

ICC-ES Evaluation Report

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This report also contains:

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- City of LA Supplement

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- FL Supplement w/HVHZ

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DIVISION: 03 00 00 — CONCRETE

Section: 03 16 00 — Concrete Anchors

DIVISION: 05 00 00 —

METALS

Section: 05 05 19 — Post-Installed Concrete

Anchors

REPORT HOLDER:

DEWALT



EVALUATION SUBJECT:

PURE220+TM ADHESIVE ANCHOR SYSTEM AND POST-INSTALLED REINFORCING BAR IN CRACKED AND UNCRACKED CONCRETE (DEWALT)



1.0 EVALUATION SCOPE

Compliance with the following codes:

- 2024, 2021, 2018 and 2015 *International Building Code*® (IBC)
- 2024, 2021, 2018 and 2015 International Residential Code® (IRC)

Main references of this report are for the 2024 IBC and IRC. See Table 22 and Table 23 for applicable sections of the code for previous IBC and IRC editions

Property evaluated:

Structural

2.0 USES

DEWALT Pure220+ adhesive anchor system is used as anchorage to resist static, wind or earthquake (IBC Seismic Design Categories A through F) tension and shear loads in cracked and uncracked normal-weight and lightweight concrete with $^{3}/_{8^{-}}$, $^{1}/_{2^{-}}$, $^{5}/_{8^{-}}$, $^{3}/_{4^{-}}$, $^{7}/_{8^{-}}$, 1-, and $^{11}/_{4^{-}}$ inch fractional diameter, and M10, M12, M16, M20, M24, M27 and M30 metric diameter threaded steel rods and No. 3 through No. 10 fractional size and Ø10, Ø12, Ø14, Ø16, Ø20, Ø25, Ø28 and Ø32 EU metric size, and 10M, 15M, 20M, 25M, and 30M Canadian metric size steel reinforcing bars in hammer-drilled holes (or DEWALT hollow drill bit system). Use is limited to normal-weight and lightweight concrete with a specified compressive strength, f_c , of 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).

DEWALT Pure220+ adhesive anchor system is used as anchorage to resist static, wind or earthquake (IBC Seismic Design Categories A through F) tension and shear loads in cracked and uncracked normal-weight and lightweight concrete with $^{3}/_{8^{-}}$, $^{1}/_{2^{-}}$, $^{5}/_{8^{-}}$, $^{3}/_{4^{-}}$, $^{7}/_{8^{-}}$, 1-, and $^{11}/_{4^{-}}$ inch fractional diameter threaded steel rods in diamond core-drilled holes. Use is limited to normal-weight and lightweight concrete with a specified compressive strength, f_{c} , of 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).

DEWALT Pure220+ adhesive anchor system is used as anchorage to resist static, wind or earthquake (IBC Seismic Design Categories A and B only) tension and shear loads in uncracked normal-weight and lightweight concrete with No. 3 through No. 10 fractional size steel reinforcing bars in diamond core-drilled holes. Use is limited to normal-weight and lightweight concrete with a specified compressive strength, f_c , of 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).





DEWALT Pure220+ adhesive post-installed reinforcing bars are used as reinforcing bar connections (for development lengths and non-contact splice lengths) to resist static, wind and earthquake (IBC Seismic Design Categories A through F) tension loads in concrete with No. 3 through No. 11 fractional size and \emptyset 10, \emptyset 12, \emptyset 14, \emptyset 16, \emptyset 20, \emptyset 25, \emptyset 28, \emptyset 32 and \emptyset 36 EU metric size, and 10M, 15M, 20M, 25M, and 30M Canadian metric size steel reinforcing bars in hammer-drilled (or DEWALT hollow drill bit system) and diamond core drilled holes. Use is limited to normal-weight concrete with a specified compressive strength, f_c , of 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).

The anchor system complies with anchors as described in Section 1901.3 of the 2024 IBC. The anchor systems may also be used where an engineered design is submitted in accordance with Section R301.1.3 of the IRC.

The post-installed reinforcing bar connection system is an alternative to cast-in-place reinforcing bars governed by ACI 318 and IBC Chapter 19.

3.0 DESCRIPTION

3.1 General:

The DEWALT Pure220+ Adhesive Anchor System is comprised of two-component adhesive filled in cartridges, static mixing nozzles and manual or powered dispensing tools, hole cleaning equipment and adhesive injection accessories, and steel anchor elements, which are continuously threaded steel rods or steel reinforcing bars (to form the DEWALT Pure220+ Adhesive Anchor System).

The primary components of the DEWALT Pure220+ Adhesive Anchor System, including the adhesive cartridge, static mixing nozzle, dispenser, and steel anchor elements, are shown in <u>Figure 2</u> of this report. The manufacturer's printed installation instructions (MPII), included with each adhesive unit package, are shown in <u>Figure 4</u> of this report.

3.2 Materials:

3.2.1 DEWALT Pure220+ Adhesive: DEWALT Pure220+ adhesive is an injectable two-component epoxy adhesive. The two components are kept separate by means of a labelled dual-cylinder cartridge. The two components combine and react when dispensed through a static mixing nozzle, supplied by DEWALT, which is attached to the cartridge. DEWALT Pure220+ adhesive is available in 9.5-ounce (280 mL), 13.5-ounce (400 mL), 20.5-ounce (610 mL) and 50.5-ounce (1500 mL) cartridges. Each cartridge label is marked with the adhesive expiration date. The shelf life, as indicated by the expiration date, applies to an unopened cartridge stored in a dry, dark, and cool environment, in accordance with the MPII, as illustrated in Figure 4 of this report.

3.2.2 Hole Cleaning Equipment:

- **3.2.2.1 Standard Equipment:** Hole cleaning equipment is comprised of steel wire brushes supplied by DEWALT, and air blowers which are shown in <u>Figure 4</u> of this report. The DEWALT dust extraction system shown in <u>Figure 1</u> of this report removes dust with a HEPA dust extractor during the hole drilling and cleaning operation.
- **3.2.2.2 DEWALT Hollow Drill Bit System (DustX+™):** The DEWALT hollow drill bit system shown in Figure 1 is comprised of DEWALT hollow drill bits with carbide tips conforming to ANSI B212.15 attached to a HEPA vacuum that has a minimum air flow rating of 90 cfm (150 m³/h, 42 l/s), e.g. DWV015, DWV905M, DWV905H or equivalent approved by DEWALT (applicable for both post-installed adhesive anchor system and post-installed reinforcing bar connections). The vacuum dust extractor system removes the drilling dust during the drilling operation, eliminating the need for additional hole cleaning.
- **3.2.3 Dispensers:** DEWALT Pure220+ adhesive must be dispensed with manual dispensers, pneumatic dispensers, or electric powered dispensers supplied by DEWALT.

3.2.4 Steel Anchor Elements:

3.2.4.1 Threaded Steel Rods: Threaded steel rods must be clean and continuously threaded (all-thread) in diameters described in <u>Tables 4</u> and <u>12</u> and <u>Figure 4</u> of this report. Specifications for grades of threaded rod, including the mechanical properties, and corresponding nuts and washers, are included in <u>Table 2</u> of this report. Carbon steel threaded rods may be furnished with a minimum 0.0002-inch-thick (0.005 mm) zinc electroplated coating complying with ASTM B633 SC1 or a minimum 0.0021-inch-thick (0.053 mm) mechanically deposited zinc coating complying with ASTM B695, Class 55. The stainless-steel threaded rods must comply with <u>Table 2</u> of this report. Steel grades and types of material (carbon, stainless) for the washers and nuts must match the threaded rods. Threaded steel rods must be clean, straight, and free of indentations or other defects along their length. The embedded end may be flat cut or cut on the bias to a chisel point.

- **3.2.4.2 Steel Reinforcing Bars:** Steel reinforcing bars are deformed reinforcing bars as described in Table 3 of this report. Tables 8 and 15, and Figure 4 summarize reinforcing bar size ranges. The embedded portions of reinforcing bars must be clean, straight, and free of mill scale, rust, mud, oil, and other coatings (other than zinc) that may impair the bond with the adhesive. Reinforcing bars must not be bent after installation except as set forth in ACI 318-19 Section 26.6.3.2 (b), with the additional condition that the bars must be bent cold, and heating of reinforcing bars to facilitate field bending is not permitted.
- **3.2.4.3 Ductility:** In accordance with ACI 318-19 Section 2.3 in order for a steel anchor element to be considered ductile, the tested elongation must be at least 14 percent and reduction of area must be at least 30 percent. Steel elements with a tested elongation less than 14 percent or a reduction of area less than 30 percent, or both, are considered brittle. Values for various steel materials are provided in <u>Table 2</u> of this report. Where values are nonconforming or unstated, the steel must be considered brittle.
- **3.2.4.4 Steel Reinforcing Bars for use in Post-Installed Reinforcing Bar Connections:** Steel reinforcing bars used in post-installed reinforcing bar connections are deformed reinforcing bars (rebar), with size ranges summarized in <u>Tables 19</u>, <u>20</u> and <u>21</u>. The embedded portions of reinforcing bars must be straight, and free of mill scale, rust and other coatings that may impair the bond with the adhesive. Reinforcing bars must not be bent after installation except as set forth in ACI 318-19 Section 26.6.3.2 (b) with the additional condition that the bars must be bent cold, and heating of reinforcing bars to facilitate field bending is not permitted.

3.3 Concrete:

Normal-weight and lightweight concrete must comply with Sections 1903 and 1905 of the IBC. The specified compressive strength of the concrete must be from 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).

4.0 DESIGN AND INSTALLATION

4.1 Strength Design:

4.1.1 General: The design strength of anchors under the 2024 IBC, as well as the 2024 IRC, must be determined in accordance with ACI 318-19 and this report.

The strength design of anchors must comply with ACI 318-19 17.5.1.2, except as required in ACI 318-19 17.10.

Design parameters are provided in <u>Tables 4</u> through <u>18</u> of this report. Strength reduction factors, ϕ , as given in ACI 318-19 17.5.3, must be used for load combinations calculated in accordance with Section 1605.1 of the 2024 IBC or ACI 318-19 5.3.

- **4.1.2 Static Steel Strength in Tension:** The nominal static steel strength of a single anchor in tension, N_{sa} , in accordance with ACI 318-19 17.6.1.2 and the associated strength reduction factors, ϕ , in accordance with ACI 318-19 17.5.3 are provided in <u>Tables 4</u>, <u>8</u>, <u>12</u> and <u>15</u> of this report for the corresponding anchor steel.
- **4.1.3 Static Concrete Breakout Strength in Tension:** The nominal static concrete breakout strength of a single anchor or group of anchors in tension, *N_{cb}* or *N_{cbg}*, must be calculated in accordance with ACI 318-19 17.6.2 with the following addition:

The basic concrete breakout strength of a single anchor in tension, N_b , must be calculated in accordance with ACI 318-19 17.6.2.2 using the values of $k_{c,cr}$ and $k_{c,uncr}$ as provided in Tables 5, 9, 13, and 16 of this report. Where analysis indicates no cracking in accordance with ACI 318-19 17.6.2.5, N_b must be calculated using $k_{c,uncr}$ and $\Psi_{c,N} = 1.0$. For anchors in lightweight concrete see ACI 318-19 17.2.4. The value of f_c used for calculation must be limited to 8,000 psi (55 MPa) in accordance with ACI 318-19 17.3.1. Additional information for the determination of nominal bond strength in tension is given in Section 4.1.4 of this report.

4.1.4 Static Bond Strength in Tension: The nominal static bond strength of a single adhesive anchor or group of adhesive anchors in tension, N_a or N_{ag} , must be calculated in accordance with ACI 318-19 17.6.5.

Bond strength values ($\tau_{k,cr}$, $\tau_{k,uncr}$) are a function of concrete compressive strength, concrete state (cracked, uncracked), drilling method (hammer-drilled, core-drilled), and installation conditions (dry concrete, water-saturated concrete, water-filled holes, submerged concrete). Special inspection level is qualified as periodic for all anchors except as noted in Section 4.4 of this report. The selection of continuous special inspection level, with an onsite proof loading program, is not necessary and does not provide a benefit of a lower anchor category or an increase in the associated strength reduction factors for design. The following table summarizes the requirements:

CONCRETE STATE	DRILLING METHOD	BOND STRENGTH	CONCRETE COMPRESSIVE STRENGTH	PERMISSIBLE INSTALLATION CONDITIONS	ASSOCIATED STRENGTH REDUCTION FACTOR
	Hammer-drill with carbide drill bit or			Dry concrete	$\phi_{ extsf{d}}$
Cracked and	DEWALT hollow bit	Tk,cr Of Tk,uncr	f 'c	Water-saturated concrete	$\phi_{ m ws}$
Uncracked	Hammer-drill with carbide drill bit			Water-filled hole (flooded)	$K_{\it wf}\cdot\phi_{\it wf}$
				Underwater (submerged)	$\phi_{ m uw}$
Cracked and	Core-drill with		<i>t</i> (Dry concrete	фа
Uncracked	diamond core bit	Tk,cr Or Tk,uncr	f 'c	Water-saturated concrete	<i>∲</i> ws

Strength reduction factors for determination of the bond strength are given in <u>Tables 6, 7, 10, 11, 14, 17</u> and <u>18</u> of this report. Adjustments to the bond strength may also be made for increased concrete compressive strength as noted in the footnotes to the corresponding tables and this section.

The bond strength values in <u>Tables 6</u>, $\underline{7}$, $\underline{10}$, $\underline{11}$, $\underline{14}$, $\underline{17}$ and $\underline{18}$ of this report correspond to concrete compressive strength f_c equal to 2,500 psi (17.2 MPa).

For concrete compressive strength, f_c between 2,500 psi and 8,000 psi (17.2 MPa and 55 MPa), the tabulated characteristic bond strength in hammer-drilled (or DEWALT hollow drill bit system) holes may be increased by the following as follows: threaded rod in uncracked concrete by $(f_c/2,500)^{0.21}$ [For SI: $f_c/17.2)^{0.21}$]; threaded rod in cracked concrete by $(f_c/2,500)^{0.14}$ [For SI: $f_c/17.2)^{0.14}$]; fractional and EU metric reinforcing bar in uncracked concrete by $(f_c/2,500)^{0.09}$ [For SI: $f_c/17.2)^{0.09}$]; Canadian metric reinforcing bar in cracked concrete by $(f_c/2,500)^{0.09}$ [For SI: $f_c/17.2)^{0.09}$]; Canadian metric reinforcing bar in cracked concrete by $(f_c/2,500)^{0.08}$ [For SI: $f_c/17.2)^{0.09}$]

For concrete compressive strength, f_c between 2,500 psi and 8,000 psi (17.2 MPa and 55 MPa), the tabulated characteristic bond strength in diamond core drilled holes may be increased as follows: threaded rod in uncracked concrete by $(f_c/2,500)^{0.24}$ [For **SI**: $f_c/17.2)^{0.24}$]; threaded rod in cracked concrete by $(f_c/2,500)^{0.20}$ [For **SI**: $f_c/17.2)^{0.20}$]; and fractional and EU metric reinforcing bar in uncracked concrete by $(f_c/2,500)^{0.35}$ [For **SI**: $f_c/17.2)^{0.35}$].

