \pm 0.5\%$, $1/2$ w	4707-155846	89536	4707-155846	REF		
R1063	Res, ww, factory selected	1	00000	1101-100010	T T T		
R1064	Res, var, ww, $5k \pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		
R1065	Res, met flm, 4.75k $\pm 1\%$, 1/2w	4705-192500	12400	Type CEC-TO	REF		
R1066	Res, ww, $100\Omega \pm 0.5\%$, $1/2w$	4707-155846	89536	4707-155846	REF		
R1067	Res, ww, factory selected						
R1068	Res, var, ww, $5k \pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		
D1060	Dog of floor 4 75h +10/ 1/200	4705-192500	12400	Trme CEC TO	REF		
R1069 R1070	Res, met flm, $4.75k \pm 1\%$, $1/2w$ Res, ww, $1000 \pm 0.5\%$, $1/2w$	4707-155846	89536	Type CEC-TO 4707-155846	REF		
R1070	Res, ww, factory selected	1	09000	4101-133040	ILEI		
R1072	Res, var, ww, 5k ±10%, 1w	4702-215269	02660	3800P-502	REF		
R1073	Res, met flm, 4.75k $\pm 1\%$, 1/2w	4705-192500	12400	Type CEC-TO	REF		
D1074	Pos 1000 -0 50 1/2	4707-155846	89536	4707-15584f	REF		
R1074 R1075	Res, ww, $100\Omega \pm 0.5\%$, $1/2$ w Res, ww, factory selected	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	09000	4101-19994(REF		
R1076	Res, var, ww, 5k ±10%, 1w	4702-215269	02660	3800P-502	REF		
R1077	Res, met flm, $4.75k \pm 1\%$, $1/2w$	4705-192500	12400	Type CEC-TO	REF		
R1078	Res, ww, $100\Omega \pm 0.5\%$, $1/2w$	4707-155846	89536	4707-155846	REF		
		<i>L</i> -					
R1079	Res, ww, factory selected	4702-215269	00000	3800P-502	REF		
R1080 R1081	Res, var, ww, $5k \pm 10\%$, $1w$ Res, met flm, $4.75k \pm 1\%$, $1/2w$	4705-192500	02660		REF		
R1081	Res, ww, $100\Omega \pm 0.5\%$, $1/2$ w	4707-155846	89536	4707-155846	REF		
R1083	Res, ww, factory selected		00000	1.0. 200010	1022		
		4	00000	0000 500			
R1084	Res, var, ww, $5k \pm 10\%$, 1w	4702-215269	02660	3800P-502	REF	А	
R1085	Res, met flm, 4.75k $\pm 1\%$, $1/2$ w	4705-192500	12400	Type CEC-TO	REF		
R1086	Res, ww, $1000 \pm 0.5\%$, $1/2$ w	4707-155846	89536	4707-155846	REF	A 1	a n
R1087 R1088	Res, ww, factory selected Res, var, ww, $5k \pm 10\%$, $1w$	4702-215269	02660	3800P-502	REF		
10000	ICS, VAI, WW, DA TIU/0, IW	7.02-210209	02000	30001 -002	1,111		
R1089	Res, met flm, $4.75k \pm 1\%$, $1/2w$	4705-192500	12400	Type CEC-TO	REF		
R1090	Res, ww, $100\Omega \pm 0.5\%$, $1/2w$	4707-155846	89536	4707-155846	REF		
R1091	Res, ww, factory selected						
R1092	Res, var, ww, $5k \pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		17
R1093	Res, met flm, $4.75k \pm 1\%$, $1/2w$	4705-192500	12400	Type CEC-TO	REF		
R1094	Res, ww, $100\Omega \pm 0.5\%$, $1/2w$	4707-155846	89536	4707-155846	REF		
R1095	Res, ww, factory selected		Y 11				
R1096	Res, var, ww, $5k \pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		
R1097	Res, met flm, $4.75k \pm 1\%$, $1/2w$	4705-192500	12400	Type CEC-TO	REF		
R1098	Res, ww, $400\Omega \pm 0.25\%$, $1/2w$	4707-131698	89536	4707-131698	1		
	4						

REF		STOCK		MFR	тот	REC	USE
DESIG	DESCRIPTION	NO	MFR	PART NO	QTY	QTY	CODE
R1099	Res, ww, factory selected					ľ	
R1100	Res, var, ww, $25\Omega \pm 10\%$, $1 \frac{1}{4}$ w	4702-161703	71450	Type 110	11		
R1101	Res, met flm, 23. $2\Omega \pm 1\%$, $1/2$ w	4705-200790	12400	Type CEC-TO	11		
R1102	Res, met flm, $100 \pm 1\%$, $1/2$ w	4705-151043	12400	Type CEC-TO	11		
R1103	Res, var, ww, $25\Omega \pm 10\%$, $1 1/4\text{w}$	4702-161703	71450	Type 110	REF		
R1104	Res, met flm, 23. $2\Omega \pm 1\%$, $1/2$ w	4705-200790	12400	Type CEC-TO	REF		
R1105	Res, met flm, $10\Omega \pm 1\%$, $1/2$ w	4705-151043	12400	Type CEC-TO	REF		
R1106	Res., var, ww, $25\Omega \pm 10\%$, $1 \frac{1}{4}$ w	4702-161703	71450	Type 110	REF		
R1107	Res, met flm, 23. $2\Omega \pm 1\%$, $1/2$ w	4705-200790	12400	Type CEC-TO	REF	j	
R1108	Res, met flm, $10\Omega \pm 1\%$, $1/2$ w	4705-151043	12400	Type CEC-TO	REF		
R1109	Res, var, ww, $25\Omega \pm 10\%$, $1 \frac{1}{4}$ w	4702-161703	71450	Type 110	REF		
R1110	Res, met flm, 23. $2\Omega \pm 1\%$, $1/2$ w	4705-200790	12400	Type CEC-TO	REF		
R1111	Res, met flm, $10\Omega \pm 1\%$, $1/2$ w	4705-151043	12400	Type CEC-TO	REF		
R1112	Res, var, ww, $25\Omega \pm 10\%$, $1 \frac{1}{4}$ w	4702-161703	71450	Type 110	REF		
R1113	Res, met flm, 23. $2\Omega \pm 1\%$, $1/2w$	4705-200790	12400	Type CEC-TO	REF		
R1114	Res, met flm, $10\Omega \pm 1\%$, $1/2$ w	4705-151043	12400	Type CEC-TO	REF		
R1115	Res, var, ww, $25\Omega \pm 10\%$, $1 \frac{1}{4}$ w	4702-161703	71450	Type 110	REF		
R1116	Res, met flm, 23. $2\Omega \pm 1\%$, $1/2$ w	4705-200790	12400	Type CEC-TO	REF		
R1117	Res, met flm, $10\Omega \pm 1\%$, $1/2$ w	4705-151043	12400	Type CEC-TO	REF		
R1118	Res, var, ww, $25\Omega \pm 10\%$, $1 \frac{1}{4}$ w	4702-161703	71450	Type 110	REF		
R1119	Res, met flm, 23. $2\Omega \pm 1\%$, $1/2$ w	4705-200790	12400	Type CEC-TO	REF		
R1120	Res, met flm, $10\Omega \pm 1\%$, $1/2$ w	4705-151043	12400	Type CEC-TO	REF		
R1121	Res, var, ww, $25\Omega \pm 10\%$, $1 \frac{1}{4}$ w	4702-161703	71450	Type 110	REF		
R1122	Res, met flm, 23. $2\Omega \pm 1\%$, $1/2$ w	4705-200790	12400	Type CEC-TO	REF		
R1123	Res, met flm, $10\Omega \pm 1\%$, $1/2$ w	4705-151043	12400	Type CEC-TO	REF		
R1124	Res, var, ww, $25\Omega \pm 10\%$, $1 \frac{1}{4}$ w	4702-161703	71450	Туре 110	REF		
R1125	Res, met flm, 23. $2\Omega \pm 1\%$, $1/2$ w	4705-200790	12400	Type CEC-TO	REF		
R1126	Res, met flm, $10\Omega \pm 1\%$, $1/2w$	4705-151043	12400	Type CEC-TO	REF		
R1127	Res, var, ww, $25\Omega \pm 10\%$, $1 \frac{1}{4}$ w	4702-161703	71450	Type 110	REF		
R1128	Res, met flm, 23. $2\Omega \pm 1\%$, $1/2$ w	4705-200790	12400	Type CEC-TO	REF		
R1129	Res, met flm, $10\Omega \pm 1\%$, $1/2$ w	4705-151043	12400	Type CEC-TO	REF		
R1130	Res, var, ww, $25\Omega \pm 10\%$, $1 \frac{1}{4}$ w	4702-161703	71450	Type 110	REF		
R1131	Res, met flm, 23. $2\Omega \pm 1\%$, $1/2$ w		12400	7 X	REF		
R1132	Res, met flm, $10\Omega \pm 1\%$, $1/2$ w	4705-151043	12400	Type CEC-TO	REF		
R1133	Res, var, ww, $150\Omega \pm 20\%$, $1 \frac{1}{4}$ w	4702-163642	71450	Type 110	1		
			L	<u> </u>	L		