Where applicable, the modified bond strength values must be used in lieu of $\tau_{k,cr}$ and $\tau_{k,uncr}$ in ACI 318-19 (17.6.5.1.2b) and (17.6.5.2.1).

The resulting nominal bond strength must be multiplied by the associated strength reduction factor ϕ_d , ϕ_{ws} , ϕ_{wf} or ϕ_{uw} , as applicable.

- **4.1.5 Static Steel Strength in Shear:** The nominal static steel strength of a single anchor in shear as governed by the steel, V_{sa} , in accordance with ACI 318-19 17.7.1.2 and the strength reduction factor, ϕ , in accordance with ACI 318-19 17.5.3 are given in <u>Tables 4</u>, <u>8</u>, <u>12</u>, and <u>15</u> of this report for the corresponding anchor steel.
- **4.1.6 Static Concrete Breakout Strength in Shear:** The nominal static concrete breakout strength of a single anchor or group of anchors in shear, V_{cb} or V_{cbg} , must be calculated in accordance with ACI 318-19 17.7.2 based on information given in <u>Tables 5</u>, <u>9</u>, <u>13</u>, and <u>16</u> in this report.

The basic concrete breakout strength of a single anchor in shear, V_b , must be calculated in accordance with ACI 318-19 17.7.2.2 using the values of d given in Tables 5, 9, 13, and 16 for the corresponding anchor steel in lieu of d_a . In addition, h_{ef} must be substituted for ℓ_e . In no case shall ℓ_e exceed 8d. The value of f_c shall be limited to a maximum of 8,000 psi (55 MPa) in accordance with ACI 318-19 17.3.1.

- **4.1.7** Static Concrete Pryout Strength in Shear: The nominal static pryout strength of a single anchor or group of anchors in shear, V_{cp} or V_{cpg} , shall be calculated in accordance with ACI 318-19 17.7.3.
- **4.1.8 Interaction of Tensile and Shear Forces:** For designs that include combined tension and shear, the interaction of tension and shear loads must be calculated in accordance with ACI 318-19 17.8.
- **4.1.9 Minimum Member Thickness** h_{min} , **Anchor Spacing** s_{min} , **Edge Distance** c_{min} : In lieu of ACI 318-19 17.9.2 values of s_{min} and s_{min} described in this report must be observed for anchor design and installation. The minimum member thicknesses, s_{min} , described in this report must be observed for anchor design and installation. For adhesive anchors that will remain untorqued, ACI 318-19 17.9.3.

For anchors that will be torqued during installation, the maximum torque, T_{max} , must be reduced for edge distances less than five anchor diameters (5d). T_{max} is subject to the edge distance, c_{min} , and anchor spacing, s_{min} , and shall comply with the following requirements:

	INSTALLATION TORQUE SU	JBJECT TO EDGE DISTANC	E		
NOMINAL ANCHOR SIZE, d	MINIMUM EDGE DISTANCE, Cmin	MINIMUM ANCHOR SPACING, Smin	MAXIMUM TORQUE, T _{max}		
⁵ / ₈ in. to 1 in. #5 to #8 M16 to M27 Ø14 to Ø 25 15M to 25M	1.75 in. (45 mm)	F-4	0 45 T		
1 ¹ / ₄ in. #9 to #10 M30 Ø28 to Ø 32 30M	2.75 in. (70 mm)	5 <i>d</i>	0.45·T _{max}		

For values of T_{max} , see Figure 4 of this report.

4.1.10 Critical Edge Distance c_{ac} and $\psi_{cp,Na}$: The modification factor, $\psi_{cp,Na}$, must be determined in accordance with ACI 318-19 17.6.5.5 except as noted below:

For all cases where c_{Na}/c_{ac} <1.0, $\psi_{cp,Na}$ determined from ACI 318-19 Eq. 17.6.5.5.1b, need not be taken less than c_{Na}/c_{ac} . For all other cases, $\psi_{cp,Na}$ shall be taken as 1.0.

The critical edge distance, c_{ac} must be calculated according to Eq. 17.6.5.5.1c of ACI 318-19, in lieu of ACI 318-19 17.9.5.

$$c_{ac} = h_{ef} \cdot \left(\frac{\tau_{k, uncr}}{1160}\right)^{0.4} \cdot \left[3.1 - 0.7 \frac{h}{h_{ef}}\right]$$

(Eq. 17.6.5.5.1c for ACI 318-19)

where

$$\left[\frac{h}{h_{\rm nf}}\right]$$
 need not be taken as larger than 2.4; and

 $\tau_{k,uncr}$ = the characteristic bond strength stated in the tables of this report whereby $\tau_{k,uncr}$ need not be taken as larger than:

$$au_{k,uncr} = rac{k_{uncr} \sqrt{h_{ef}f_c'}}{\pi \cdot d_a}$$
 Eq. (4-1)

4.1.11 Requirements for Seismic Design Categories C, D, E and F: In structures assigned to Seismic Design Category C, D, E or F under the IBC or IRC, anchors must be designed in accordance with ACI 318-19 17.10.

The nominal steel shear strength, V_{sa} , must be adjusted by $\alpha_{V,seis}$ as given in <u>Tables 4</u>, <u>8</u>, <u>12</u>, and <u>15</u> for the corresponding anchor steel. The nominal bond strength $\square_{\square\square cr}$ must be adjusted by $\alpha_{N,seis}$ as given in <u>Tables 6</u>, <u>7</u>, <u>10</u>, <u>14</u>, <u>17</u> and <u>18</u> for the corresponding anchor steel.

4.2 Strength Design of Post-Installed Reinforcing Bars:

- **4.2.1 General:** The design of straight post-installed deformed reinforcing bars must be determined in accordance with ACI 318 rules for cast-in-place reinforcing bar development and splices and this report.
- **4.2.2 Determination of bar development length** I_d : Values of I_d must be determined in accordance with the ACI 318 development and splice length requirements for straight cast-in-place reinforcing bars.

Exceptions:

- 1. For uncoated and zinc-coated (galvanized) post-installed reinforcing bars, the factor Ψ_e shall be taken as 1.0. For all other cases, the requirements in ACI 318-19 Table 25.4.2.5 shall apply.
- 2. When using alternate methods to calculate the development length (e.g. anchor theory), the applicable factors for post-installed anchors generally apply.



4.2.3 Minimum Member Thickness, h_{min} , **Minimum Concrete Cover**, $c_{c,min}$, **Minimum Concrete Edge Distance**, $c_{b,min}$, **Minimum Spacing**, $s_{b,min}$: For post-installed reinforcing bars, there is no limit on the minimum member thickness. In general, all requirements on concrete cover and spacing applicable to straight cast-in-bars designed in accordance with ACI 318 shall be maintained.

For post-installed reinforcing bars installed at embedment depths greater than 20d ($h_{ef} > 20d$), the minimum concrete cover shall be as follows:

REBAR SIZE	MINIMUM CONCRETE COVER, Cc,min
$d_b \le \text{No. 6}$ $(d_b \le 16\text{mm};$ $d_b \le 15\text{M})$	1- ³ / ₁₆ in. (30mm)
No. $6 < d_b \le No. 11$ (16mm $< d_b \le 36$ mm; $15M < d_b \le 35M$)	1- ⁹ / ₁₆ in. (40 mm)

The following requirements apply for minimum concrete edge and spacing for hef > 20d:

Required minimum edge distance for post-installed reinforcing bars (measured from the center of the bar):

$$C_{b,min} = d_o/2 + C_{c,min}$$

Required minimum center-to-center spacing between post-installed bars:

$$S_{b,min} = d_o + C_{c,min}$$

Required minimum center-to-center spacing from existing (parallel reinforcing):

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s_{b,min} = d_b/2 (existing reinforcing) + d_o/2 + c_{c,min}
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All other requirements applicable to straight cast-in place bars designed in accordance with ACI 318 shall be maintained.

- **4.2.4 Design Strength in Seismic Design Categories C, D, E and F:** In structures assigned to Seismic Category C, D, E or F under the IBC or IRC, design of straight post-installed reinforcing bars must consider the provisions of ACI 318-19 Chapter 18.
- **4.2.5 Design in Fire Resistive Construction Conditions:** For post-installed reinforcing bars, the relationship of bond stress to temperature under fire conditions suitable for use in determining conformance with fire resistance rating requirements is as given in <u>Figure 3</u>.

For temperatures above θ_{max} of 477°F (247°C), $\tau_{fire}(\theta) = 0$. The bond stress $\tau_{fire}(\theta)$, shall not exceed 1,090 psi (7.5 N/ mm²); Where θ is the temperature in the concrete at the post-installed reinforcing bar in °F (for psi) or °C (for N/mm²), as applicable.

Determination of the temperature in the concrete at the location of the post-installed reinforcing bar is dependent on the geometry of the concrete members under consideration and its calculation is the responsibility of the design professional. The design professional shall use the bond strength / temperature curves in Figure 4 along with a determination of the temperature in the concrete appropriate for the member geometry under consideration to calculate the reinforcing bar development length I_d .

4.3 Allowable Stress Design (ASD):

4.3.1 General: For anchors designed using load combinations in accordance with Section 1605.1 of the 2024 IBC (Allowable Stress Design), allowable loads shall be established using Eq. (4-2) or Eq. (4-3):

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T_{allowable,ASD}=\phi N_n/\alpha Eq. (4-2) and V_{allowable,ASD}=\phi V_n/\alpha Eq. (4-3) where:
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 ϕN_n

 $T_{allowable,ASD}$ = Allowable tension load (lbf or kN)

 $V_{allowable,ASD}$ = Allowable shear load (lbf or kN)

= The lowest design strength of an anchor or anchor group in tension as determined in accordance with ACI 318-19 Chapter 17, 2024 IBC Section 1905.7, and Section 4.1 of this report, as applicable.

ϕV_n	=	The lowest design strength of an anchor or anchor group in shear as determined in
		accordance with ACI 318-19 Chapter 17, 2024 IBC Section 1905.7, and Section 4.1 of this
		report, as applicable.

 Conversion factor calculated as a weighted average of the load factors for the controlling load combination. In addition, α must include all applicable factors to account for non-ductile failure modes and required over-strength.

The requirements for member thickness, edge distance and spacing, described in <u>Table 1</u> of this report, must apply.

4.3.2 Interaction of Tensile and Shear Forces: In lieu of ACI 318-19 17.8.2 and 17.8.3, interaction of tension and shear loads must be calculated as follows:

If $T_{applied} \leq 0.2 \ T_{allowable,ASD}$, then the full allowable strength in shear, $V_{allowable,ASD}$, shall be permitted.

If $V_{applied} \leq 0.2 \ V_{allowable,ASD}$, then the full allowable strength in tension, $T_{allowable,ASD}$, must be permitted.

For all other cases:

$$\frac{T_{applied}}{T_{allowable, ASD}} + \frac{V_{applied}}{V_{allowable, ASD}} \le 1.2 \qquad \text{Eq. (4-4)}$$

4.4 Installation:

α

Installation parameters are illustrated in <u>Figures 2</u> and <u>4</u> and <u>Tables 5</u>, <u>9</u>, <u>13</u>, and <u>16</u> of this report. Installation must be in accordance with ACI 318-19 26.7.2. Anchor locations must comply with this report and the plans and specifications approved by the code official. Installation of the DEWALT Pure220+ Adhesive Anchor System must conform to the manufacturer's printed installation instructions included in each unit package as described in <u>Figure 3</u> of this report.

The adhesive anchor system may be installed in downwards, horizontally and upwardly inclined orientation applications (e.g. overhead). If the bottom or back of the drilled hole is not reached with the mixing nozzle, a mixer extension tube, supplied by DEWALT must be attached to the mixing nozzle as described in Figure 4 of this report. Additionally, for upwardly inclined or between horizontal and upwardly inclined orientation applications of all drilled hole depths, and downward and horizontal applications with a drilled depth of more than 10 inch (250 mm) are to be installed using piston plugs for the $^5/_8$ -inch and M16 through $^{11}/_4$ -inch and M30 diameter threaded steel rods, and No. 5, Ø14, and 15M through No. 10, Ø32 and 30M, steel reinforcing bars, installed in the specified hole diameter, and attached to the mixing nozzle and extension tube supplied by DEWALT as described in Figure 4 in this report. For installation with the $^3/_8$ -inch, $^1/_2$ -inch, M10 and M12 diameter threaded steel rods, and No. 3, No. 4, Ø10, Ø12 and 10M steel reinforcing bars only, a piston plug is not required.

Installation of anchors in horizontal or upwardly inclined orientations shall be fully restrained from movement throughout the specified curing period using temporary wedges, external supports, or other methods. Where temporary restraint devices are used, their use shall not result in impairment of the anchor shear resistance.

4.5 Special Inspection:

Periodic special inspection must be performed where required in accordance with Section 1705.1.1 and Table 1705.3 of the 2024 IBC and this report. The special inspector must be on the jobsite initially during anchor installation to verify the anchor type, adhesive expiration date, anchor dimensions, concrete type, concrete compressive strength, hole dimensions, hole cleaning procedures, anchor spacing, edge distances, concrete thickness, anchor embedment, tightening torque, and adherence to the manufacturer's printed installation instructions.

The special inspector must verify the initial installations of each type and size of adhesive anchor by construction personnel on site. Subsequent installations of the same anchor type and size by the same construction personnel are permitted to be performed in the absence of the special inspector. Any change in the anchor product being installed or the personnel performing the installation requires an initial inspection. For ongoing installations over an extended period, the special inspector must make regular inspections to confirm correct handling and installation of the product.

Continuous special inspection of adhesive anchors installed in horizontal or upwardly inclined orientations to resist sustained tension loads must be performed in accordance with ACI 318-19 26.13.3.2(e).

Under the IBC, additional requirements as set forth in Sections 1705, 1706 or 1707 must be observed, where applicable.

5.0 CONDITIONS OF USE:

The DEWALT Pure220+ Adhesive Anchor and Post Installed Reinforcing Bar Connection System described in this report complies with, or is a suitable alternative to what is specified in, those codes listed in Section 1.0 of this report, subject to the following conditions:

- **5.1** DEWALT Pure220+ adhesive anchors and post-installed reinforcing bars must be installed in accordance with the manufacturer's printed installation instructions included with each cartridge and provided in Figure 4 of this report.
 - Anchors [3/8-, 1/2-, 5/8-, 3/4-, 7/8-, 1-, and 1-1/4-inch fractional diameter and M10, M12, M16, M20, M24, M27 and M30 metric diameter threaded steel rods, and No. 3 through No. 10 fractional size, \emptyset 10, \emptyset 12, \emptyset 14, \emptyset 16, \emptyset 20, \emptyset 25, \emptyset 28 and \emptyset 32 EU metric, and 10M, 15M, 20M, 25M, and 30M Canadian steel reinforcing bars] described in this report must be installed in cracked and uncracked normal-weight concrete having a specified compressive strength f_c = 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).
- 5.2 Post-installed reinforcing bars with diameters No. 3 through No. 11 fractional size and Ø10, Ø12, Ø14, Ø16, Ø20, Ø25, Ø28, Ø32 and Ø36 EU metric, and 10M, 15M, 20M, 25M, and 30M Canadian size steel reinforcing bars in hammer-drilled (or DEWALT hollow drill bit system) and diamond core holes are used in cracked and uncracked normal-weight concrete only, to resist static, wind or earthquake (IBC Seismic Design Categories A through F) tension and shear loads. Use is limited to normal-weight concrete with a specified compressive strength, f'c = 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa)
- **5.3** The values of f'_c used for calculation purposes must not exceed 8,000 psi (55 MPa).
- **5.4** Anchors and post-installed reinforcing bars must be installed in concrete base materials in holes predrilled in accordance with the instructions provided in Figure 4 of this report.
- 5.5 Loads applied to the anchors must be adjusted in accordance with Section 1605.1 of the 2024 IBC for strength design or for allowable stress design.
- **5.6** In structures assigned to Seismic Design Categories C, D, E, and F under the IBC or IRC, anchor strength must be adjusted in accordance with Section 4.1.11 of this report.
- 5.7 DEWALT Pure220+ adhesive anchors are permitted to be installed in concrete that is cracked or that may be expected to crack during the service life of the anchor, subject to the conditions of this report.
- 5.8 Strength design values are established in accordance with Section 4.1 of this report.
- **5.9** Minimum anchor spacing and edge distance as well as minimum member thickness must comply with the values described in this report.
- **5.10** Prior to anchor installation, calculations and details demonstrating compliance with this report must be submitted to the code official. The calculations and details must be prepared by a registered design professional where required by the statutes of the jurisdiction in which the project is to be constructed.
- 5.11 Anchors are not permitted to support fire-resistive construction. Where not otherwise prohibited by the code, DEWALT Pure220+ adhesive anchors are permitted for installation in fire-resistive construction provided that at least one of the following conditions is fulfilled:
 - Anchors are used to resist wind or seismic forces only.
 - Anchors that support gravity load—bearing structural elements are within a fire-resistive envelope or a
 fire-resistive membrane, are protected by approved fire-resistive materials, or have been evaluated for
 resistance to fire exposure in accordance with recognized standards.
 - Anchors are used to support nonstructural elements.
 - Post-installed reinforcing bars designed in accordance with Section 4.2.5 of this report.
- **5.12** Since an ICC-ES acceptance criteria for evaluating data to determine the performance of adhesive anchors subjected to fatigue or shock loading is unavailable at this time, the use of these anchors under such conditions is beyond the scope of this report.
- 5.13 Use of zinc-plated carbon steel threaded rods or steel reinforcing bars is limited to dry, interior locations.
- **5.14** Use of hot-dipped galvanized carbon steel and stainless-steel rods is permitted for exterior exposure or damp environments.
- 5.15 Steel anchoring materials in contact with preservative-treated and fire-retardant-treated wood shall be of zinc-coated steel or stainless steel. The minimum coating weights for zinc-coated steel shall be in accordance with ASTM A153.

- **5.16** Periodic special inspection must be provided in accordance with Section 4.3 in this report. Continuous special inspection for anchors installed in horizontal or upwardly inclined orientations to resist sustained tension loads must be provided in accordance with Section 4.3 of this report.
- **5.17** Installation of anchors and post-installed reinforcing bars in horizontal or upwardly inclined orientations to resist sustained tension loads must be performed by personnel certified by an applicable certification program in accordance with ACI 318-19 26.7.2(e).
- 5.18 DEWALT Pure220+ adhesive anchors and post-installed reinforcing bars may be used to resist tension and shear forces in floor, wall for overhead installations into concrete with a temperature between 41°F and 104°F (5°C and 40°C) for threaded rods and reinforcing bars.
- 5.19 DEWALT Pure220+ adhesive is manufactured under a quality control program with inspections by ICC-ES.

6.0 EVIDENCE SUBMITTED

6.1 Data in accordance with the ICC-ES Acceptance Criteria for Post-installed Adhesive Anchors and Reinforcing Bar Connections in Concrete (AC308) (24), published April 2025, which incorporates requirements in ACI 355.4-19 for use in cracked and uncracked concrete.

7.0 IDENTIFICATION

- 7.1 The ICC-ES mark of conformity, electronic labelling, or the evaluation report number (ICC-ES ESR-5144) along with the name, registered trademark, or registered logo of the report holder must be included in the product label.
- 7.2 In addition, DEWALT Pure220+ adhesive is identified by packaging labelled with the manufacturer's name (DEWALT) and address, anchor name, the lot number, the expiration date, and the evaluation report number (ESR-5144). Threaded rods, nuts, washers, and deformed reinforcing bars are standard steel anchor elements and must conform to applicable national or international specifications as set forth in Tables 2 and 3 of this report.
- **7.3** The report holder's contact information is the following:

DEWALT
701 EAST JOPPA ROAD
TOWSON, MARYLAND 21286
(800) 524-3244
www.DEWALT.com
anchors@DEWALT.com

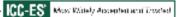


TABLE 1—DESIGN TABLE INDEX

DESIGN	STRENGTH1 - THREADED RODS	Fractional	Metric		
T-4	Steel Strength - N_{sa} , V_{sa}	Table 4	Table 12		
-	Concrete Strength - N_{pn} , N_{sb} , N_{sbg} , N_{cb} , N_{cbg} , V_{cb} , V_{cbg} , V_{cp} , V_{cpg}	Table 5	Tabl	<u>e 13</u>	
	Bond Strength ² - N _a , N _{ag}	Table 6 and Table 7	Table 14		
DESIGN S	STRENGTH1 - REINFORCING STEEL	Fractional	Metric	Canadian	
	Steel Strength - N _{sa} , V _{sa}	Table 8	Table 15	Table 15	
***************************************	Concrete Strength - N_{pn} , N_{sb} , N_{sbg} , N_{cb} , N_{cbg} , V_{cb} , V_{cbg} , V_{cp} , V_{cpg}	Table 9	Table 16	Table 16	
HILLIGHTEREFERE	Bond Strength ² - N _a , N _{ag}	Table 10 and Table 11	Table 17	Table 18	
	Determination of development lengths and non-contact lap splices for post-installed reinforcing bar connections ³	Table 19	Table 20	Table 21	

¹Ref. ACI 318-19 17.5.2.

TABLE 2—SPECIFICATIONS AND PHYSICAL PROPERTIES OF COMMON CARBON AND STAINLESS STEEL THREADED ROD MATERIALS¹

	THREADED ROD SPECIFICATION	UNITS	MINIMUM SPECIFIED ULTIMATE STRENGTH, futa	MIN. SPECIFIED YIELD STRENGTH 0.2 PERCENT OFFSET, fya	f _{uta} /f _{ya}	ELONGATION, MIN. PERCENT ¹¹	REDUCTION OF AREA, MIN. PERCENT	SPECIFICATION FOR NUTS ¹²	
	ASTM A193 ² Grade B7	psi (MPa)	125,000 (862)	105,000 (724)	1.19	16	50	ASTM A194 / A563 Grade D	
	ASTM A36 ³ / F1554 ⁴ , Grade 36	psi (MPa)	58,000 (400)	36,000 (250)	1.61	23	40	ASTM A194 / A563	
	ASTM F1554 ⁴ Grade 55	psi (MPa)	75,000 (517)	55,000 (380)	1.36	23	40	Grade A	
STEEL	ASTM F1554 ⁴ Grade 105	psi (MPa)	125,000 (860)	105,000 (724)	1.19	15	45		
TS NC	ASTM A449 ⁵ ³ / ₈ to 1 in.	psi (MPa)	120,000 (830)	92,000 (635)	1.30	14	35	ASTM A194 / A563 Grade DH	
CARBON	ASTM A449 ⁵ 1 ¹ / ₄ in	psi (MPa)	105,000 (720)	81,000 (560)	1.30	14	35		
	ASTM F568M ⁶ Class 5.8 (equivalent to ISO 898-1)	psi (MPa)	72,500 (500)	58,000 (400)	1.25	10	35	ASTM A563 Grade DH DIN 934 (8-A2K) ¹³	
	ISO 898-1 ⁷ Class 5.8	MPa (psi)	500 (72,500)	400 (58,000)	1.25	22	-	EN ISO 4032 Grade 6	
	ISO 898-1 ⁷ Class 8.8	MPa (psi)	800 (116,000)	640 (92,800)	1.25	12	52	EN ISO 4032 Grade 8	
	ASTM F593 ⁸ CW1 ³ / ₈ to ⁵ / ₈ in.	psi (MPa)	100,000 (690)	65,000 (450)	1.54	20	-	ASTM F594 Alloy	
STEEL	ASTM F593 ⁸ CW2 3/ ₄ to 1 ¹ / ₄ in.	psi (MPa)	85,000 (590)	45,000 (310)	1.89	25	-	Group 1, 2 or 3	
STAINLESS S	ASTM A193/A193M ⁹ Grade B8/B8M2, Class 2B	psi (MPa)	95,000 (655)	75,000 (515)	1.27	25	40	ASTM A194/A194M	
STAII	ISO 3506-1 ¹⁰ A4-70 (M8-M24)	MPa (psi)	700 (101,500)	450 (65,250)	1.56	40	-	EN ISO 4032	
	ISO 3506-1 ¹⁰ A4-50 (M27-M30)	MPa (psi)	500 (72,500)	210 (30,450)	2.38	40	-	EN ISO 4032	

Adhesive must be used with continuously threaded carbon or stainless steel rod (all-thread) having thread characteristics complying with ANSI B1.1 UNC Coarse Thread Series.

²See Section 4.1 of this evaluation report.

³For design of post-installed reinforcing bars in fire resistive construction conditions, see Section 4.2.5 and Figure 3 of this evaluation report.

²Standard Specification for Alloy-Steel and Stainless steel Bolting Materials for High temperature of High Pressure service and Other Special Purpose Applications.

³Standard Specification for Carbon Structural steel

^{**}Standard Specification for Anchor Bolts, Steel 36, 55 and 105-ksi Yield Strength.

**Standard Specification for Anchor Bolts, Steel 36, 55 and 105-ksi Yield Strength.

**Standard Specification for Hex Cap Screws, Bolts and Studs, Heat Treated, 120/105/50 ksi Minimum Tensile Strength, General Use.

**Standard Specification for Carbon and Alloy Steel external Threaded Metric Fasteners.

⁷Mechanical properties of fasteners made of carbon steel and alloy steel - Part 1: Bolts, Screws and Studs.

⁸Standard Specification for Alloy-Steel and Stainless Steel Bolting for High Temperature or High Pressure Service and Other Special Purpose Applications.

⁹Standard Specification for Stainless Steel Bolts, Hex Cap Screws, and Studs.

¹⁰Mechanical properties of corrosion-resistant stainless steel fasteners - Part 1: Bolts, Screws and Studs.

¹¹Based on 2-in. (50 mm) gauge length except for ASTM A193, which is based on a gauge length of 4d.

¹²Nuts and washers of other grades and style having specified proof load stress greater than the specified grade and style are also suitable. Nuts must have specified proof load stresses equal to or greater than the minimum tensile strength of the specified threaded.

TABLE 3—SPECIFICATIONS AND PHYSICAL PROPERTIES OF COMMON CARBON REINFORCING BARS

REINFORCING SPECIFICATION	UNITS	MINIMUM SPECIFIED ULTIMATE STRENGTH, f _{uta}	MINIMUM SPECIFIED YIELD STRENGTH, fya
ASTM A615 ¹ , A767 ³	psi	100,000	75,000
Grade 75	(MPa)	(690)	(520)
ASTM A615 ¹ , A767 ³ , A996 ⁴	psi	80,000	60,000
Grade 60	(MPa)	(620)	(414)
ASTM A706 ² , A757 ³	psi	80,000	60,000
Grade 60	(MPa)	(550)	(414)
ASTM A615 ¹	psi	60,000	40,000
Grade 40	(MPa)	(415)	(275)
DIN 488 ⁵ BSt 500	MPa	550	500
	(psi)	(80,000)	(72,500)
CAN/CSA-G30.18 ⁶ Gr. 400	MPa	540	400
	(psi)	(78,300)	(58,000)

¹Standard Specification for Deformed and Plain Carbon-Steel Bars for Concrete Reinforcement.

⁶Billet-Steel Bars for Concrete Reinforcement



FIGURE 1— EXAMPLES OF DEWALT DUST REMOVAL DRILLING SYSTEMS WITH HEPA DUST EXTRACTORS FOR ILLUSTRATION

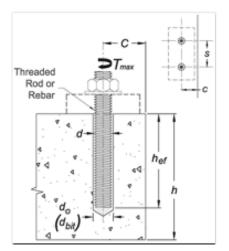








FIGURE 2— PURE220+ ADHESIVE ANCHOR SYSTEM INCLUDING TYPICAL STEEL ANCHOR ELEMENTS AND BASIC INSTALLATION PARAMETERS

²Standard Specification for Low-Alloy Steel Deformed and Plain Bars for Concrete Reinforcement.

³Standard specification for Zinc-Coated (Galvanized) steel Bars for Concrete Reinforcement.

⁴Standard specification for Rail-Steel and Axle-steel Deformed bars for Concrete Reinforcement.

⁵Reinforcing steel, reinforcing steel bars; dimensions and masses.