These resistors are factory selected. Replace with exact value. When ordering, include model, serial number, reference designation and all information stamped on the resistor.

REF DESIG	DESCRIPTION	STOCK NO	MFR	MFR PART NO	TOT	REC QTY	USE CODE
	BRIDGE P/C ASSEMBLY - Figure 5-4	1702-200295 (720A-4002)	89536	1702-200295	REF		
R201 R202 R203 R204 R205	Res, ww, 39.536k, matched set Res, ww, 39.536k, matched set Res, var, ww, $100\Omega \pm 20\%$, $1 \frac{1}{4}$ w Res, ww, $15.814k \pm 0.02\%$, 1 w Res, var, ww, $100\Omega \pm 20\%$, $1 \frac{1}{4}$ w	2 2 4702-112797 4707-200550 4702-112797	71450 89536 71450	4707-200550	2 1 REF	1	
R206 R207 R208 R209	Res, ww, 4.873k, matched set Res, ww, 4.873k, matched set Res, met flm, 15k $\pm 1\%$, 1/2w Res, ww, 250 Ω $\pm 0.5\%$, 1/2w	3 3 4705-151498 4707-199893	12400 89536		1	1	
						1	

These resistors are factory matched. If replacement is required, an entire set, part number 4710-217679, must be ordered.

These resistors are factory matched. If replacement is required, an entire set, part number 4710-217687, must be ordered.

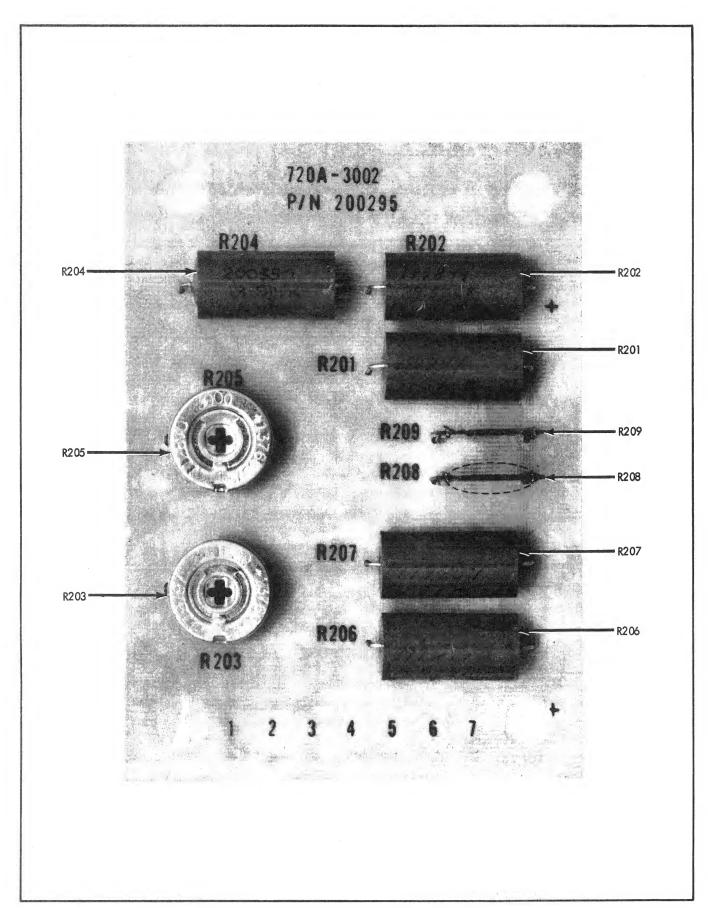


Figure 5-4. BRIDGE P/C ASSEMBLY

REF DESIG	DESCRIPTION	STOCK NO	MFR	MFR PART NO	TOT QTY	REC QTY	USE CODE
	"B" DECADE SWITCH ASSEMBLY Figure 5-5	5110-217307 (720A-4004)	89536	5110-217307	REF		
R401 thru R411	Res, ww, 9.898k, matched set	4					
R412	Res, ww, $39.536k \pm 0.01\%$, 1w	4707-199810	89536	4707-199810	1	1	
S2	Switch, "B", rotary, 3p, 11 pos, 5 sect	5107-218602	89536	5107-218602	2		

These resistors are a factory matched set, part number 4710-217646. If replacement of one or more resistors in the set is required, include all information stamped on the resistor along with the information described in paragraph 5-6. Should the information on the resistor not be discernible, include all of the above information about the adjacent resistors.