ICC-ES* Most Widely Assented and Trasted

TABLE 4—STEEL DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT THREADED ROD1

	DESIGN INFORMATION	Symbol	Units			Nominal	Rod Diamet	er (inch)					
	DESIGN INFORMATION	Syllibol		3/8	1/2	5/8	3/4	7/8	1	1 ¹ / ₄			
Threaded r	od O.D.	da	in. (mm)	0.375 (9.5)	0.500 (12.7)	0.625 (15.9)	0.750 (19.1)	0.875 (22.2)	1.000 (25.4)	1.250 (31.8)			
Threaded r	od effective cross-sectional area	Ase	in.² (mm²)	0.0775 (50)	0.1419 (92)	0.2260 (146)	0.3345 (216)	0.4617 (298)	0.6057 (391)	0.9691 (625)			
	Naminal attenuate as assumed by steel	N _{sa}	lb (kN)	4,495 (20.0)	8,230 (36.6)	13,110 (58.3)	19,400 (86.3)	26,780 (119.1)	35,130 (156.3)	56,210 (250.0)			
1554	Nominal strength as governed by steel strength (for a single anchor)	V _{sa}	Ìb	2,695	4,940	7,860	11,640	16,070	21,080	33,725			
36/F de 3(Reduction factor for seismic shear	α _{V,seis}	(kN)	(12.0)	(22.0)	(35.0)	(51.8) 0.70	(71.4)	(93.8)	(150.0)			
ASTM A36/F1554, Grade 36	Strength reduction factor for tension ²	φ	_				0.75						
AS	Strength reduction factor for shear ²	φ	_				0.65						
	Citerigit reduction factor for shear	,	lb	5,815	10,645	16,950	25,090	34,630	45,430	72,685			
4	Nominal strength as governed by steel strength (for a single anchor)	N _{sa}	(kN)	(25.9) 3,490	(47.6) 6,385	(75.5) 10,170	(111.7) 15,055	(154.1) 20,780	(202.1) 27,260	(323.1) 43,610			
ASTM F1554 Grade 55	energin (for a emgle another)	V _{sa}	(kN)	(15.5)	(28.6)	(45.3)	(67)	(92.5)	(121.3)	(193.9)			
TM F	Reduction factor for seismic shear	α <i>v,seis</i>	-				0.70						
AS	Strength reduction factor for tension ²	φ	-				0.75						
	Strength reduction factor for shear ²	φ	-				0.65						
	Nominal strength as governed by steel	N _{sa}	lb (kN)	9,685 (43.1)	17,735 (78.9)	28,250 (125.7)	41,810 (186.0)	57,710 (256.7)	75,710 (336.8)	121,135 (538.8)			
193 37 554 05	strength (for a single anchor)	V _{sa}	lb (kN)	5,810 (25.9)	10,640 (47.3)	16,950 (75.4)	25,085 (111.6)	34,625 (154.0)	45,425 (202.1)	72,680 (323.3)			
M A A A A A A A A A A A A A A A A A A A	Reduction factor for seismic shear	α <i>v,seis</i>	-	(2010)	(17.0)	(101.)	0.70	(10110)	(===::)	(020.0)			
ASTM A193 Grade B7 ASTM F1554 Grade 105	Strength reduction factor for tension ²		-	0.75									
	Strength reduction factor for shear ²	φ	-	0.65									
	Nominal strength as governed by steel strength (for a single anchor)	N _{sa}	lb (kN)	9,300	17,030	27,120 (120.9)	40,140	55,405	72,685	101,755			
6		V _{sa}	Ìb	(41.4) 5,580	(76.2) 10,220	16,270	(178.8) 24,085	(246.7) 33,240	(323.7) 43,610	(450.0) 61,055			
ASTM A449	Reduction factor for seismic shear		(kN)	(24.8) (45.7) (72.5) (107.3) (148) (194.2) (270.0) 0.70									
ASTA	Strength reduction factor for tension ²	α _{V,seis}	_				0.75						
	Strength reduction factor for shear ²	φ	-				0.75						
	Strength reduction factor for shear-	φ	- Ib	5,620	10,290	16,385	24,250	33,470	43,910	70,260			
5	Nominal strength as governed by steel strength (for a single anchor)	N _{sa}	(kN)	(25) 3,370	(46) 6,175	(73) 9,830	(108) 14,550	(149)	(195.5) 26,350	(312.5) 42,155			
568N 5.8	Strength (for a single anchor)	V _{sa}	(kN)	(15)	(27.6)	(43.8)	(64.8)	(89.4)	(117.3)	(187.5)			
ASTM F568M Class 5.8	Reduction factor for seismic shear	α _{V,seis}	-				0.70						
AS.	Strength reduction factor for tension ²	φ	-				0.65						
	Strength reduction factor for shear ²	ϕ	-				0.60						
_	Nominal strength as governed by steel	N _{sa}	lb (kN)	7,750 (34.5)	14,190 (63.1)	22,600 (100.5)	28,430 (126.5)	39,245 (174.6)	51,485 (229.0)	82,370 (366.4)			
3 CV	strength (for a single anchor)	V _{sa}	lb (kN)	4,650 (20.7)	8,515 (37.9)	13,560 (60.3)	17,060 (75.9)	23,545 (104.7)	30,890 (137.4)	49,425 (219.8)			
ASTM F593 CW Stainless	Reduction factor for seismic shear	α <i>v</i> ,seis	-	(2011)	(07.0)	(00.0)	0.70	(10)	(10711)	(2:0:0)			
STM	Strength reduction factor for tension ²	φ	-				0.65						
⋖	Strength reduction factor for shear ²	φ	-				0.60						
L SSI		N _{sa}	lb ((A))	7,365	13,480	21,470	31,780	43,860	57,540	92,065			
., Cla	Nominal strength as governed by steel strength (for a single anchor)	V _{sa}	(kN) lb	(32.8) 4,420	(60.3) 8,090	(95.6) 12,880	(141.5) 19,070	(195.2) 26,320	(256.1) 34,525	(409.4) 55,240			
93/A 38M2 1B	Reduction factor for calamia about		(kN) -	(19.7)	(36.2)	(57.4)	(84.9)	(117.1)	(153.7)	(245.6)			
ASTM A193/A193M Grade B8/B8M2, Class 2B	Reduction factor for seismic shear	α _{V,seis}	-				0.70						
AST) rade	Strength reduction factor for tension ²	φ	-				0.75						
` ਯੁੱ	Strength reduction factor for shear ²	φ	-				0.65						

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006894 MPa. For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

¹Values provided for common rod material types based on specified strengths and calculated in accordance with ACI 318-19 Eq. 17.6.1.2 and Eq. 17.7.1.2b. Nuts and washers must comply with requirements for the rod.
²The tabulated value of *ϕ* applies when the load combinations of Section 1605.1 of the 2024 IBC or ACI 318-19, as set forth in ACI 318-19 17.5.3 are used.

TABLE 5—CONCRETE BREAKOUT DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT THREADED ROD1

DECICAL INFORMATION	0	11	Nominal Rod Diameter (inch)										
DESIGN INFORMATION	Symbol	Units	3/8	1/2	5/8	3/4	7/8	1	1 ¹ / ₄				
Effectiveness factor for cracked concrete	k _{c,cr}	in-lb (SI)				17 (7)							
Effectiveness factor for uncracked concrete	$k_{c,uncr}$	in-lb (SI)				24 (10)							
Min. anchor spacing	Smin	in. (mm)	1 ⁷ / ₈ (48)	2 ³ / ₈ (60)	3 (76)	3 ³ / ₄ (95)	4 ¹ / ₄ (108)	4 ³ / ₄ (121)	5 ⁷ / ₈ (149)				
Min. edge distance	Cmin	in.	1 ⁵ / ₈	1 ³ / ₄	2 (51)	2 ³ / ₈ (60)	2 ¹ / ₂ (64)	2 ³ / ₄ (70)	3 ¹ / ₄ (82)				
	Onmi	(mm)	(41)	(44)	See Section 4.1.9 of this report for smaller edge distance with 0.45								
Min. member thickness	h _{min}	in. (mm)		+ 1 ¹ / ₄ _f + 30)		h _{ef} + 2d ₀ w	here d₀ is hole d	iameter					
Critical edge distance - splitting (for uncracked concrete) ²	C _{ac}	-			See Sec	tion 4.1.10 of thi	s report.						
Critical anchor spacing – splitting	Sac	-				2-c _{ac}							
Strength reduction factor for tension, concrete failure modes ²	φ	-		0.65									
Strength reduction factor for shear, concrete failure modes ²	ϕ	1		·	·	0.70	·	·					

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006894 MPa.For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

TABLE 6—BOND STRENGTH DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT THREADED ROD IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR DEWALT HOLLOW CARBIDE DRILL BIT)¹

			1	1							
	DESIGN INFO	DMATION	Cumhal	Units	Nominal Rod Diameter (inch)						
	DESIGN INFO	RIVIATION	Symbol	Units	3/8	1/2	5/8	3/4	7/8	1	1 ¹ / ₄
	Minimum em	pedment	h _{ef,min}	in.	2 ³ / ₈	23/4	31/8	31/2	31/2	4	5
				(mm)	(60.3)	(69.9)	(79.4)	(88.9)	(88.9)	(101.6)	(127.0)
	Maximum em	bedment	h _{ef,max}	in. (mm)	7 ¹ / ₂ (191)	10 (254)	12 ¹ / ₂ (318)	15 (381)	17 ¹ / ₂ (445)	20 (508)	25 (635)
	Character	istic bond strength in		psi	2,200	2,135	2.075	2,010	1,950	1,885	1,760
Temperature		acked concrete	$\tau_{k,uncr}$	(N/mm²)	(15.1)	(14.7)	(14.3)	(13.8)	(13.4)	(13.0)	(12.1)
range A ^{2,3}		istic bond strength in		psi	1.525	1,535	1,375	1.555	1,530	1.495	1.445
		cked concrete	$\tau_{k,cr}$	(N/mm ²)	(10.5)	(10.6)	(9.4)	(10.7)	(10.5)	(10.3)	(9.9)
		stic bond strength in	T.	psi	1,720	1,675	1,625	1,575	1,525	1,480	1,380
Temperature		acked concrete	$\tau_{k,uncr}$	(N/mm ²)	(11.8)	(11.5)	(11.2)	(10.8)	(10.5)	(10.1)	(9.5)
range B ^{2,3}	Character	Tk.cr	psi	1,195	1,205	1,080	1,215	1,200	1,170	1,135	
	crae	VN,01	(N/mm²)	(8.2)	(8.3)	(7.4)	(8.3)	(8.2)	(8.0)	(7.8)	
T	Characteri uncr	Tk,uncr	psi (N/mm²)	970 (6.7)	940	915 (6.3)	885 (6.1)	855 (5.9)	825	770 (F. 2)	
Temperature range C ^{2,3}			(N/mm²) psi	665	(6.5) 680	610	680	665	(5.7) 665	(5.3) 640	
range o		Characteristic bond strength in cracked concrete			(4.6)	(4.7)	(4.2)	(4.7)	(4.6)	(4.6)	(4.4)
		Anchor Category	-	(N/mm²) -		. , ,	. ,	1			. ,
	Dry concrete	Strength reduction factor	фа	-	0.65						
	Water-saturated	Anchor Category	-	-				2			
Permissible	concrete	Strength reduction factor	φws	-				0.55			
installation		Anchor Category	-	-				3			
conditions	Water-filled hole	Strength reduction factor	ϕ_{wt}	-				0.45			
	(flooded)	Modification factor for Water-filled holes	Kwt	-				0.85			
	Underwater	Anchor Category	-	-				2			
	(submerged)	Strength reduction factor	$\phi_{\sf UW}$	-	0.55						
Re	duction factor for	seismic tension	∝N,seis	-	1.00	1.00	0.90	1.00	0.95	1.00	1.00

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006894 MPa. For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

¹Bond strength values correspond to concrete compressive strength f_c = 2,500 psi (17.2 N/mm²).. For concrete compressive strength, f_c between 2,500 psi (17.2 N/mm²) and 8,000 psi (55.2 N/mm²), the tabulated characteristic bond strength may be increased by a factor of $(f_c/2500)^{0.21}$ [For SI: $(f_c/17.2)^{0.21}$] for uncracked concrete, and $(f_c/2500)^{0.14}$ [For SI: $(f_c/17.2)^{0.14}$] for cracked concrete. See Section 4.1.4 of this report.

²Temperature range A: Maximum short term temperature = 140°F (60°C), maximum long term temperature = 110°F (43°C); Temperature range B: Maximum short

²Temperature range A: Maximum short term temperature = 140°F (60°C), maximum long term temperature = 110°F (43°C); Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 110°F (43°C); Temperature range C: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 140°F (60°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

¹Additional setting information is described in Figure 4, installation instructions.

² The strength reduction factor applies when the load combinations from the IBC or ACI 318 are used and the requirements of ACI 318-19 17.5.3 are met.

³Characteristic bond strengths are for sustained loads including dead and live loads. For load combinations consisting of short-term loads only such as wind or seismic, bond strengths may be increased by 17 percent for temperature range A and B and by 92 percent for temperature range C.

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TABLE 7—BOND STRENGTH DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT THREADED ROD IN HOLES DRILLED WITH A DIAMOND CORE BIT¹

							Nominal	Rod Diame	ter (inch)		
	DESIGN INFO	RMATION	Symbol	Units	3/8	1/2	5/8	3/4	7/8	1	1 ¹ / ₄
	Minimum embedment				2 ³ / ₈ (60.3)	2 ³ / ₄ (69.9)	3 ¹ / ₈ (79.4)	3 ¹ / ₂ (88.9)	3 ¹ / ₂ (88.9)	4 (101.6)	5 (127.0)
	Maximum embedment			in. (mm)	7 ¹ / ₂ (191)	10 (254)	12 ¹ / ₂ (318)	15 (381)	17 ¹ / ₂ (445)	20 (508)	25 (635)
Temperature		istic bond strength in acked concrete	$ au_{k,uncr}$	psi (N/mm²)	1655 (11.4)	1550 (10.7)	1495 (10.3)	1435 (9.9)	1390 (9.6)	1350 (9.3)	1290 (8.9)
range A ^{2,3}	Characteri crad	Tk,cr	psi (N/mm²)	1205 (8.3)	1116 (7.7)	1045 (7.2)	1000 (6.9)	970 (6.7)	945 (6.5)	945 (6.5)	
Temperature	Characteri uncr	$ au_{k,uncr}$	psi (N/mm²)	1350 (9.3)	1275 (8.8)	1220 (8.4)	1160 (8.0)	1130 (7.8)	1100 (7.6)	1045 (7.2)	
range B ^{2,3}	Characteri crad	Tk,cr	psi (N/mm²)	970 (6.7)	915 (6.3)	855 (5.9)	810 (5.6)	800 (5.5)	770 (5.3)	770 (5.3)	
Temperature		istic bond strength in acked concrete	$ au_{k,uncr}$	psi (N/mm²)	970 (6.7)	915 (6.3)	885 (6.1)	840 (5.8)	810 (5.6)	800 (5.5)	755 (5.2)
range C ^{2,3}	Characteristic bond strength in cracked concrete		Tk,cr	psi (N/mm²)	650 (4.5)	610 (4.2)	580 (4.0)	550 (3.8)	535 (3.7)	520 (3.6)	520 (3.6)
	Dry concrete	Anchor Category	-	-				1			
Permissible installation	Dry concrete	Strength reduction factor	ϕ_{d}	-		•		0.65	•		
conditions	Water-saturated	Anchor Category	-	-	1	2	2	2	3	3	3
	concrete	Strength reduction factor	φws	-	0.65	0.55	0.55	0.55	0.45	0.45	0.45
Re	duction factor for	seismic tension	QN,seis	-	1.00	1.00	1.00	0.98	0.99	0.98	1.00

For **SI:** 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006894 MPa.

For **pound-inch** units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

 $^{^1}$ Bond strength values correspond to concrete compressive strength f_c = 2,500 psi (17.2 N/mm²). For concrete compressive strength, f_c between 2,500 (17.2 N/mm²) psi and 8,000 psi (55.2 N/mm²), the tabulated characteristic bond strength may be increased by a factor of $(f_c/2500)^{0.24}$ [For SI: $(f_c/17.2)^{0.24}$] for uncracked concrete, and $(f_c/2500)^{0.20}$ [For SI: $(f_c/17.2)^{0.20}$] for cracked concrete. See Section 4.1.4 of this report. 2 Temperature range A: Maximum short term temperature = 140°F (60°C), maximum long term temperature = 110°F (43°C); Temperature range B: Maximum short

²Temperature range A: Maximum short term temperature = 140°F (60°C), maximum long term temperature = 110°F (43°C); Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 110°F (43°C); Temperature range C: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 140°F (60°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

³Characteristic bond strengths are for sustained loads including dead and live loads. For load combinations consisting of short-term loads only such as wind or seismic, bond strengths may be increased by 20 percent for temperature range A and B and by 61 percent for temperature range C.

TABLE 8—STEEL DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT REINFORCING BARS1

_	ECICN INFORMATION	Cumbal	Unita				Nomina	I Bar Size							
ט	for shear ² Nominal strength as governed by steel streng (for a single anchor) Reduction factor for seismic shear Strength reduction factor for tension ² Strength reduction factor for shear ² Nominal strength as	Symbol	Units	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 9	No. 10				
Reinfo	orcing bar O.D.	da	in.	0.375	0.500	0.625	0.750	0.875	1.000	1.128	1.270				
	9	- Ca	(mm)	(9.5)	(12.7)	(15.9)	(19.1)	(22.2)	(25.4)	(28.6)	(31.8)				
		Ase	in.² (mm²)	0.110 (71)	0.200 (129)	0.310 (200)	0.440 (284)	0.600 (387)	0.790 (510)	1.000 (645)	1.270 (819)				
	1		(IIIIII-)	11,000	20,000	31,000	44,000	60,000	79,000	100,000	127,000				
_	Nominal strength as	N _{sa}	(kN)	(48.9)	(89.0)	(137.9)	(195.7)	(266.9)	(351.4)	(444.8)	(564.9)				
.92		V _{sa}	Ìb	6,600	12,000	18,600	26,400	36,000	47,400	60,000	76,200				
, A 75	(for a single anchor)	V _{sa}	(kN)	(29.4)	(53.4)	(82.7)	(117.4)	(160.1)	(210.8)	(266.9)	(338.9)				
A615 rade	Reduction factor for seismic shear	αv,seis	-		0.70										
STM	Strength reduction factor for tension ²	φ	-		0.65										
	oli erigiri reduction factor	φ	-		0.60										
96	Nominal etronath as	N _{sa}	lb	8,800	16,000	24,800	35,200	48,000	63,200	80,000	101,600				
A96		I V sa	(kN)	(39.1)	(71.2)	(110.3)	(156.6)	(213.5)	(281.1)	(355.9)	(452.0)				
37,	(for a single anchor)	V _{sa}	lb (kN)	5,280	9,600	14,880	21,120	28,800	37,920	48,000	60,960				
5, A76 ade 60		αv,seis	- (KIN)	(23.5)	(23.5) (42.7) (66.2) (93.9) (128.1) (168.7) (213.5) (271.2) 0.70										
M A61 Gr	Strength reduction factor	φ	-	0.65											
ASTI	Strength reduction factor for shear ²	φ	-				0	.60							
	Nominal strength as	N _{sa}	lb	8,800	16,000	24,800	35,200	48,000	63,200	80,000	101,600				
9		I Vsa	(kN)	(39.1)	(71.2)	(110.3)	(156.6)	(213.5)	(281.1)	(355.9)	(452.0)				
ade		V_{sa}	lb (LN)	5,280	9,600	14,880	21,120	28,800	37,920	48,000	60,960				
ğ			(kN)	(23.5)	(42.7)	(66.2)	(93.9)	(128.1)	(168.7)	(213.5)	(271.2)				
۸706	shear	αv,seis					0	.70							
ASTM A706 Grade 60	Strength reduction factor ϕ for tension ²	φ					0	.75							
	Strength reduction factor ϕ for shear ²	φ					0	.65							
	Nominal strength as	N _{sa}	lb	6,600	12,000	18,600	26,400								
46	governed by steel strength	IVsa	(kN)	(29.4)	(53.4)	(82.7)	(117.4)								
Grade 40	(for a single anchor)	V _{sa}	lb (kN)	3,960 (17.6)	7,200 (32.0)	11,160 (49.6)	15,840 (70.5)			M A615, Grad zes No. 3 thro					
2	Reduction factor for seismic shear	αv,seis	-	0.70											
Ä	Strength reduction factor for tension ²	φ	-				0	.65							
AS ⁻	Strength reduction factor for shear ²	φ	-				0	.60							

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006894 MPa. For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

TABLE 9—CONCRETE BREAKOUT DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT REINFORCING BARS1

DECICAL INFORMATION	Symbol	Halta				Nomin	al Bar Size					
DESIGN INFORMATION	Symbol	Units	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 9	No.10		
Effectiveness factor for cracked concrete	k _{c,cr}	in-lb (SI)					17 (7)					
Effectiveness factor for uncracked concrete	k _{c,uncr}	inlb. (SI)					24 (10)					
Min. anchor spacing	Smin	in. (mm)										
Min. edge spacing ⁴	C _{min}	in. (mm)	1 ⁵ / ₈ (41)	1 ³ / ₄ (44)	2 (51)	2 ³ / ₈ (60)	2 ¹ / ₂ (64)	2 ³ / ₄ (70)	3 (76)	3 ¹ / ₄ (82)		
	Cmin	(11111)	(+1)	(44)	See Se	ection 4.1.9 of t	his report for s	maller edge dis	stances with ().45 T _{max}		
Min. member thickness	h _{min}	in. (mm)		+ 1 ¹ / ₄ + 30)		h _{ef}	+ 2d ₀ where d	is hole diame	ter			
Critical edge spacing – splitting (for uncracked concrete) ²	Cac	1				See Section 4	.1.10 of this rep	oort.				
Critical anchor spacing – splitting	Sac	-					2 · <i>C</i> ac					
Strength reduction factor for tension, concrete failure modes ²	φ	-	0.65									
Strength reduction factor for shear, concrete failure modes ²	φ	-	0.70									

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa. For **pound-inch** units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

¹Values provided for common bar material types based on specified strengths and calculated in accordance with ACI 318-19 Eq. 17.6.1.

²The tabulated value of φ applies when the load combinations of Section 1605.1 of the 2024 IBC or ACI 318-19 as set forth in ACI 318-19 17.5.3 are used.

 $^{^3}$ In accordance with ASTM A615, Grade 40 bars are furnished only in sizes No. 3 through No. 6.

¹Additional setting information is described in Figure 4, installation instructions.

²The strength reduction factor applies when the load combinations from the IBC or ACI 318 are used and the requirements of ACI 318-19 17.5.3 are met.

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TABLE 10—BOND STRENGTH DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR DEWALT HOLLOW CARBIDE DRILL BIT)¹

	DESIGN INFOR	DMATION.	Symbol	Units				Nomina	al Bar Size)		
	DESIGN INFOR	NIMATION	Symbol	Units	No.3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 9	No.10
	Minimum emb	pedment	h _{ef,min}	in. (mm)	2 ³ / ₈ (60)	2 ³ / ₄ (70)	3 ¹ / ₈ (79)	3 ¹ / ₂ (89)	3 ¹ / ₂ (89)	4 (102)	4 ¹ / ₂ (114)	5 (127)
	Maximum emb	bedment	h _{ef,max}	in. (mm)	7 ¹ / ₂ (191)	10 (254)	12 ¹ / ₂ (318)	15 (381)	17 ¹ / ₂ (445)	20 (508)	22.5 (572)	25 (635)
Temperature		stic bond strength in acked concrete	Tk,uncr	psi (N/mm²)	1,945 (13.4)	1,910 (13.1)	1,875 (12.9)	1,845 (12.7)	1,810 (12.4)	1,775 (12.2)	1,705 (11.7)	1,705 (11.7)
range A ^{2,3}		stic bond strength in ked concrete	Tk,cr	psi (N/mm²)	1,460 (10.0)	1,460 (10.0)	1,315 (9.0)	1,460 (10.0)	1,460 (10.0)	1,460 (10.0)	1,430 (9.8)	1,430 (9.8)
Temperature		stic bond strength in acked concrete	Tk,uncr	psi (N/mm²)	1,525 (10.5)	1,495 (10.3)	1,470 (10.1)	1,445 (9.9)	1,420 (9.7)	1,390 (9.5)	1,330 (9.1)	1,335 (9.2)
range B ^{2,3}		stic bond strength in ked concrete	Tk,cr	psi (N/mm²)	1,145 (7.8)	1,145 (7.8)	1,030 (7.1)	1,145 (7.8)	1,145 (7.8)	1,145 (7.8)	1,120 (7.7)	1,120 (7.7)
Temperature		stic bond strength in acked concrete	$ au_{k,uncr}$	psi (N/mm²)	855 (5.9)	840 (5.8)	825 (5.7)	810 (5.6)	795 (5.5)	785 (5.4)	755 (5.2)	755 (5.2)
range C ^{2,3}		stic bond strength in ked concrete	Tk,cr	psi (N/mm²)	680 (4.7)	680 (4.7)	680 (4.7)	680 (4.7)	680 (4.7)	680 (4.7)	680 (4.7)	680 (4.7)
	Dry concrete	Anchor Category	-	-					1			
	Dry concrete	Strength reduction factor	ϕ_{d}	-				(0.65			
	Water-saturated	Anchor Category	-	-					2			
	concrete	Strength reduction factor	φws	-				(0.55			
Permissible installation		Anchor Category	-	-					3			
conditions	Water-filled hole (flooded)	Strength reduction factor	ϕ_{wt}	-				(0.45			
	(nooded)	Modification factor for Water-filled holes	Kwf	-				(0.85			
	Underwater Anchor Category			-	2							
	(submerged) Strength reduction factor			-	0.55							
Red	Reduction factor for seismic tension			-	1.00							

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 006894 MPa. For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

¹Bond strength values correspond to concrete compressive strength f_c = 2,500 psi (17.2 N/mm²). For uncracked concrete compressive strength, f_c between 2,500 psi (17.2 N/mm²) and 8,000 psi (55.2 N/mm²), the tabulated characteristic bond strength may be increased by a factor of (f_c / 2500)^{0.18} [For SI: (f_c / 17.2)^{0.18}]. See Section 4.1.4 of this report.

²Temperature range A: Maximum short term temperature = 140°F (60°C), maximum long term temperature = 110°F (43°C); Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 110°F (43°C); Temperature range C: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 140°F (60°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

³Characteristic bond strengths are for sustained loads including dead and live loads. For load combinations consisting of short-term loads only such as wind or seismic, bond strengths may be increased by 17 percent for temperature range A and B and by 92 percent for temperature range C.

TABLE 11—BOND STRENGTH DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT REINFORCING BARS IN HOLES DRILLED WITH A DIAMOND CORE BIT¹

_	SECION INFO	PMATION	Completed	I I i a				Nomina	l Bar Size			
L	ESIGN INFO	RMATION	Symbol	Units	No.3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 9	No.10
	Minimum em	bedment	h _{ef,min}	in. (mm)	2 ³ / ₈ (60)	2 ³ / ₄ (70)	3 ¹ / ₈ (79)	3 ¹ / ₂ (89)	3 ¹ / ₂ (89)	4 (102)	4 ¹ / ₂ (114)	5 (127)
	Maximum embedment			in. (mm)	7 ¹ / ₂ (191)	10 (254)	12 ¹ / ₂ (318)	15 (381)	17 ¹ / ₂ (445)	20 (508)	22.5 (572)	25 (635)
Temperature range A ^{2,3}		eristic bond strength in cracked concrete	Tk,uncr	psi (N/mm²)	1,480 (10.2)	1,465 (10.1)	1,350 (9.3)	1,350 (9.3)	1,350 (9.3)	1,350 (9.3)	1,350 (9.3)	1,350 (9.3)
Temperature range B ^{2,3}		eristic bond strength in cracked concrete	Tk,uncr	psi (N/mm²)	1,205 (8.3)	1,205 (8.3)	1,100 (7.6)	1,100 (7.6)	1,100 (7.6)	1,100 (7.6)	1,100 (7.6)	1,100 (7.6)
Temperature range C ^{2,3}		eristic bond strength in cracked concrete	Tk,uncr	psi (N/mm²)	870 (6.0)	870 (6.0)	800 (5.5)	800 (5.5)	800 (5.5)	800 (5.5)	800 (5.5)	800 (5.5)
	Dry	Anchor Category	-	-					1			
Permissible	Permissible concrete Strength reduction factor		ϕ_{d}	-				0.	65			
installation conditions	Water-	Anchor Category	-	-	1	2	2	2	3	3	3	3
CONGILIONS	saturated concrete	Strength reduction factor	ϕ_{ws}	-	0.65	0.55	0.55	0.55	0.45	0.45	0.45	0.45

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006894 MPa.

For **pound-inch** units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

Short term elevated concrete temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

³Characteristic bond strengths are for sustained loads including dead and live loads. For load combinations consisting of short-term loads only such as wind or seismic, bond strengths may be increased by 20 percent for temperature range A and B and by 61 percent for temperature range C.

TABLE 12—STEEL DESIGN INFORMATION FOR METRIC THREADED ROD1

DE	SIGN INFORMATION	Completed	I I a i i a a			Nomina	al Rod Diamete	er (mm)				
DE	SIGN INFORMATION	Symbol	Units	M10	M12	M16	M20	M24	M27	M30		
Threa	ded rod O.D.	da	mm (in.)	10 (0.39)	12 (0.47)	16 (0.63)	20 (0.79)	24 (0.94)	27 (1.06)	30 (1.18)		
	ded rod effective cross- nal area	Ase	mm² (in.²)	58.0 (0.090)	84.3 (0.131)	157 (0.243)	245 (0.380)	353 (0.547)	459 (0.711)	561 (0.870)		
5.8	Nominal strength as governed by steel	N _{sa}	kN (lb)	29.0 (6,518)	42.2 (9,473)	78.5 (17,643)	122.5 (27,532)	176.5 (39,668)	229.5 (51,580)	280.5 (63,043)		
S	strength (for a single anchor)	V _{sa}	kN (lb)	14.5 (3,260)	25.3 (5,684)	47.1 (10,586)	73.5 (16,519)	105.9 (23,801)	137.7 (30,948)	168.3 (37,826)		
898-1 C	Reduction factor for seismic shear	$\alpha_{V,seis}$	-									
SO 89	Strength reduction factor for tension ²	φ	- 0.65									
SI	Strength reduction factor for shear ²	φ	-	0.60								
8.8	Nominal strength as governed by steel	N _{sa}	kN (lb)	46.4 (10,428)	67.4 (15,157)	125.6 (28,229)	196 (44,051)	282.4 (63,470)	367.2 (82,528)	448.8 (100,868)		
Class 8	strength (for a single anchor)	V _{sa}	kN (lb)	23.0 (5,216)	40.5 (9,094)	75.4 (16,937)	117.6 (26,431)	169.4 (38,082)	220.3 (49,517)	269.3 (60,521)		
898-1 CI	Reduction factor for seismic shear	α <i>v,seis</i>	-				0.70					
SO 898	Strength reduction factor for tension ²	φ	-				0.65					
S	Strength reduction factor for shear ²	φ	-				0.60					
6	Nominal strength as governed by steel	N _{sa}	kN (lb)	40.6 (9,125)	59 (13,263)	109.9 (24,700)	171.5 (38,545)	247.1 (55,536)	229.5 (51,580)	280.5 (63,043)		
St -	strength (for a single anchor)	V _{sa}	kN (lb)	20.3 (4,564)	35.4 (7,958)	65.9 (14,820)	102.9 (23,127)	148.3 (33,322)	137.7 (30,948)	168.3 (37,826)		
SO 3506-1, stainless ste	Reduction factor for seismic shear	α <i>v,seis</i>	-				0.70					
ISO A4 stair	factor for tension ²	φ	-				0.65					
	Strength reduction factor for shear ²	φ	-	- 0.60								

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006894 MPa. For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

¹Bond strength values correspond to concrete compressive strength f'_c = 2,500 psi (17.2 N/mm²). For compressive strength, f'_c between 2,500 psi (17.2 N/mm²) and 8,000 psi (55.2 N/mm²), the tabulated characteristic bond strength may be increased by a factor of $(f'_c/2500)^{0.35}$ [For SI: $(f'_c/17.2)^{0.35}$]. See Section 4.1.4 of this report.