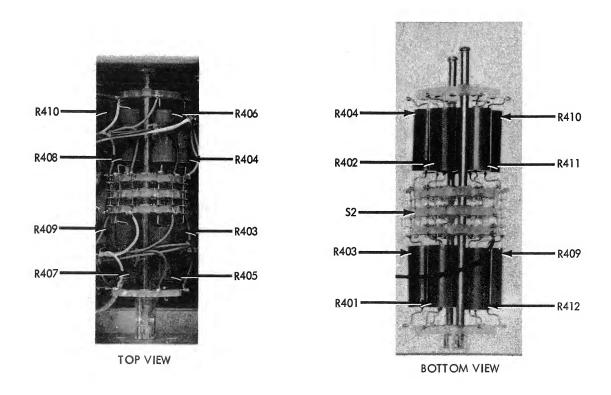


Figure 5-5. "B" DECADE SWITCH ASSEMBLY

REF DESIG	DESCRIPTION	STOCK NO	MFR	MFR PART NO	TOT QTY	REC QTY	USE CODE
	"C" DECADE SWITCH ASSEMBLY Figure 5-6	5110-217315 (720A-4005)	89536	5110-217315	REF		-
R501 thru R511	Res, ww, 4k, matched set	5	:				
R512	Res, ww, $40.31k \pm 0.02\%$, 1w	4707-199836	89536	4707-199836	1	1	
S3	Switch, "C", rotary, 3p, 11 pos, 5 sect	5107-218602	89536	5107-218602	REF		

These resistors are a factory matched set, part number 4710-217653. If replacement of one or more resistors in the set is required, include all information stamped on the resistor along with the information described in paragraph 5-6. Should the information on the resistor not be discernible, include all of the above information about the adjacent resistors.

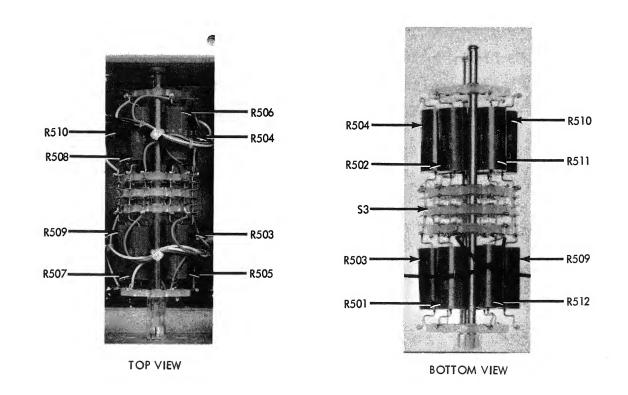


Figure 5-6. "C" DECADE SWITCH ASSEMBLY

REF DESIG	DESCRIPTION	STOCK NO	MFR	MFR PART NO	TOT QTY	REC QTY	USE CODE
	"D", "E", "F", AND "G" DECADES SWITCH ASSEMBLY - Figure 5-7	5110-217323 (720A-4006)	89536	5110-217323	REF		
R601 thru R611	Res, ww, 1k, matched set	6					
R612	Res, ww, 2.5k, matched set	6>					
R701 thru R711	Res, ww, 1k, matched set	6>					
R712	Res, ww, 2.5k, matched set	6>					
R801 thru R811	Res, ww, 1k, matched set	6					
R812	Res, ww, 2.5k, matched set	6>					
R901 thru R910	Res, ww, 1k, matched set	6					
S4	Switch, "D", rotary, 2p, 10 pos, 4 sect	5107-218594	89536	5107-218594	3		
S5	Switch, "E", rotary, 2p, 10 pos, 4 sect	5107-218594	89536	5107-218594	REF		
S6	Switch, "F", rotary, 2p, 10 pos, 4 sect	5107-218594	89536	5107-218594	REF		× .
S7	Switch, "G", rotary, 1p, 11 pos, 3 sect	5107-218586	89536	5107-218586	1		
			· ·				
) ÷			

6

These resistors are a factory matched set, part number 4710-217661. If replacement of one or more resistors in the set is required, include all information stamped on the resistor along with the information described in paragraph 5-6. Should the information on the resistor not be discernible, include all of the above information about the adjacent resistors.

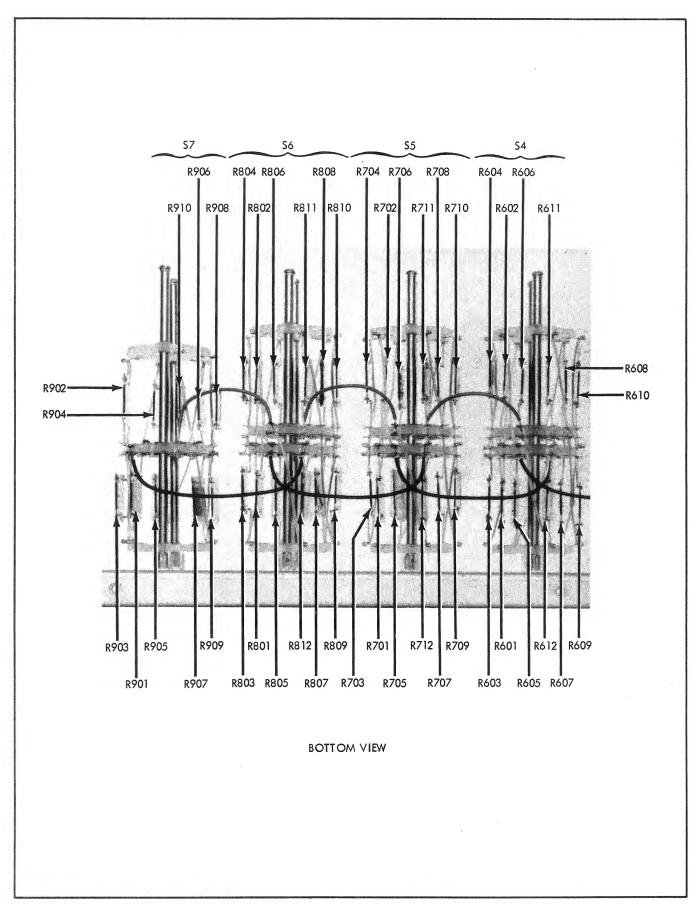


Figure 5-7. "D", "E", "F" AND "G" DECADES SWITCH ASSEMBLY

Section 7

General Information

7-1. This section of the manual contains generalized user information as well as supplemental information to the List of Replaceable Parts contained in Section 5.