²Temperature range A: Maximum short term temperature = 140°F (60°C), maximum long term temperature = 110°F (43°C); Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 110°F (43°C); Temperature range C: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 140°F (60°C).

¹Values provided for common rod material types based on specified strengths and calculated in accordance with ACI 318-19 Eq. 17.6.1.2 and Eq. 17.7.1.2b. Nuts and washers must comply with requirements for the rod.

²The tabulated value of ϕ applies when the load combinations of Section 1605.1 of the 2024 IBC or ACI 318-19 5.3 as set forth in ACI 318-19 17.5.3 are used. ³A4-70 Stainless steel (M8-M24); A4-50 Stainless steel (M27-M30).

TABLE 13—CONCRETE BREAKOUT DESIGN INFORMATION FOR METRIC THREADED ROD 1

DESIGN INFORMATION	Symbol	Heito			Nomin	al Rod Diamete	er (mm)					
DESIGN INFORMATION	Symbol	Units	M10	M12	M16	M20	M24	M27	M30			
Effectiveness factor for cracked concrete	K _{c,cr}	SI (in-lb)				7 (17)						
Effectiveness factor for uncracked concrete	k _{c,uncr}	SI (in-lb)				10 (24)						
Min. anchor spacing	Smin	mm (in.)	50 (2)	60 (2 ³ / ₈)	80 (3 ¹ / ₈)	95 (3 ³ / ₄)	115 (4 ¹ / ₂)	130 (5 ¹ / ₈)	145 (5 ¹ / ₂)			
Min. edge distance	C _{min}	mm (in.)	40 (1 ⁵ / ₈)	45 (1 ³ / ₄)	55 (2 ¹ / ₄)	60 (2 ³ / ₈) 1 4.1.9 of this rep	70 (2 ³ / ₄)	75 (3)	80 (3 ¹ / ₈)			
Min. member thickness	h _{min}	mm (in.)		$\frac{1}{e^f + 30}$ $\frac{1}{f + 1^1/4}$	OCC OCCIIO		where d_0 is hole		With 0.43 Finax			
Critical edge distance - splitting (for uncracked concrete) ²	Cac	-	See Section 4.1.10 of this report.									
Strength reduction factor for tension, concrete failure modes ²	φ	-	0.65									
Strength reduction factor for shear, concrete failure modes ²	φ		0.70									

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006894 MPa. For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

TABLE 14—BOND STRENGTH DESIGN INFORMATION FOR METRIC THREADED ROD IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR DEWALT HOLLOW CARBIDE DRILL BIT)1

	DESIGN INFOR	DMATION	Symbol	Units			Nominal	Rod Diame	ter (inch)		
	DESIGN INFOR	IMATION	Symbol	Units	M10	M12	M16	M20	M24	M27	M30
	Minimum emb	edment	h _{ef,min}	mm (in.)	60 (2.4)	70 (2.8)	80 (3.1)	90 (3.5)	96 (3.8)	108 (4.3)	120 (4.7)
	Maximum emb	pedment	h _{ef,max}	mm (in.)	200 (7.8)	240 (14.8)	320 (12.6)	400 (15.8)	480 (18.8)	540 (21.4)	600 (23.6)
Temperature		stic bond strength in cked concrete	T _{k,uncr}	N/mm² (psi)	15.0 (2,190)	14.8 (2,150)	14.2 (2,070)	13.7 (1,995)	13.2 (1,915)	12.7 (1,855)	12.3 (1,795)
range A ^{2,3}		stic bond strength in ked concrete	Tk,cr	N/mm² (psi)	10.5 (1,525)	10.6 (1,540)	9.4 (1,375)	10.7 (1,555)	10.5 (1,535)	10.3 (1,495)	9.9 (1,450)
Temperature		stic bond strength in cked concrete	Tk,uncr	N/mm² (psi)	11.8 (1,715)	11.6 (1,685)	11.1 (1,625)	10.7 (1,560)	10.3 (1,500)	10.0 (1,453)	9.7 (1,405)
range B ^{2,3}		stic bond strength in ked concrete	$ au_{k,cr}$	N/mm² (psi)	8.2 (1,195)	8.3 (1,205)	7.4 (1,080)	8.3 (1,215)	8.2 (1,200)	8.0 (1,170)	7.8 (1,135)
Temperature		stic bond strength in cked concrete	T _{k,uncr}	N/mm² (psi)	6.7 (970)	6.4 (930)	6.0 (870)	5.8 (840)	5.5 (800)	5.4 (785)	5.3 (770)
range C ^{2,3}		stic bond strength in ked concrete	Tk,cr	N/mm² (psi)	4.5 (650)	4.2 (610)	4.0 (580)	3.8 (550)	3.7 (535)	3.6 (520)	3.6 (520)
	Dry Concrete	Anchor category	ı	-				1			
	Dry Concrete	Strength reduction factor	ϕ_d	ı				0.65			
	Water-saturated	Anchor category	-	-				2			
Permissible	Concrete	Strength reduction factor	$\phi_{ m ws}$	-				0.55			
installation conditions		Anchor category	-	-				3			
Conditions	Water-filled hole (flooded)	Strength reduction factor	ϕ_{wt}	-				0.45			
	, ,	Modification factor for water filled holes	K_{Wf}	-				0.85			
	Underwater	Anchor Category	-	-				2			
	(submerged)	Strength reduction factor	$\phi_{\scriptscriptstyle UW}$	-				0.55			
Re	Reduction factor for seismic tension			-	1.00	1.00	0.90	0.94	0.94	1.00	1.00

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006894 MPa. For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

¹Additional setting information is described in <u>Figure 4</u>, installation instructions. ²The strength reduction factor applies when the load combinations from the IBC or ACI 318 are used and the requirements of ACI 318-19 17.5.3 are met.

¹Bond strength values correspond to concrete compressive strength $f_c = 2,500$ psi (17.2 N/mm²). For concrete compressive strength, f_c between 2,500 psi (17.2 N/mm²) and 8,000 psi (55.2 N/mm²), the tabulated characteristic bond strength may be increased by a factor of $(f_c/2500)^{0.21}$ [For SI: $(f_c/17.2)^{0.21}$] for uncracked concrete and $(f_c/2500)^{0.14}$ [For SI: $(f_c/17.2)^{0.14}$] for cracked concrete. See Section 4.1.4 of this report.

²Temperature range A: Maximum short term temperature = 140°F (60°C), maximum long term temperature = 110°F (43°C); Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 110°F (43°C); Temperature range C: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 140°F (60°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

³ Characteristic bond strengths are for sustained loads including dead and live loads. For load combinations consisting of short-term loads only such as wind or seismic, bond strengths may be increased by 17 percent for temperature range A and B and by 92 percent for temperature range C.

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TABLE 15—STEEL DESIGN INFORMATION FOR EU METRIC AND CANADIAN METRIC REINFORCING BARS 1

DESIG	N INFORMATION	Symbol	Unito				Nominal	Bar Size (EU	J)			
DESIG	IN INFORMATION	Symbol	Ullits	ø 10	Ø 12	ø 14	ø 16	Ø 20	ø 25	ø 28	ø 32	
Reinforcing ba	ar O.D.	da	mm (in.)	10 (0.394)	12 (0.472)	14 (0.551)	16 (0.630)	20 (0.787)	25 (0.984)	28 (1.102)	32 (1.260)	
Reinforcing ba sectional area	ar effective cross-	Ase	mm² (in.²)	78.5 (0.121)	113.1 (0.175)	153.9 (0.239)	201.1 (0.312)	314.2 (0.487)	490.9 (0.761)	615.8 (0.954)	804.2 (1.247)	
	Nominal strength as governed by steel	N _{sa}	kN (lb)	43.2 (9,739)	62.2 (14,024)	84.7 (19,088)	110.6 (24,932)	172.8 (38,956)	270.0 (60,868)	338.7 (76,353)	442.3 (99,727)	
DIN 488 BSt 500	strength (for a single anchor)	V _{sa}	kN (lb)	25.9 (5,843)	37.3 (8,414)	50.8 (11,453)	66.4 (14,959)	103.7 (23,373)	162.0 (36,521)	203.2 (45,812)	265.4 (59,836)	
88 B(Reduction factor for seismic shear	av,seis €	-					0.70				
N A	Strength reduction factor for tension ²	φ	-	- 0.65								
	Strength reduction factor for shear ²	φ	-	- 0.60								
DESIG	N INFORMATION	Symbol	Units				Nominal Bar					
DEGIC	it itt ottillation	Cymbol	Office	10M		15M		OM	25M		30M	
Rein	forcing bar O.D.	da	mm (in.)	11.3 (0.445)	16.0 (0.630)		9.5 768)	25.2 (0.992)		29.9 (1.177)	
	ng bar effective cross- ectional area	Ase	mm² (in.²)	100.3 (0.155)		201.1 (0.312)	(0.4	8.6 163)	498.8 (0.773)		702.2 (1.088)	
8	Nominal strength as governed by steel	N _{sa}	kN (lb)	54.0 (12,175	5)	108.5 (24,410)	(36,	1.5 255)	270.0 (60,550)		380.0 (85,240)	
330.18	strength (for a single anchor)	V _{sa}	kN (lb)	32.5 (7,305))	65.0 (14,645)		7.0 755)	161.5 (36,330)		227.5 (51,145)	
CAN/CSA G30.18	Reduction factor for seismic shear	αv,seis	-	·				0.70		·		
AN/C	Strength reduction factor for tension ²	φ	-					0.65				
	Strength reduction factor for shear ²	φ	-					0.60				

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006894 MPa. For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

TABLE 16—CONCRETE BREAKOUT DESIGN INFORMATION FOR EU AND CANADIAN METRIC REINFORCING BARS 1

TABLE 10—CONCRETE	DHEARC	שם וטכ	SIGN II	AL OUNIN	ATTON I	ON EU	AND C	ANADI	AN IVIE	I NIC N		CING	MNO		
DESIGN INFORMATION	Cumbal	Units						Nom	inal Bar	Size					
DESIGN INFORMATION	Symbol	Ullits	Ø 10	10M	Ø 12	Ø 14	15M	Ø 16	Ø 20	20M	Ø 25	25M	Ø 28	30M	Ø 32
Effectiveness factor for cracked concrete	K _{c,cr}	SI (in-lb)							7 (17)						
Effectiveness factor for uncracked concrete	k _{c,uncr}	SI (in-lb)							10 (24)						
Min. anchor spacing	S _{min}	mm (in.)	50 (2)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$											
Min. edge spacing	Gmin	mm	40	45	45	50 (2)	50 (2)	55 (2 ¹ / ₄)	60 (2 ³ / ₈)	60 (2 ³ / ₈)	70 (2 ³ / ₄)	70 (2 ³ / ₄)	75 (3)	80 (3 ¹ / ₈)	85 (3 ¹ / ₈)
dage opaog	Cmin	(in.)	$(1^{5}/_{8})$	(13/4)	$(1^{3}/_{4})$	S	ee Secti	on 4.1.9	of this re	port for s	maller ed	dge dista	nces with	0.45 <i>T</i> m	ıax
Min. member thickness	h _{min}	mm (in.)		$h_{ef} + 30$ $(h_{ef} + 1^{1}/_{4})$)				h _{ef} + 2d ₀	where a	lo is hole	diameter			
Critical edge spacing – splitting (for uncracked concrete) ²	Cac	-					See	Section	4.1.10 o	f this rep	ort.				
Strength reduction factor for tension, concrete failure modes ²	φ	-	0.65												
Strength reduction factor for shear, concrete failure modes ²	φ	-	0.70												

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006894 MPa. For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

¹Values provided for common bar material types based on specified strengths and calculated in accordance with ACI 318-19 Eq. 17.6.1.2 and Eq. 17.7.1.2b.

²The tabulated value of φ applies when the load combinations of Section 1605.1 of the 2024 IBC or ACI 318-19 5.3 as set forth in ACI 318-19 17.5.3 are used.

¹Additional setting information is described in <u>Figure 4</u>, installation instructions.

²The strength reduction factor applies when the load combinations from the IBC or ACI 318 are used and the requirements of ACI 318-19 17.5.3 are met.

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TABLE 17—BOND STRENGTH DESIGN INFORMATION EU METRIC REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR DEWALT HOLLOW CARBIDE DRILL BIT)¹

	DESIGN INFOR	MATION	Symbol	Units			N	Iominal Ba	ar Size (E	U)		
	DESIGN INFOR	WIATION	Syllibol	Units	Ø 10	Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
	Minimum embe	edment	h _{ef,min}	mm. (in.)	60 (2.4)	70 (2.8)	75 (3.0)	80 (3.1)	90 (3.5)	100 (3.9)	112 (4.4)	128 (5.0)
	Maximum emb	edment	h _{ef,max}	mm (in.)	200 (7.9)	240 (9.4)	280 (11.0)	320 (12.6)	400 (15.7)	500 (19.7)	560 (22.0)	640 (25.2)
Temperature		tic bond strength in cked concrete	□k,uncr	N/mm² (psi)	13.3 (1,940)	13.2 (1,920)	13.0 (1,895)	12.8 (1,855)	12.5 (1,815)	12.2 (1,775)	12.0 (1,745)	11.7 (1,705)
range A ^{2,3}		tic bond strength in ked concrete	□k,cr	N/mm² (psi)	10.0 (1,460)	10.0 (1,460)	10.0 (1,460)	9.0 (1,315)	10.0 (1,460)	10.0 (1,460)	9.8 (1,430)	9.8 (1,430)
Temperature		tic bond strength in cked concrete	□k,uncr	N/mm² (psi)	10.4 (1,520)	10.3 (1,505)	10.2 (1,485)	10.0 (1,455)	9.7 (1,420)	9.5 (1,390)	9.4 (1,365)	9.2 (1,335)
range B ^{2,3}		tic bond strength in ked concrete	□ _{k,cr}	N/mm² (psi)	7.8 (1,145)	7.8 (1,145)	7.8 (1,145)	7.1 (1,030)	7.8 (1,145)	7.8 (1,145)	7.7 (1,120)	7.7 (1,120)
Temperature		tic bond strength in cked concrete	□k,uncr	N/mm² (psi)	5.9 (855)	5.8 (840)	5.7 (825)	5.6 (810)	5.5 (795)	5.4 (785)	5.3 (770)	5.2 (755)
range C ^{2,3}	Characteris crack	□k,cr	N/mm² (psi)	4.7 (680)	4.7 (680)	4.7 (680)	4.7 (680)	4.7 (680)	4.7 (680)	4.7 (680)	4.7 (680)	
	Dry Concrete	Cracked concrete Anchor category Dry Concrete		-					1			
	Dry Concrete	Strength reduction factor	□d	-				0.	65			
	Water-saturated	Anchor category		-				2	2			
Permissible	Concrete	Strength reduction factor	□ws	-				0.	55			
installation conditions		Anchor category		-				(3			
Conditions	Water-filled hole (flooded)	Strength reduction factor	\Box_{wf}	-				0.	45			
	Modification factor fo water filled holes		□wf	-				0.	85			
	Underwater	Anchor Category	-	-				2	2			
	(submerged) Strength reduction factor		□ _{uw}	-	0.55							
Re	eduction factor for se	eismic tension	α _{N,seis}	-				1	.0			

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006894 MPa.For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

¹Bond strength values correspond to concrete compressive strength $f_c = 2,500$ psi (17.2 N/mm²).. For uncracked concrete compressive strength, f_c between 2,500 psi (17.2 N/mm²) and 8,000 psi (55.2 N/mm²), the tabulated characteristic bond strength may be increased by a factor of $(f_c/2500)^{0.18}$ [For SI: $(f_c/17.2)^{0.18}$]. See Section 4.1.4 of this report

Section 4.1.4 of this report.

2Temperature range A: Maximum short term temperature = 140°F (60°C), maximum long term temperature = 110°F (43°C); Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 176°F (80°C), maximum long term temperature = 140°F (60°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

³Characteristic bond strengths are for sustained loads including dead and live loads. For load combinations consisting of short-term loads only such as wind or seismic, bond strengths may be increased by 17 percent for temperature range A and B and by 92 percent for temperature range C.



TABLE 18—BOND STRENGTH DESIGN INFORMATION METRIC CANADIAN REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR DEWALT HOLLOW CARBIDE DRILL BIT)1

	DECION INFOR	MATION	Comple ed	Heite		Nomir	nal Rod Diamete	er (CA)			
	DESIGN INFOR	MATION	Symbol	Units	10M	15M	20M	25M	30M		
	Minimum emb	edment	h _{ef,min}	mm. (in.)	60 (2.4)	80 (3.1)	90 (3.5)	100 (3.9)	120 (4.7)		
	Maximum emb	edment	h _{ef,max}	mm (in.)	200 (7.9)	300 (11.8)	400 (15.7)	500 (19.7)	600 (23.6)		
Temperature		tic bond strength in cked concrete	$ au_{k,uncr}$	N/mm² (psi)	12.7 (1,850)	12.2 (1,780)	12.0 (1,745)	11.8 (1,720)	11.4 (1,665)		
range A ^{2,3}		tic bond strength in ked concrete	Tk,cr	N/mm² (psi)	9.0 (1,305)	7.9 (1,155)	8.6 (1,253)	8.4 (1,225)	8.1 (1,175)		
Temperature		tic bond strength in cked concrete	Tk,uncr	N/mm² (psi)	9.9 (1,450)	9.6 (1,395)	9.4 (1,370)	9.2 (1,350)	8.9 (1,300)		
range B ^{2,3}		tic bond strength in ked concrete	Tk,cr	N/mm² (psi)	7.0 (1,020)	6.2 (905)	6.7 (980)	6.6 (960)	6.3 (920)		
Temperature	Characteris uncra	$ au_{k,uncr}$	N/mm² (psi)	5.6 (810)	5.5 (795)	5.4 (785)	5.2 (755)	5.1 (740)			
range C ^{2,3}		tic bond strength in ked concrete	Tk,cr	N/mm² (psi)	4.2 (610)	4.1 (595)	4.0 (580)	4.0 (580)	4.0 (580)		
	Dry Concrete	Anchor category	_	-			1				
	Dry Concrete	Strength reduction factor	фа	-			0.65				
	Water-saturated	Anchor category	_	-			2				
D	Concrete	Strength reduction factor	φws	-			0.55				
Permissible installation		Anchor category	_	-			3				
conditions	Water-filled hole	Strength reduction factor	ϕ_{wt}	-			0.45				
	(flooded) Modification factor for water filled holes		K_{wf}	-			0.85				
	Underwater Anchor Category		-	-	2						
	(submerged) Strength reduction factor			-	0.55						
Reduction factor	ction factor for seismic tension			-	1.0						

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006894 MPa. For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

Bond strength values correspond to concrete compressive strength f'_c = 2,500 psi (17.2 N/mm²). For uncracked concrete compressive strength, f'_c between 2,500 psi (17.2 N/mm²) and 8,000 psi (55.2 N/mm²), the tabulated characteristic bond strength may be increased by a factor of $(f_c/2500)^{0.08}$ [For SI: $(f_c/17.2)^{0.08}$] for uncracked concrete and $(f_c/2500)^{0.09}$ [For SI: $(f_c/17.2)^{0.09}$] for cracked concrete. See Section 4.1.4 of this report.

² Temperature range A: Maximum short term temperature = 140°F (60°C), maximum long term temperature = 110°F (43°C); Temperature range B: Maximum short term temperature = 110°F (80°C), maximum long term temperature = 176°F (80°C), maximum short term temperature = 176°F (80°C), maximum long term temperature = 140°F (60°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling. Long term concrete temperatures are roughly

onstruction of state of the constant over significant periods of time.

3 Characteristic bond strengths are for sustained loads including dead and live loads. For load combinations consisting of short-term loads only such as wind or seismic, bond strengths may be increased by 17 percent for temperature range A and B and by 92 percent for temperature range C.

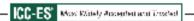


TABLE 19—DEVELOPMENT LENGTH FOR U.S. CUSTOMARY UNIT REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR DEWALT HOLLOW CARBIDE DRILL BIT) OR DIAMOND CORE BIT^{1,2,4,5,6}

	_						No	minal Bar	size			
DESIGN INFORMATION	Symbol	Criteria Section of Reference Standard	Units	#3	#4	#5	#6	#7	#8	#9	#10	#11
Naminal rainforcing har diameter	d _b		in.	0.375	0.500	0.625	0.750	0.875	1.000	1.128	1.270	1.410
Nominal reinforcing bar diameter	Цb	ASTM A615/	(mm)	(9.5)	(12.7)	(15.9)	(19.1)	(22.2)	(25.4)	(28.7)	(32.3)	(35.8)
Naminal har area	4	A706 Grade 60	in ²	0.11	0.20	0.31	0.44	0.60	0.79	1.00	1.27	1.56
Nominal bar area	Ab		(mm²)	(71)	(129)	(199)	(284)	(387)	(510)	(645)	(819)	(1006)
Development length for $f_y = 60 \text{ ksi}$,		in.	12.0	14.4	18.0	21.6	31.5	36.0	40.6	45.7	50.8
and $f'_c = 2,500 \text{ psi}$ (normal weight concrete) ³	I _d		(mm)	(305)	(366)	(457)	(549)	(800)	(914)	(1031)	(1161)	(1289)
Development length for $f_y = 60 \text{ ksi}$,		in.	12.0	13.1	16.4	19.7	28.8	32.9	37.1	41.7	46.3
and $f'_c = 3,000 \text{ psi}$ (normal weight concrete) ³	I _d		(mm)	(305)	(334)	(417)	(501)	(730)	(835)	(942)	(1060)	(1177)
Development length for $f_y = 60$ ksi	,	ACI 318-19 25.4.2.4	in.	12.0	12.0	14.2	17.1	24.9	28.5	32.1	36.1	40.1
and $f'_c = 4,000 \text{ psi}$ (normal weight concrete) ³	I _d	AGI 316-19 25.4.2.4	(mm)	(305)	(305)	(361)	(434)	(633)	(723)	(815)	(918)	(1019)
Development length for $f_y = 60 \text{ ksi}$,		in.	12.0	12.0	12.0	13.9	20.3	23.2	26.2	29.5	32.8
and $f'_c = 6,000 \text{ psi}$ (normal weight concrete) ³	I _d		(mm)	(305)	(305)	(305)	(354)	(516)	(590)	(666)	(750)	(832)
Development length for $f_y = 60 \text{ ksi}$,		in.	12.0	12.0	12.0	12.1	17.6	20.1	22.7	25.6	28.4
and $f'_c = 8,000 \text{ psi}$ (normal weight concrete) ³	I _d		(mm)	(305)	(305)	(305)	(307)	(447)	(511)	(577)	(649)	(721)

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa. For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

$${}^{4}\!\left(\frac{c_{b}+K_{tr}}{d_{b}}\right)=2.5\,,\;\psi_{t}=1.0,\;\psi_{e}=1.0,\;\psi_{s}=0.8\;\text{for}\;d_{b}\leq\#6,\;1.0\;\text{for}\;d_{b}>\#6.$$

TABLE 20—DEVELOPMENT LENGTH FOR EU METRIC REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR DEWALT HOLLOW CARBIDE DRILL BIT) OR DIAMOND CORE BIT 1.2.4.5.6

	0						Nominal	Bar size			
DESIGN INFORMATION	Symbol	Criteria Section of Reference Standard	Units	ф 10	ф 12	ф 16	ф 20	ф 25	ф 28	ф 32	ф 36
Nominal reinforcing bar diameter	d		mm	10	12	16	20	25	28	32	36
Norminal reinforcing bar diameter	dь	DIN 488, BSt 500	(in.)	(0.394)	(0.472)	(0.630)	(0.787)	(0.984)	(1.102)	(1.260)	(1.417)
Nominal bar area	4	(BS 4449:2005)	mm²	79	113	201	314	491	616	804	1018
Nominai bar area	Ab		(in²)	(0.12)	(0.18)	(0.31)	(0.49)	(0.76)	(0.95)	(1.25)	(1.58)
Development length for $f_y = 72.5 \text{ ksi}$			mm	348	418	557	870	1088	1218	1392	1566
and $f'_c = 2,500 \text{ psi}$ (normal weight concrete) ³	ld		(in.)	(13.7)	(16.4)	(21.9)	(34.3)	(42.8)	(48.0)	(54.8)	(61.7)
Development length for $f_y = 72.5 \text{ ksi}$			mm	318	381	508	794	993	1112	1271	1430
and $f'_c = 3,000 \text{ psi}$ (normal weight concrete) ³	I _d		(in.)	(12.5)	(15.0)	(20.0)	(31.3)	(39.1)	(43.8)	(50.0)	(56.3)
Development length for $f_y = 72.5$ ksi		A OL 040 40 05 4 0 4 ⁷	mm	305	330	440	688	860	963	1100	1238
and $f'_c = 4,000 \text{ psi}$ (normal weight concrete) ³	ld	ACI 318-19 25.4.2.4 ⁷	(in.)	12.0	13.0	17.3	27.1	33.8	37.9	43.3	48.7
Development length for $f_y = 72.5 \text{ ksi}$			mm	305	305	359	562	702	786	899	1011
and $f'_c = 6000 \text{ psi}$ (normal weight concrete) ³	l _d		(in.)	(12.0)	(12.0)	(14.2)	(22.1)	(27.6)	(31.0)	(35.4)	(39.8)
Development length for $f_y = 72.5$ ksi and $f'_c = 8000$ psi			mm	305	305	311	486	608	681	778	875
(normal weight concrete) 3	I _d		(in.)	(12.0)	(12.0)	(12.3)	(19.1)	(23.9)	(26.8)	(30.6)	(34.5)

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa. For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

$$4\left(\frac{c_b + K_{tr}}{d_b}\right) = 2.5$$
, $\psi_t = 1.0$, $\psi_e = 1.0$, $\psi_s = 0.8$ for $d_b < 20$ mm, 1.0 for $d_b \ge 20$ mm.

¹Development lengths valid for static, wind, and earthquake loads (SDC A and B).

²Development lengths in SDC C through F must comply with ACI 318-19 Chapter 18 and section 4.2.4 of this report.

 $^{^3}$ f_y and f_c used in this table are for example purposes only. For sand-lightweight concrete, increase development length by 33%, unless the provisions of ACI 318-19 25.4.2.5 are met to permit $\lambda > 0.75$.

⁵Calculations may be performed for other steel grades per ACI 318-19 Chapter 25.

⁶Minimum development length shall not be less than 12 in (305 mm) per ACI-19 Section 25.4.2.1.

¹Development lengths valid for static, wind, and earthquake loads (SDC A and B).

²Development lengths in SDC C through F must comply with ACI 318-19 Chapter 18 and section 4.2.4 of this report.

 $^{^3}$ f_y and f'_c used in this table are for example purposes only. For sand-lightweight concrete, increase development length by 33%, unless the provisions of ACI 318-19 25.4.2.5 are met to permit $\lambda > 0.75$.

⁵Calculations may be performed for other steel grades per ACI 318-19 Chapter 25.

⁶Minimum development length shall not be less than 12 in (305 mm) per ACI-19 Section 25.4.2.1.

 $^{^{7}}$ l_{0} must be increased by 9.5% to account for ψ_{0} in ACI 318-19 25.4.2.4. ψ_{0} has been interpolated from Table 25.4.2.5 of ACI 318-19 for $f_{y}=72.5$ ksi.



TABLE 21—DEVELOPMENT LENGTH FOR CA METRIC REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR DEWALT HOLLOW CARBIDE DRILL BIT) OR DIAMOND CORE BIT^{1,2,4,5,6}

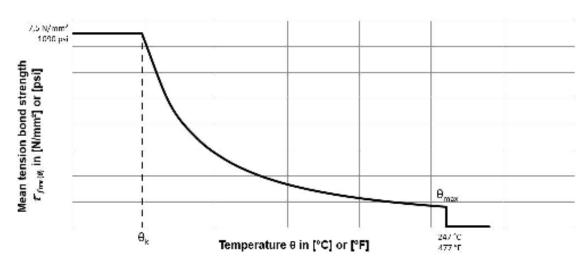
WITH A HAWWEN DRIL	LAN	D CALIDIDE BIT (OR	DEWA	LITIOLLOW	CALIDIDE DI			OHE BIT	•
	Symbol	Criteria Section of Reference Standard	Units	Bar size					
DESIGN INFORMATION				10M	15M	20M	25M	30M	35M
Nominal reinforcing bar diameter	dь	CAN/CSA G30.18 Grade 400	mm (in.)	11.3 (0.445)	16.0 (0.630)	19.5 (0.768)	25.2 (0.992)	29.9 (1.177)	35.7 (1.406)
Nominal bar area	A_b		mm² (in²)	100 (0.16)	200 (0.31)	300 (0.46)	500 (0.77)	700 (1.09)	1000 (1.56)
Development length for $f_y = 58$ ksi and $f'_c = 2,500$ psi (normal weight concrete) ³	I _d	ACI 318-19 25.4.2.4 ⁷	mm (in.)	315 (12.4)	446 (17.5)	679 (26.7)	877 (34.5)	1041 (41.0)	1243 (48.9)
Development length for $f_y = 58$ ksi and $f'_c = 3,000$ psi (normal weight concrete) ³	I _d		mm (in.)	305 (12.0)	407 (16.0)	620 (24.4)	801 (31.5)	950 (37.4)	1134 (44.7)
Development length for $f_y = 58$ ksi and $f'_c = 4,000$ psi (normal weight concrete) ³	I _d		mm (in.)	305 (12.0)	352 (13.9)	537 (21.1)	693 (27.3)	823 (32.4)	982 (38.7)
Development length for $f_y = 58$ ksi and $f'_c = 6000$ psi (normal weight concrete) ³	I _d		mm (in.)	305 (12.0)	305 (12.0)	438 (17.2)	566 (22.3)	672 (26.4)	802 (31.6)
Development length for $f_y = 58$ ksi and $f'_c = 8000$ psi (normal weight concrete) ³	I _d		mm (in.)	305 (12.0)	305 (12.0)	379 (14.9)	490 (19.3)	582 (22.9)	695 (27.3)

For **SI:** 1 inch \equiv 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

$${}^{4}\left(\frac{C_{b}+K_{tr}}{d_{b}}\right)=2.5 \text{ , } \psi_{t}=1.0, \ \psi_{e}=1.0, \ \psi_{s}=0.8 \text{ for } d_{b}<20 \text{mm}, \ 1.0 \text{ for } d_{b}\geq20 \text{mm}.$$

⁷ I_d must be increased by 9.5% to account for ψ_g in ACI 318-19 25.4.2.4. ψ_g has been interpolated from Table 25.4.2.5 of ACI 318-19 for fy = 72.5 ksi.