D9816 01101 02697 04423 Parker-Hannifin Corp. Telonic Berkley Inc. Westermann Wilhelm Augusta-Anlage Wabash Inc Mannheim-Nackarau Germany (Formerly Wabash Magnetics) O-Ring Div Laguna Beach, CA Lexington, KY Wabash, IN 04713 S0482 Sony Corp. Motorola Inc. RCA-Solid State Div. Tokyo, Japan Allen Bradley Co. Semiconductor Group Milwaukee, WI Somerville, NJ Phoenix, AZ Oshino Electric Lamp Works Tokoyo, Japan TRW Electronics & Defense Sector 02768 Standard Wire and Cable ITW (IL Tool Works) R F Devices Rancho Dominquez, CA 0AD86 Lawndale, CA Fastex Division IN General Des Plaines, IL 05173 El Paso, TX 01295 General Radio TX Instruments Inc. 02799 NY,NY. Semiconductor Group Arco Electronics Inc. Replaced by: Autosplice Inc. Dallas, TX Chatsworth, CA Woodside, NY 01526 03296 24655 Genicom Nylon Molding Corp. Genrad,INC. Noritake Co. Inc. Waynesboro, VA Monrovia, CA Concord, MA Burlington, MA 01537 05236 03445 Motorola Communications & Lercon Electronics Inc Jonathan Mfg. Co. Electronics Inc. Burbank, CA Topaz Semiconductor Inc Fullerton, CA San Jose, CA Franklin Park, IL 05245 General Electric Co. 01686 Corcom Inc. Conductive (Pkg) Containers Inc. RCL Electronics/Shallcross Inc. Semiconductor Products Libertyville, IL Brookfield, WI Electro Components Div. & Batteries Aubum, NY Manchester, NH 05276 ITT Pomona Emhart Fastening Group 01884 03797 Sprague Electric Co. Genisco Technology Corp. Shelton, CT Electronics Div. Eltronics Div. (Now 56289) Pomona, CA Rancho Dominguez, CA 01961 05277 **OFB81** Westinghouse Elec. Corp. S-Mos Systems Inc. Varian Associates Inc. Gilbert Engineering Co.Inc Incon Sub of Transitron Pulse Engineering Div. Convoy, CT Semiconductor Div. San Jose, CA Youngwood, PA Electronic Corp. 0FFP1 Everready LTD Glendale, AZ 05347 Ever Ready Special Battery Div. Cherry Electrical Products Corp Ultronix Inc. Dawley Telford Salop UK Waukegan, IL 03888 Grand Junction, CO KDI Electronics Inc. Pyrofilm Div. 05397 00199 Marcon Electronics Corp Spectrol Electronics Corp. Union Carbide Corp. Whippany, NJ Materials Systems Div. Cleveland. OH Keamy, NJ City of Industry, CA 03911 Clairex Corp. Amperex Electronic Corp. Nytronics Comp. Group Inc. Clairex Electronics Div. 05571 Sprague Electric Co. Mount Vernon, NY Darrlingon, NC Ferrox Cube Div. (Now 56289) Saugerties, NY 03980 02131 Muirhead Inc. Welwyn International Inc. 05574 Westlake, OH General Instrument Corp. Mountainside, NJ Viking Connectors Inc Government Systems Div. Westwood, MA Sub of Criton Corp. Chatsworth, CA Aerovox Corp. Cooper Industries, Inc. New Bedford, MA 02395 Arrow Hart Div. 05791 Sonar Radio Corp. LYN-TRON Hartford, CT Hollywood, FL Burbank, CA Film Capacitors Inc. 04217 Essex International Inc. 02533 Passaic, NJ Leigh Instruments Ltd. Wire & Cable Div. 05820 Frequency Control Div. Anaheim, CA EG & G Wakefield Engineering AMP, Inc. Don Mills, Ontario, Canada Wakefield, MA 04221 Harrisburg, Pennsylvania 05839 02606 Midland-Ross Corp. Advance Electrical 00853 Fenwal Labs Midtex Div. N. Mankato, MN Sangamo Weston Inc Division of Travenal Labs Chicago, IL Components Div Morton Grove, IL Pickens, NC 04222 02660 AVX Corp. 05972 Bunker Ramo-Eltra Corp. AVX Ceramics Div. Loctite Corp.

Myrtle Beach, SC

Newington, CT

Allied Plastics Co.

Los Angeles, CA

Amphenol NA Div.

Broadview, IL

1B715 07047 08111 06001 (United Shoe & Nylock Corp) General Electric Co. Ross Milton Co., The MF Electronics New Rochelle, NY Southampton, PA -Nylock Fastener Corp.-Electric Capacitor Product Paramus, NJ Section Columbia, SC Westinghouse Electric Corp. Industro Transistor Corp. 10059 Barker Engineering Corp. Kenilworth, NJ Industrial & Government Long Island City, NY 06141 Tube Div. Fairchild Weston Systems Inc. Data Systems Div. Horseheads, NY 08261 10389 Spectra-Strip Sarasota, FL IL Tool Works Inc. An Eltra Co. Garden Grove, CA Benchmark Technology Inc. Licon Div. 06192 La Deau Mfg. Co. City of Industry, CA Chicago, IL Glendale, CA Electri-Cord Mfg., Inc 11236 Biddle Instruments Westfield, PA CTS Corp. 06229 Blue Bell, PA Resistor Products Div. Electrovert Inc. Berne, IN Elmsford, NY Reliance Mica Corp. 07256 Silicon Transistor Corp. Brooklyn, NY 11237 06383 Sub of BBF Inc. CTS Corp of CA Panduit Corp. Chelmsford, MA 08718 Electro Mechanical Div. Tinley Park, IL ITT Cannon Electric Paso Robles, CA Phoenix Div. 06473 07261 Bunker Ramo Corp. Amphenol NA Div. 11295 Avnet Corp. Phoenix, AZ ECM Motor Co. Culver City, CA 08806 Schaumburg, IL SAMS Operation General Electric Co. 07263 Chatsworth, CA Minature Lamp Products Fairchild Semiconductor Cleveland, OH Columbia Broadcasting System North American Sales 06540 Mite Corp Amatom-Electrical Div CBS Electronic Div. Ridgeview, CT Newburyport, MA Nylomatic 07344 Fallsington, PA Bircher Co. Inc., The 11403 Vacuum Can Co. Beede Electrical Instrument Rochester, NY Best Coffee Maker Div. Penacook, NH Skottie Electronics Inc. Chicago, IL 07374 Archbald, PA Optron Corp 06665 Woodbridge, CT 11502 (can also use 35009) Precision Monolithics 09021 TRW Inc. Sub of Boums Inc. Airco Inc. TRW Resistive Products Div. 07557 Santa Clara, CA Campion Co. Inc. Boone, NC Airco Electronics Bradford, PA Philadelphia, PA General Devices Co. Inc. Keystone Columbia Inc. 09023 INpolis, IN 07597 Cornell-Dublier Electronics Burndy Corp. Tape/Cable Div. Freemont, IN Fuquay-Varina, NC 11532 Electron Corp. Rochester, NY Teledyne Relays Teledyne 09214 Littleton, CO General Electric Co. Industries Inc. Hawthorne, CA Semiconductor Products Dept. TRW Inc. (Can use 11502) 06743 Aubum, NY Gould Inc. IRC Fixed Resistors/ 11711 Foil Div. Burlington General Instrument Corp. Eastlake, OH Burlington, VT 00353 C and K Components Inc. Rectifier Div. Hicksville, NY Newton, MA 06751 Lerma Engineering Corp. Components Inc. Semoor Div. Northampton, MA 09423 Scientific Components Inc. Santa Barbara, CA Qualidyne Corp. Phoenix, AZ Santa Clara, CA Bock Corp. Madison, WI 09922 Robinson Nugent Inc. Chicago Rivet & Machine Co. Burndy Corp. New Albany, IN Norwalk, CT Naperville, IL Teledyne Semiconductor Mtn. View, CA 09969 12020 06915 Dale Electronics Inc. Ovensine Richco Plastic Co. Div. of Electronic Technologies Yankton, SD Chicago, IL Raytheon Co. Charlottesville, VA Semiconductor Div. 09975 06961 Mountain View, CA Burroughs Corp. 12038 Vernitron Corp. Electronics Components Simco Piezo Electric Div. (Div of Ransburg Corp) Detroit, MI Bedford, OH