The mean tension bond strength $\bar{\tau}_{fire}(\theta)$ under fire conditions shall be determined in accordance with the following equations:

For hammer drill and carbide bit (or DEWALT hollow carbide bit):	For diamond core bit:
$\bar{\tau}_{fire}(\theta) = 1955671 \cdot \theta^{-1.585} \le 1090 \text{ [psi] with } \theta \text{ in } {}^{\circ}\text{F}$	$\bar{\tau}_{fire}(\theta) = 1814842 \cdot \theta^{-1.585} \le 1090 \text{ [psi] with } \theta \text{ in } {}^{\circ}\text{F}$
$\bar{\tau}_{fire}(\theta) = 1277 \cdot \theta^{-1.341} \le 7.5 [\text{N/mm}^2] \text{ with } \theta \text{ in } ^{\circ}\text{C}$	$\bar{\tau}_{fire}(\theta) = 1185 \cdot \theta^{-1.341} \leq 7.5 [\text{N/mm}^2] \text{ with } \theta \text{ in } ^{\circ}\text{C}$
$\theta_k = 113^{\circ} F (46^{\circ} C)$	$\theta_k = 108^{\circ} \text{F (44°C)}$

¹See Section 4.2.5 of this report. With $\theta_{\text{max}} = 247^{\circ}\text{C}$ (477°F). For temperatures larger than θ_{max} the bond strength $\bar{\tau}_{fire}(\theta) = 0$.

¹Development lengths valid for static, wind, and earthquake loads (SDC A and B).

² Development lengths in SDC C through F must comply with ACI 318-19 Chapter 18 and section 4.2.4 of this report.

³ f_{ν} and f_{ν} used in this table are for example purposes only. For sand-lightweight concrete, increase development length by 33%, unless the provisions of ACI 318-19 25.4.2.5 are met to permit $\lambda > 0.75$.

 $^{^{\}rm 5}$ Calculations may be performed for other steel grades per ACI 318-19 Chapter 25.

⁶ Minimum development length shall not be less than 12 in (305 mm) per ACI-19 Section 25.4.2.1

²For application with rebar #11 (36mm) or larger in an overhead installation, the bond strengths must be decreased by 11 percent.

³Bond strengths under fire are for short-term loads such as wind and seismic, and for long-term/sustained loads including dead and live loads.

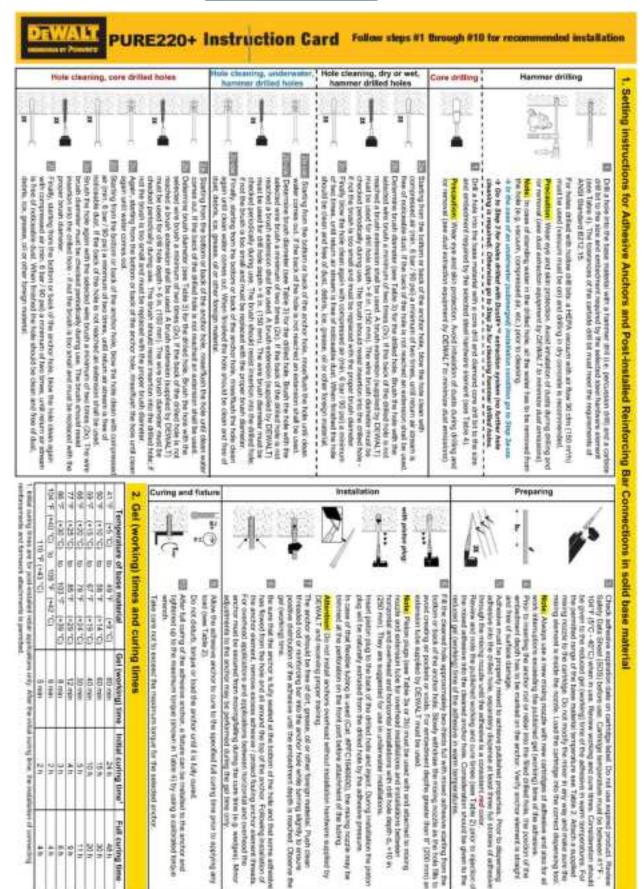
For post-installed reinforcing bar applications in holes drilled with a hammer drill and carbide bit (or DEWALT hollow carbide drill bit) or diamond core bit.

TABLE 22— APPLICABLE SECTIONS OF THE IBC CODE UNDER EACH EDITION OF THE IBC

2024 IBC	2021 IBC	2018 IBC	2015 IBC			
Section 1	605.1	Section 1605.2 or 1605.3				
	Section 1705.1.1					
Table 1705.3						
Section 1705						
Section 1706						
Section 1707						
Chapter 19						
Section 1901.3						
Section 1903						
Section 1905						
Section 1905.7	Section 1905.7 Section 1905.1.8					

TABLE 23— APPLICABLE SECTIONS OF ACI 318 UNDER EACH EDITION OF THE IBC

2024 IBC	2021 IBC	2018 IBC	2015 IBC	
ACI 318-19		ACI 318-14		
2.3		2.3		
5.3		5.3		
Cha	pter 17	Chapter 17		
	7.2.4	17.2.6		
	7.3.1	17.2.7		
17.5.1.2		17.3.1		
17.5.2		17.3.1.1		
	7.5.3	17.3.3		
	.6.1.2	17.4.1.2		
	7.6.2		4.2	
	.6.2.2	17.4		
	.6.2.5	17.4		
	7.6.5		4.5	
	.5.1.2b	17.4.1.5d		
	5.5.2.1	17.4.5.2		
	.6.5.5	17.4.5.5		
	.6.5.5.1b	Eq. 17.4.5.5b		
	7.6.5.5.1c	Eq. 17.4.5.5c		
	.7.1.2	17.5.1.2		
	7.7.2	17.5.2		
17.7.2.2		17.5.2.2		
17.7.3		17.5.3		
17.8		17.6		
17.8.2 and 17.8.3		17.6.1, 17.6.2 and 17.6.3 17.7.1 and 17.7.3		
	17.9.2			
17.9.3		17.7.4 17.7.6		
17.9.5 17.10		17.7.6 17.2.3		
Chapter 18		_		
Chapter 19		Chapter 18 Chapter 19		
Chapter 19 Chapter 25		Chapter 19 Chapter 25		
25.4.2.5		25.4.2.4		
26.6.3.2 (b)		26.6.3.1 (b)		
26.7.2		17.8.1 and 17.8.2		
26.7.1(l) and 26.7.2(e)		17.8.2.2 or 17.8.2.3		
26.13.3.2(e)		17.8.2.4, 26.7.1(h) and 26.13.3.2(c)		
20.13.3.2(8)		17.0.2.7, 20.7.1(11) and 20.10.0.2(b)	



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Heat

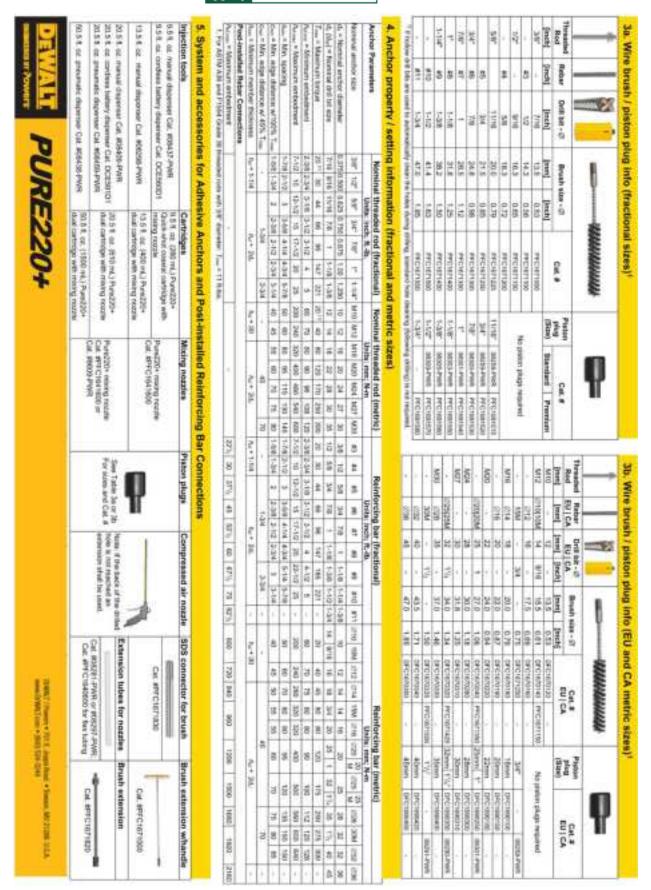


FIGURE 4—INSTALLATION INSTRUCTIONS (Continued)



ICC-ES Evaluation Report

ESR-5144 City of LA Supplement

Reissued November 2024
Revised August 2025

This report is subject to renewal November 2025.

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A Subsidiary of the International Code Council®

DIVISION: 03 00 00—CONCRETE Section: 03 16 00—Concrete Anchors

DIVISION: 05 00 00—METALS

Section: 05 05 19—Post-Installed Concrete Anchors

REPORT HOLDER:

DEWALT

EVALUATION SUBJECT:

PURE220+™ ADHESIVE ANCHOR SYSTEM AND POST-INSTALLED REINFORCING BAR IN CRACKED AND UNCRACKED CONCRETE (DEWALT)

1.0 REPORT PURPOSE AND SCOPE

Purpose:

The purpose of this evaluation report supplement is to indicate that DEWALT Pure220+ Adhesive Anchor System and Post-Installed Reinforcing Bar in Cracked and Uncracked Concrete, described in ICC-ES evaluation report <u>ESR-5144</u>, has also been evaluated for compliance with the codes noted below as adopted by the Los Angeles Department of Building and Safety (LADBS).

Applicable code editions:

- 2023 City of Los Angeles Building Code (LABC)
- 2023 City of Los Angeles Residential Code (<u>LARC</u>)

2.0 CONCLUSIONS

The DEWALT Pure220+ Adhesive Anchor System and Post-Installed Reinforcing Bar in Cracked and Uncracked Concrete, described in Sections 2.0 through 7.0 of the evaluation report <u>ESR-5144</u>, complies with the LABC Chapter 19, and the LARC, and are subject to the conditions of use described in this supplement.

3.0 CONDITIONS OF USE

The DEWALT Pure220+ Adhesive Anchor System and Post-Installed Reinforcing Bar in Cracked and Uncracked Concrete described in this evaluation report must comply with all of the following conditions:

- All applicable sections in the evaluation report ESR-5144.
- The design, installation, conditions of use and identification of the anchors are in accordance with the 2021 *International Building Code*[®] (IBC) provisions noted in the evaluation report <u>ESR-5144</u>.
- The design, installation and inspection are in accordance with additional requirements of LABC Chapters 16 and 17, as applicable.
- Under the LARC, an engineered design in accordance with LARC Section R301.1.3 must be submitted.
- The design strength values listed in the evaluation report and tables are for the connection of the anchors or post installed reinforcing bars to the concrete. The connection between the anchors or post installed reinforcing bars and the connected members shall be checked for capacity (which may govern).
- For use in wall anchorage assemblies to flexible diaphragms, anchors shall be designed per the requirements of City of Los Angeles Information Bulletin P/BC 2020-071.

This supplement expires concurrently with the evaluation report, reissued November 2024 and revised August 2025.





ICC-ES Evaluation Report

ESR-5144 FL Supplement w/ HVHZ

Reissued November 2024 Revised August 2025

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Section: 05 05 19—Post-Installed Concrete Anchors

REPORT HOLDER:

DEWALT

EVALUATION SUBJECT:

PURE220+™ ADHESIVE ANCHOR SYSTEM AND POST-INSTALLED REINFORCING BAR IN CRACKED AND UNCRACKED CONCRETE (DEWALT)

1.0 REPORT PURPOSE AND EVALUATION SCOPE

Purpose:

The purpose of this evaluation report supplement is to indicate that DEWALT Pure220+ Adhesive Anchor System and Post-Installed Reinforcing Bar in Cracked and Uncracked Concrete, recognized in ICC-ES evaluation report <u>ESR-5144</u>, has also been evaluated for compliance with the codes noted below.

Compliance with the following codes:

- 2023 Florida Building Code—Building
- 2023 Florida Building Code—Residential

2.0 PURPOSE OF THIS SUPPLEMENT

The DEWALT Pure220+ Adhesive Anchor System and Post-Installed Reinforcing Bar in Cracked and Uncracked Concrete, described in Sections 2.0 through 7.0 of the evaluation report <u>ESR-5144</u>, complies with the *Florida Building Code—Building* and the *Florida Building Code—Residential*, as applicable, provided the design requirements are determined in accordance with the *Florida Building Code—Building* or the *Florida Building Code—Residential*, as applicable. The installation requirements noted in ICC-ES evaluation report <u>ESR-5144</u> for the 2021 *International Building Code®* meet the requirements of the *Florida Building Code—Building* or the *Florida Building Code—Residential*, as applicable.

Use of the DEWALT Pure220+ Adhesive Anchor System and Post-Installed Reinforcing Bar in Cracked and Uncracked Concrete has also been found to be in compliance with the High-Velocity Hurricane Zone provision of the *Florida Building Code—Building and the Florida Building Code—Residential* with the following condition.

a) For connections subject to uplift, the connection must be designed for no less than 700 pounds (3114 N).

For products falling under Florida Rule 61G20-3, verification that the report holder's quality assurance program is audited by a quality assurance entity approved by the Florida Building Commission for the type of inspections being conducted is the responsibility of an approved validation entity (or the code official when the report holder does not possess an approval by the Commission).

This supplement expires concurrently with the evaluation report, reissued November 2024 and revised August 2025.