1A791

LFE Electronics

Danvers, MA

Calmos Systems Inc.

Kanata, Ont. Canada

Dallas Semiconductor

080A9

Dallas, TX

06980

EIMAC

(See Varian)

San Carlos, CA

Hatfield, PA

Danbury, CT

National Semiconductor Corp.

12060 13050 14704 16473 Diodes Inc. Potter Co. Crydom Controls Cambridge Scientific Industries Northridge, CA Wesson, MS (Division of Int Rectifier) Div. of Chemed Corp. El Segundo, CA Cambridge, MD PHC Industries Inc. Thermalloy Co., Inc. 14752 Formerly Philadelphia Handle Co. Electro Cube Inc. Dallas, TX Cablewave Systems Inc. Camden, NJ San Gabriel, CA North Haven, CT 13327 12300 Solitron Devices Inc. 14936 AMF Canada Ltd. Tappan, NY General Instrument Corp. 16742 Potter-Brumfield Discrete Semi Conductor Div. Paramount Plastics Guelph, Ontario, Canada Hicksville, NY Fabricators Inc. Bunker-Ramo Corp. Downey, CA Amphenol Cadre Div. 14040 Practical Automation Inc. Los Gatos, CA Trompeter Electronics 16758 Shelton, CT Chatsworth, CA General Motors Corp. Delco Electronics Div. 13606 15412 Kokomo, IN Sprague Electric Co. Freeway Corp. Amtron Cleveland, OH (Use 56289) Midlothian, IL Circuit Structures Lab 12406 13680 15542 Burbank, CA SPS Technologies Inc. Elpac Electronics Inc. Scientific Components Corp. Santa Ana, CA Hatfield, NJ Mini-Circuits Laboratory Div. Brooklyn, NY Electronic Molding Corp. Woonsocket, RI Micro Plastics 12443 15636 Budd Co.,The Elec-Trol Inc. Flippin, AZ Plastics Products Div. High Pressure Eng. Co. Inc. Saugus, CA Phoenixville, PA 13919 OK City, OK Burr-Brown Research Corp. Tucson, AZ Bausch & Lomb Inc. Hitachi Metals Inernational Ltd. Graphics & Control Div. Aluminum Filter Co. Hitachi Magna-Lock Div. Austin, TX Carpinteria, CA Semtech Corp. Newbury Park, CA Big Rapids, MO Fenwal Eletronics Inc. Atlantic Semiconductors Inc. US Terminals Inc. Div. of Kidde Inc. Asbury Park, NJ Framingham, MA Cincinnati, OH McGray-Edison Co. Commercial Development Div. Manchester, NH Angstrohm Precision, Inc. Hamlin Inc. Teledyne Inc. Co. Hagerstown, MD LaKe Mills, WI 14189 Teledyne Semiconductor Div. Ortronics, Inc. Mountain View, CA Orlando, FL Siliconix Inc. Wesco Electrical 15849 Santa Clara, CA Greenfield, MA Useco Inc. Cal-R-Inc. (Now 88245) 18178 Santa Monica, CA E G & Gvactee Inc. 15898 St. Louis, MO Clarostat Mfg. Co. Inc. International Business Dover, NH Anderson Electronics Machines Corp. Hollidaysburg, PA Essex Junction, VT KRL/Bantry Components Inc. Manchester, NH James Electronic Inc. Wells Electronics Inc. International Diode Div. 18310 Chicago, IL South Bend, IN Harrison, NJ Concord Electronics 12856 New York, NY MicroMetals Inc. 16162 Watkins-Johnson Co. MMI Anaheim, CA Southfield, MI Palo Alto, CA Signetics Corp. 12881 Sacramento, CA Metex Corp. 16245 Microsemi Corp. Edison, NJ Conap Inc. (Formerly Micro-Semiconductor) Olean, NY 18377 Santa Ana CA Parlex Corp. Cleveland Electric Motor Co. 16258 Methuen, MA Cleveland, OH Space-Lok Inc. Elmwood Sensors, Inc Burbank, CA Sharp Electronics Corp. Pawtucket, RI Microsemi Corp. 16352 Paramus, NJ 14655 Components Group Codi Corp. Comell-Dublier Electronics Linden, NJ Scottsdale, AZ Div. of Federal Pacific Wabash Inc. 12969 Electric Co. Govt Cont Dept. 16469 Wabash Relay & Electronics Div.

MCL Inc.

LaGrange, IL

Wabash, IN

Unitrode Corp.

Lexington, MA

Newark, NJ

18565 2Y384 23732 26402 Tracor Applied Sciences Inc. Chomerics Inc. North American Philips Lighting Corp. Lumex,Inc. Rockville, MD Woburn, MA Van Wert, OH Bayshore, NY 26629 18612 Stanford Applied Engineering Santa Clara, CA Frequency Sources Inc. Enochs Mfg. Inc. Vishay Intertechnology Inc. Vishay Resistor Products Group INpolis, IN Sources Div. Chelmsford, MA Malvem, PA 20891 23936 Cosar Corp. William J. Purdy Co. Norton-Chemplast Dallas, TX Pamotor Div. American Zettler Inc. Santa Monica, CA Burlingame, CA Irvine, CA 21317 Electronics Applications Co. 27014 National Semiconductor Corp. Scanbe Mfg. Co. El Monte, CA 24347 Div. of Zero Corp. Penn Engineering Co. Santa Clara, CA S. El Monte, CA El Monte, CA 21604 Buckeye Stamping Co. Columbus, OH 24355 Coming Glass Works Corning 18736 Voltronics Corp. Analog Devices Inc. Electronics Norwood, MA East Hanover, NJ 21845 Wilmington, NC Solitron Devices Inc. Semiconductor Group 24444 27264 Molex Inc. 18786 Rivera Beach, FL General Semiconductor Micro-Power Industries, Inc. Lisle, IL Long Island City, NY 21847 Tempe, AZ Acrtech 27440 Now TRW Microwave Inc. 24546 Industrial Screw Products GTE Products Corp. Bradford Electronics Sunnyvale, CA Los Angeles, CA Bradford, PA Precision Material Products 21962 27494 Business Parts Div. Vectron Corp.
Replaced by: S.W. Electronics Staffall, Inc. 24618 Titusville.PA Transcon Mfg. Providence, RI Now: D.J. Associates Inc. Robinson Electronics Inc. DuPont, El DeNemours & Co. Inc. San Luis Obispo, CA 27745 Genrad Inc. (Replaced General Radio 05173) DuPont Connector Systems Associated Spring Barnes Group Inc. 19112 Advanced Products Div. Syracuse, NY Garry Corp. New Cumberland, PA Concord, MA Langhome, PA 22626 24750 Component Parts Corp. Micro Semiconductor Lenox-Fugle Electronics Inc. Bellmore, NY Bendix Corp., The (Now 14552) South Plainfield, NJ Navigation & Control Group 27956 Terboro, NJ 22670 24796 Relcom (Now 14482) GM Nameplate AMF Inc. Seattle, WA Potter & Brumfield Div. 28175 Perine Machine Tool Corp. San Juan Capistrano, CA Alpha Metals Kent, WA Chicago, IL ITT Semiconductors Specialty Connector Co. 28198 Palo Alto, CA Delta Electronics Greenwood, IN Positronic Industries Alexandria, VA Springfield, MO 22784 24995 Palmer Inc. ECS MN Mining & Mfg. Co. Textool Products Dept. MN Mining & Mfg. Co. Consumer Products Div. Cleveland, OH Grants Pass, OR Electronic Product Div. 23050 25088 3M Center Irving, TX Saint Paul, MN Product Comp. Corp. Siemen Corp. Mount Vernon, NY Isilen, NJ 28309 Caddock Electronics Inc. 23223 25099 Kaiser CTS Microelectronics Cascade Gasket Minette.AL. Riverside, CA Kent, WA Lafayette, NY 28425 Mepco/Centralab Inc. 23237 25403 Serv-O-Link Amperex Electronic Corp.
Semiconductor & Micro-Circuit Div.
Slatersville, RI I.R.C., Inc. A N. American Philips Co. Euless, TX Mineral Wells, TX Microcircuits Divison Philadelphia, PA 28478 Deltrol Corporation Deltrol Controls Div. 23302 25435 2B178 S.W. Electronics & Mfg. Corp. Wire Products Moldtronics, Inc Milwaukee, WI Cherry Hill, NJ Downers Grove, IL Cleveland, OH 28480 23730 Hewlett Packard Co. Boyd Corporation Mark Eyelet and Stamping Inc. Dabum Electronic & Cable Corp. Corporate HQ

Norwood, NJ

Portland, OR

Wolcott, CT

Palo Alto, CA

28484 31433 33246 36701 Van Waters & Rogers Emerson Electric Co. Kemet Electonics Corp. Epoxy Technology Inc. Gearmaster Div. Simpsonville, NC Billerica, MA Valley Field, Quebec, Canada McHenry, IL Army Safeguard Logistics Command Pioneer Sterilized Wiping Cloth Co. Mallory Capacitor Corp. Sub of Emhart Industries 28520 Heyco Molded Products Huntsville, AL Portland, OR Kenilworth, NJ INpolis, IN 31471 33297 28932 Gould Inc. NEC Electronics USA Inc. 39003 Lumax Industrials, Inc Semiconductor Div Electronic Arrays Inc. Div. Maxim Industries Mountain View. CA Middleboro, MA Altoona, PA Santa Clara, CA 33010 4F434 29083 31522 Monsanto Co. Metal Masters Inc. Nortek Inc. Plastic Sales Santa Clara, CA Cranston, RI Los Angeles, CA Baldwin, MS 31746 40402 Stackpole Components Co. Cannon Electric 34114 Roderstein Electronics Inc. Raleith, NC Oak Industries Statesville, NC Woodbury, TN Rancho Bemardo, CA 42498 29907 31827 Omega Engineering Inc. National Radio Budwig CTS Electronics Corp. Stamford, CT Ramona, CA Melrose, MA Brownsville,TX 3D536 31918 43543 Aimsco Inc. **ITT-Schadow** 34333 Nytronics Inc.(Now 53342) Silicon General Inc. Eden Prairie, MN Seattle, WA 43744 Garden Grove, CA Panasonic Industrial Co. 30035 32293 Jolo Industries Inc. Intersil San Antonio, TX Cupertino, CA Advanced Micro Devices (AMD) Garden Grove, CA Sunnyvale, CA 43791 32539 Datron Systems Solid Power Corp. Mura Corp. 34359 Wilkes Barre, PA MN Mining & Mfg. Co. Commercial Office Supply Div. Westbury, Long Island, N.Y. Farmingdale, NY 44655 Ohmite Mfg. Co. 30146 32559 Saint Paul, MN Symbex Corp. Painesville, OH Bivar Skokie, IL Santa Ana, CA 34371 Harris Corp. 47001 32719 Harris Semiconductor Lumberg Inc. AB Enterprise Inc. Siltronics Products Group Richmond, VA Ahoskie, NC Santa Ana, CA Melbourne, FL 47379 34576 ISOCOM Griffith Plastics Corp. Aavid Engineering Inc. Rockwell International Corp. Campbell, CA Laconia, NH Burlingame, CA Newport Beach, CA IDT (International Development & Trade) Itron Corp. Advanced Mechanical Components Instrument Specialties Dallas, TX San Diego, CA Northridge, CA Euless, TX RCA Corp. New York, NY 34649 IL Tool Works Inc. Murata Erie North America Inc. Intel Corp. Chicago, IL Carlisle Operations Santa Clara, CA Carlisle, Pennsylvania 49956 34802 Raytheon Company General Instrument Corp. 32997 Electromotive Inc. **Executive Offices** Bourns Inc. Kenilworth, NJ Capacitor Div. Lexington, MA Hicksville, NY Trimpot Div. Riverside, CA 34848 5D590 Hartwell Special Products Mostek Corp. Placentia, CA Replaced by: SGS Thompson Microelec Fastec Chicago,ILL M/A ComOmni Spectra, Inc. (Replacing Omni Spectra) Microwave Subsystems Div. 31019 Renfrew Electric Co. Ltd. 5F520 Panel Components Corp. Santa Rosa, CA Solid State Scientific Inc. Tempe, AZ IRC Div. Willow Grove, PA Toronto, Ontario, Canada 35986 Alpha Industries Inc. CO Crystal Corp. Nobel Electronics Amrad Melrose Park, IL Microelectronics Div. Loveland, CO Suffem, NY Hatfield, PA 36665 5W664 33173 General Electric Co. Mitel Corp. NDK Div. of Nihon Dempa Kogyo LTD Metro Supply Company Kanata, Ontario, Canada Owensboro, KY

Lynchburg, VA

Sacramento, CA

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56481 59610 60911 64537 Shugart Associates Souriau Inc Inmos Corp. KDI Electronics Sub of Xerox Corp. Valencia, CA CO Springs, CO Whippany, NJ Sunnyvale, CA 60935 **HV** Component Associates Precision Control Mfg. Inc. Westlake Capacitor Inc. RCD Components Inc. Howell, NJ Tantalum Div. Bellevue, WA Manchester, NH Greencastle, IN 59640 64834 56708 Supertex Inc. 60958 West M G Co. Zilog Inc. Sunnyvale, CA ACIC San Francisco, CA Campbell, CA Intercomp Wire & Cable Div. 59660 Hayesville, NC 56856 Tusonix Inc. 64961 Vamistor Corp. of TN Tucson, AZ 61271 Electronic Hardware LTD Sevierville, TN Fujitsu Microelectronics Inc North Hollywood, CA San Jose, CA Thomas and Betts Corp. 56880 IA City, IA 61394 Sangamo Weston Inc. SEEQ Technology Inc. Magnetics Inc. Weston Instruments Div. Baltimore, MD San Jose, CA Newark, NJ Semtronics Corp. 57026 Watchung, NJ 61429 65786 Endicott Coil Co. Inc. Fox Electronics Cypress Semi Binghamton, NY Cape Coral, FL San Jose, CA American Components Inc. an Insilco Co. RPC Div. 61529 65940 Gates Energy Products Hayesville, NC Aromat Corp. Rohm Corp & Whatney Denver, CO New Providence, NJ Irvine, CA 57170 Allen, Robert G. Inc. 61752 65964 Cambridge Thermionic Van Nuys, CA IR-ONICS Inc Evox Inc. Cambridge, MA Warwick, RI Bannockburn, IL Replaced by: Burgess Switch Co., Inc 61772 66150 Interconnection Products Inc. Northbrook, IL Integrated Device Technology Entron Inc. Santa Clara, CA Winslow Teltronics Div. Glendale, NY R-ohm Corp AMD Enterprises, Inc. 61802 Irvine, CA Roswell, GA Toshiha Houston, TX 66302 VLSI Technology Inc. SGS - Thomson Microelectronics Inc SGS/ATES Semiconductor Corp. 61857 San Jose, CA Montgomeryville, PA SAN-O Industrial Corp. INpolis, IN Bohemia, Long Island, NY 66419 Exel Hitachi Magnalock Corp. Micron Technology Inc. 61935 San Jose, CA (Now 12581) Boise, ID Schurter Inc. Petaluma, CA 58104 Dyna-Tech Electronics, Inc Power Dynamics Inc Simco 62351 Walled Lake, MI Atlanta, GA West Orange, NJ Apple Rubber Lancaster, NY 58364 60197 Bering Industries BYCAP Inc. Precicontact Inc. 62643 Freemont, CA Chicago, IL Langhome, PA United Chemicon Rosemont, IL **BKC** International Electronics Precision Lamp Squires Electronics Inc 62712 Lawrence, MA Cornelius, OR Cotat, CA Seiko Instruments Torrance, CA 60395 SGS Semiconductor Corp. 58474 Xicor Inc. 62793 Phoenix, AZ Superior Electric Co. Milpitas, CA Lear Siegler Inc. Bristol, CT Energy Products Div. Santa Ana, CA 66967 58614 Torin Engineered Blowers Powerex Inc Communications Instruments Inc. Div. of Clevepak Corp. Aubum, NY Fairview, NC Torrington, CT Ward Leonard Electric Co.Inc. Mount Vernon, NY 67183 60496 Altera KOA-Speer Electronics Inc. Micrel Inc. 64154 Santa Clara, CA Bradford, PA Sunnyvale, CA Lamb Industries Portland, OR 68919 60705 WIMA Holmberg Electronics Cera-Mite Corp. % Harry Levinson Co. Seattle, WA 64155 (formerly Sprague) Linear Technology Irvine, CA

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U.S. Service Locations

California

Fluke Technical Center 16969 Von Karman Avenue Suite 100 Irvine, CA 92714 Tel: (714) 863-9031

Fluke Technical Center 46610 Landing Parkway Fremont, CA 94538 Tel: (415) 651-5112

Colorado

Fluke Technical Center 14180 East Evans Avenue Aurora, CO 80014 Tel: (303) 695-1171

Florida

Fluke Technical Center 940 N. Fern Creek Avenue Orlando, FL 32803 Tel: (407) 896-4881

Illinois

Fluke Technical Center 1150 W. Euclid Ave. Palatine, IL 60067 Tel: (312) 705-0500

Maryland

Fluke Technical Center 5640 Fishers Lane Rockville, MD 20852 Tel: (301) 770-1576

New Jersey

Fluke Technical Center East 66 Midland Avenue Paramus, NJ 07652-0930 Tel: (201) 599-9500

Fluke Technical Center 1801 Royal Lane, Suite 307 Dallas, TX 75229 Tel: (214) 869-2848

Washington

Fluke Technical Center John Fluke Mfg. Co., Inc. 1420 75th St. S.W. M/S 6-30 Everett, WA 98203 Tel: (206) 356-5560

International

Argentina

Coasin S.A. Virrey del Pino 4071 DPTO E-65 1430 CAP FED Buenos Aires Tel: 54 1 522-5248

Australia

Philips Customer Support Scientific and Industrial 23 Lakeside Drive Tally Ho Technology Park East Burwood 3151 Victoria

Australia

Philips Customer Support Scientific & Industrial 25-27 Paul St. North North Ryde N.S.W. 2113 Tel: 61 02 888 8222

Oesterreichische Philips Industrie Unternehmensbereich Prof. Systeme Triesterstrasse 66 Postfach 217 A-1101 Wein Tel: 43 222-60101, x1388

Philips & MBLE Associated S.A. Scientific & Industrial Equip. Div Service Department. 80 Rue des deux Gares B-1070 Brussels Tel: 32 2 525 6111

Brazil

Hi-Tek Electronica Ltda. Al. Amazonas 422, Alphaville CEP 06400 Barueri Sao Paulo Tel: 55 11 421-5477

Canada

Fluke Electronics Canada Inc. 400 Britannia Rd. East, Unit #1 Mississauga Ontario L4Z 1X9 Tel: 416-890-7600

Chile

Intronica Chile Ltda. Casilla 16228 Santiago 9 Tel: 56 2 2321886, 2324308

China

Fluke International Corp. P.O. Box 9085 Beijing Tel: 86 01 512-3436

Colombia

Sistemas E Instrumentacion, Ltda. Carrera 13, No. 37-43, Of. 401 Ap. Aereo 29583 Booota DE Tel: 57 232-4532

Denmark

Philips A/S Technical Service I & E Strandlodsveij 1A PO Box 1919 DK-2300 Copenhagen S Tel: 45 1 572222

Ecuador

Proteco Coasin Cia., Ltda. P.O. Box 228-A Ave. 12 de Octubre 2285 y Orellana Quito Tel: 593 2 529684

Egypt

Philips Egypt 10, Abdel Rahman el Rafei st. el. Mohandessin P.O. Box 242 Dokki Cairo Tel: 20-2-490922

England

Philips Scientific Test & Measuring Division Colonial Way Watford Hertforshire WD2 4TT Tel: 44 923-40511

Finland

Oy Philips AB Central Service Sinikalliontie 1-3 P.O. Box 11 SF-02630 ESPOO Tel: 358-0-52572

France

S.A. Philips Industrielle et Comerciale. Science et Industry 105 Rue de Paris Bp 62 93002 Bobigny, Cedex Tel: 33-1-4942-8040

Germany (F.R.G.) Philips GmbH

Service fuer FLUKE - Produkte Department VSF Oskar-Messter-Strasse 18 D-8045 Ismaning/Munich, West Germany Tel: 49 089 9605-239

Greece

Philips S.A. Hellenique 15, 25th March Street 177 78 Tayros 10210 Athens Tel: 30 1 4894911

Hong Kong Schmidt & Co (H.K.) Ltd. 18/FL., Great Èagle Centre 23 Harbour Road Wanchai Tel: 852 5 8330222

Hinditron Services Pvt. Ltd 1st Floor, 17-B, Mahal Industrial Estate Mahakali Road, Andheri East Bombay 400 093 Tel: 91 22 6300043

Hinditron Services Pvt. Inc. 33/44A Raj Mahal Villas Extn. 8th Main Road Bangalore 560 080 Tel: 91 812 363139

Hinditron Services Pvt. Ltd. Field Service Center Emerald Complex 1-7-264 5th Floor 114 Sarojini Devi Road Secunderabad 500 003

Hindtron Services Pvt. Ltd. 15 Community Centre Panchshila Park New Delhi 110 017 Tel: 011-6433675

Tel: 08 42-821117

Indonesia

P.T. Lamda Triguna P.O. Box 6/JATJG Jakarta 13001 Tel: (021) 8195365

Israel

R.D.T. Electronics Engineering, Ltd. P.O. Box 43137 Tel Aviv 61430 Tel: 972 3 483211

Italy Philips S.p.A. Sezione I&E / T&M Viale Elvezia 2 2005 Monza Tel: 39 39 3635342

Japan John Fluke Mg. Co., Inc. Japan Branch Sumitomo Higashi Shinbashi Bldg. 1-1-11 Hamamatsucho Minato-ku Tokyo 105 Tel: 81 3 434-0181

Korea

Myoung Corporation Yeo Eui Do P.O. Box 14 Seoul 150 Tel: 82 2 784-9942

Malaysia

Mecomb Malaysia Sdn. Bhd. P.O. Box 24 46700 Petaling Jaya Selangor Tel: 60 3 774-3422

Mexel Servicios en Computacion Instrumentacion y Perifericos Blvd. Adolfo Lopez Mateos No. 163 Col. Mixcoac Mexico D.F. Tel: 52-5-563-5411

Netherlands

Philips Nederland Test & Meetapparaten Div. Postbus 115 5000 AC Tilburg Tel: 31-13-352445

New Zealand

Philips Customer Support Scientific & Industrial Division 2 Wagener Place Mt. Albert Auckland Tel: 64 9 894-160

Norway Morgenstierne & Co. A/S Konghellegate 3 P.O. Box 6688, Rodelokka Oslo 5 Tel: 47 2 356110

Pakistan

International Operations (PAK) Ltd. 505 Muhammadi House I.I. Chundrigar Road P.O. Box 5323 Karachi Tel: 92 21 221127, 239052

Importaciones & Representaciones Electronicas S.A. Avad Franklin D. Roosevelt 105 Lima 1 Tel: 51 14 288650

Philippines

Spark Radio & ElectronicS Inc. Greenhills, P.O. Box 610 San Juan, Metro-Manila Zip 3113 Tel: 63-2-775192

Decada Espectral Equipmentos de Elec. e Científicos Av. Bomberios Voluntarios Lote 102B, Miraflores/Alges 1495 Lisboa Tel: 351 1 410-3420

Singapore

Rank O'Connor's Singapore (PTE) Ltd. 98 Pasir Panjang Road Singapore 0511 Tel: 65 4737944

South Africa

South African Philips (Pty) Ltd. Service Department 195 Main Rd Martindale, Johannesburg, 2092 Tel: 27 11 470-5255

Philips Iberica S.A.E. Depto. Tecnico Instrumentacion c/Martinez Villergas 2 28027 Madrid Tel: 34 1 4042200

Philips Kistaindustrier AB Customer Support Borgarfjordsgatan 16 S-16493 Kista

Switzerland

Philips A.G. Technischer Kundendienst Postfach 670 Allmendstrasse 140 CH-8027 Zurich Tel: 41 1 482211

Taiwan

Schmidt Electronics Corp. 5th Floor, Cathay Min Sheng Commercial Building, 344 Min Sheng East Road Taipei Tel: 886 2501-3468

Thailand

Measuretronix Ltd. 2102/63 Ramkamhaeng Rd. Bangkok 10240 Tel: 66 2 374-2516, 374-1632

Turkey Turk Philips Ticaret A.S. Inonu Caddesi 78/80 Posta Kutusu 504-Beyoglu Istanbul Tel: 90 1 1435891

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Venezuela

Coasin C.A. Calle 9 Con Calle 4, Edif. Edinurbi Apartado de Correos Nr-70-136 Los Ruices Caracas 1070-A Tel: 58 2 241-0309, 241-1248

West Germany

Philips GmbH Department VSF Service fuer FLUKE - Produkte Oskar - Messter - Strasse 18 D-8045 Ismaning / Munich Tel: 49 089 9605-260

